PACIFIC NORTHWEST STRUCTURAL GROUP, LLC

A PROFESSIONAL ENGINEERING COMPANY

BASIC PERMIT PACKAGE REVIEWED FOR CODE COMPLIANCE **WITH IRC 2015** KITSAP COUNTY BUILDING DEPARTMENT

6193 NE MALBON CT. KINGSTON, WA 98346 360.903.2803

STRUCTURAL CALCULATIONS

NW HOGAN LN & NELS NELSON RD NW_{Reviewed for code compliance} with IRC 2015 Department of the property of the Kitsap County Building Department lasmith@co.kitsap.wa.us

ALL COMPUTATIONS AND ENGINEERING FOR THIS PROJECT HAVE BEEN PERFORMED BY MYSELF OR UNDER MY SUPERVISION.



26-JUL-19

DIGITAL SIGNATURE

Digitally signed by David I C1 by David L. Starkel Date: 2019.07.26

Established Basic Permit #

19-03646

| Project | Red Barn Lane - Duplex 1400 | Designer | DLS |
|----------|--|-------------|------------------------|
| Location | NW Hogan Ln & Nels Nelson Rd NW, Bremerton, WA | Project No. | 19-002c |
| Client | Envision Northwest, LLC | Revised | 15-Sep-18 |
| | Design Live and Dead Loads, Soil Data | Neviseu | 13-3 c p-10 |

DESIGN LIVE AND DEAD LOADS

| ROOF L | OAD : | | |
|-------------------------|-------|------|-----|
| Asphalt Shingles | 1.5 | PSF | |
| Re-Roof | | 1.5 | PSF |
| Roof Shtg | | 1.5 | PSF |
| Truss @ 24" oc | | 3.3 | PSF |
| Insulation | | 1.6 | PSF |
| Gypsum Shtg | | 2.2 | PSF |
| | | PSF | |
| | | PSF | |
| SUB-T | OTAL | 11.6 | PSF |
| SLOPE CORRECTION "X:12" | 5.00 | 1.1 | |
| MISCELLANE | 2.4 | PSF | |
| ROOF DEAD L | 15.0 | PSF | |
| ROOF SNOW L | 25.0 | PSF | |
| REDUCED SNOW LOA | N/A | PSF | |
| ROOF LIVE L | OAD | 16.0 | PSF |

| EXTERIOR WALL LOAD | | | | |
|-----------------------|------|-----|--|--|
| Siding | 4.0 | PSF | | |
| Wall Shtg | 1.5 | PSF | | |
| 2x6 @ 16" oc | 1.7 | PSF | | |
| Bottom & Top Plates | 0.8 | PSF | | |
| Insulation | 0.5 | PSF | | |
| Gypsum Shtg | 2.2 | PSF | | |
| Mech., Elec., & Misc. | 0.3 | PSF | | |
| EXTER. WALL DEAD LOAD | 11.0 | PSF | | |

| INTERIOR WALL LOAD | | | | |
|-------------------------|-----|-----|--|--|
| Gypsum Shtg | 4.4 | PSF | | |
| 2X4 @ 16" oc | 1.1 | PSF | | |
| Insulation | 0.5 | PSF | | |
| Bottom & Top Plates | 0.8 | PSF | | |
| Mech., Elec., & Misc. | 1.2 | PSF | | |
| INTEDIOD WALL DEAD LOAD | 9.0 | DOE | | |

| FLOOR LOAD | | | | | |
|-----------------------|------|-----|--|--|--|
| Floor Covering | 1.0 | PSF | | | |
| Floor Shtg | 2.3 | PSF | | | |
| Floor Joist | 3.3 | PSF | | | |
| Insulation | 1.3 | PSF | | | |
| Gypsum Sheathing | 5.6 | PSF | | | |
| Mech., Elec., & Misc. | 1.5 | PSF | | | |
| | | PSF | | | |
| FLOOR DEAD LOAD | 15.0 | PSF | | | |
| FLOOR LIVE LOAD | 40.0 | PSF | | | |

| DECK OR BALCONY DEAD LOAD | | | | | | |
|-------------------------------|-----|-----|--|--|--|--|
| 2x Decking | 4.5 | PSF | | | | |
| Deck Joist | 3.3 | PSF | | | | |
| Mech., Elec., & Misc. 4.2 PSF | | | | | | |
| | | PSF | | | | |
| DECK DEAD LOAD 12.0 PSF | | | | | | |
| DECK LIVE LOAD 60.0 PSF | | | | | | |

| | | PSF |
|-----------------|---|-----|
| | | PSF |
| FLOOR DEAD LOAD | - | PSF |
| FLOOR LIVE LOAD | | PSF |

The soil bearing shall be 1500 PSF unless a soil analysis has been preformed. Please revise the plans or provide a soil analysis showing the 2500 PSF.

SOILS DATA

| SOILS REPORT | N/A | | | | | | |
|-----------------------|------------|-----|----------|------------------|--------|------|-----|
| GEOTECHNICAL ENGINEER | N/A | | | DATE OF REPORT | N/A | | |
| | / | | | | | | |
| BASIC BEARING | G PRESSURE | | | ACTIVE SOIL | . PRES | SURE | |
| PADS & CONT. | FND 2,500 | PSF | | PASSIVE PRESSI | JRE | N/A | PCF |
| INCREASE FOR W | IDTH N/A | % | | SOIL FRICT | ION | N/A | |
| INCREASE FOR DE | EPTH N/A | % | | E.F.P. (Cantile | ver) | N/A | PCF |
| MAX. SOIL PRESS | SURE 2,500 | PSF | | E.F.P. (Restrain | ned) | N/A | PCF |
| ISOLATED FOUNDAT | IONS N/A | PSF | | | | • | |
| | | | <u>-</u> | | | | |

Established Basic Permit #

C:\Users\dista\Dropbox\PNW Project Files\2019 Projects\19-002C Red Barn Lane - Duplex\ENGR\19-002c Design Criteria 2018.xlsxLoads

19-03646

| Project | Red Barn Lane - Duplex 1400 | Designer | DLS |
|----------|---------------------------------------|-------------|-----------|
| Location | NW Hogan Ln & Nels Nelson Rd NW, Brem | Project No. | 19-002c |
| Client | Envision Northwest, LLC | Revised | 15-Sep-18 |
| 2 | 015 IBC Section 1609.6 Wind Loads | Reviseu | 15-3ep-16 |

|--|

| BOILDING BINITY. | | | | | | |
|--|----------|-----|-----------|-----------|----------|---|
| Ultimate Design Wind Speed, V _{ult} | 110 | MPH | Figure 16 | 609 | | |
| Exposure | В | | 1609.4 | | Exposure |) |
| Roof Pitch | 5.00 | :12 | | В | С | D |
| θ= | 22.62 | | _ | | | |
| | Conditio | n 1 | | | | |
| Building Length | 37.00 | ft | | | | |
| Building Width | 37.00 | ft | | | | |
| 1st Level Plate Height | 9.08 | ft | | | | |
| 2nd Level Plate Height | 9.08 | ft | | | | |
| 3rd Level Plate Height | 8.08 | ft | | | | |
| Gable Height | 33.95 | ft | | | | |
| Roof Height | 7.71 | ft | | | | |
| Mean Roof Height h = | 30.09 | ft | | | | |
| 1609.6 Alternate All-Heights Method | | | | | | |
| Wind directionality factor, K _d | 0.85 | | | | | |
| Topographic Factor, K _{zt} | 1.00 | | | | | |
| Velocity pressure factor, K _z | 0.70 | | ASCE 7- | 10, 27.3- | 1 | |
| IBC 2015 Table 1609.6.2, Net Pressure Coefficients, C _{net} | | | | | | |

| | 1100 | |
|---|------------|------------|
| Description | + Internal | - Internal |
| Description | pressure | pressure |
| Windward Wall | 0.43 | 0.73 |
| Leeward Wall | (0.51) | (0.21) |
| Sidewall | (0.66) | (0.35) |
| Wind perpendicular to ridge Leeward roof or flat roof | (0.66) | (0.35) |
| Wind parallel to ridge and flat roofs | (1.09) | (0.79) |
| Windward roof slopes | 0.03 | 0.34 |

| Description | Pressure | |
|---|----------|-----|
| Windward Wall | 21.42 | |
| Leeward Wall | 13.29 | psf |
| Sidewall | 18.65 | psf |
| Wind perpendicular to ridge Leeward roof or flat roof | 18.65 | |
| Windward roof slopes | 6.83 | psf |

| Al | lowable Ur | niform Wind | Load | |
|-----------------|------------|-------------|---------|--------|
| Level | Trans | sverse | Longitu | ıdinal |
| 1st Level Plate | 189.1 | plf | 101.6 | plf |
| 2nd Level Plate | 178.7 | plf | 96.0 | plf |
| 3rd Level Plate | 115.7 | plf | 88.3 | plf |

Establish | Drophox | Project Files | 2019 Projects | 19-002C Red Barn Lane - Duplex | ENGR | 19-002c Design Criteria

19-03646

| Project | Red Barn Lane - Duplex 1400 | Designer | DLS |
|----------|--|-------------|-----------|
| Location | NW Hogan Ln & Nels Nelson Rd NW, Breme | Project No. | 19-002c |
| Client | Envision Northwest, LLC | Revised | 15-Sep-18 |
| 2015 | IBC Section 1613 Earthquake Loads | Neviseu | 13-38μ-16 |

| | | 2015 | IBC Section 16 | 13 Earthquake | Loads | · · |
|--|--------------|--------------------------------|----------------------------------|------------------|------------------|----------------------------|
| | | | | | | |
| ASCE 7 | 7-10 & IBC | 2015 Section | on 1613, EAF | RTHQUAKE | | |
| Soil Site Class | D | | | | ASCE 7-10 | 11.4.2 (Default=D) |
| Response Spectral Acc. (0.2 sec) S _s | 1.39 | | | | | Figure(s) 22-1 |
| Response Spectral Acc.(1.0 sec) S ₁ | 0.55 | | | | through 22- | 18 |
| Site Coefficient F _a | 1.00 | | | | ASCE 7-10 | Table 11.4-1 |
| Site Coefficient F _v | 1.50 | | | | ASCE 7-10 | Table 11.4-2 |
| Max Considered Earthquake Acc. S_{MS} | 1.387 | F _a .S _s | | | ASCE 7-10 | (11.4-1) |
| Max Considered Earthquake Acc. S_{M1} | 0.828 | F _v .S ₁ | | | ASCE 7-10 | (11.4-2) |
| @ 5% Damped Design S_{DS} | 0.925 | 2/3.S _{MS} | | | ASCE 7-10 | , |
| S_{D1} | 0.552 | 2/3.S _{M1} | | | ASCE 7-10 | (11.4-4) |
| Risk Category | | | | II | ASCE 7-10 | Table 1-1 |
| Design Category Consideration: | | | | | | |
| In each of the two orthogonal directions, the structure, Ta, determined in accorda 0.8Ts, where Ts is determined in accord | nce with Sec | tion 12.8.2.1 is | | Yes | ASCE 7-10 | 11.6 |
| In each of two orthogonal directions, the to calculate the story drift is less than Ts | | period of the s | structure used | Yes | | |
| Diaphragms are rigid as defined in Secti flexible, the distance between vertical ele system does not exceed 40 ft. | | | | Yes | | |
| Seismic Design Category (SDC) | - | | | | ASCE 7-10 | 11.4.1 |
| Seismic Design Category for 0.1 sec | D | | | | ASCE 7-10 | Table 11.6-1 |
| Seismic Design Category for 1.0 sec | D | | | | ASCE 7-10 | Table 11.6-2 |
| S1 < .75g | - | | | | ASCE 7-10 | 11.6 |
| Seismic Design Category (SDC) | D | | | | ASCE 7-10 | 11.6 |
| Seismic Force-Resisting System | A. BEARIN | G WALL SYST | ГЕМЅ | | | |
| | 15. Light- | , , | valls sheathed w | vith wood struct | ural panels rate | ed for shear resistance or |
| Footnotes | - | - | | | | |
| | - | - | | | | |
| | - | - | | | | |
| ASCE 7 Section Where Detailing Requirements Are Specified | 14.1 and | | | | | |
| Building ht. h _n | 30.09 | ft | | ing Height (ft) | | |
| C_{t} | 0.020 | Х | 0.75 | ASCE 7-10 | Table 12.8-2 | |
| C _u | 1.400 | for SD1 of 0 | _ | | | Table 12.8-1 |
| Approximate Fundamental Period, T _a | 0.257 | sec | $C_{t} \cdot (h_n)^x$ | | ASCE 7-10 | |
| T _s | 0.597 | sec | S _{D1} /S _{DS} | | ASCE 7-10 | |
| TL | 6.00 | sec | | | ASCE 7-10 | 11.4.5 |
| Period for Computing Drift | 0.360 | sec | C _u .T _a | | | |
| Fundamental Period, T | 0.257 | sec | | | | |
| 0.8T _s | 0.478 | sec | $0.8(S_{D1}/S_{DS})$ | | ASCE 7-10 | |
| Response Modification Coef. R | 6.50 | | | | ASCE 7-10 | Table 12.14-1 |

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19-03646

| Pacific Northwest Structural Group, Ll | | Project Location Client 2015 | Red Barn Lane - Duplex 1400 NW Hogan Ln & Nels Nelson F Envision Northwest, LLC IBC Section 1613 Earthquake I | Rd NW, Breme | Designer DLS Project No. 19-002c Revised 15-Sep-18 |
|--|---------|--|--|---------------------|---|
| Over Strength Factor Ω_{o} | 3.00 | | | ASCE 7-10 | Table 12.14-1 |
| Deflection Amplification Factor, C _{db} | 4.00 | | | ASCE 7-10 | Table 12.14-1 |
| Importance factor I _E | 1.00 | | | ASCE 7-10 Table 2-2 | Table 1.5-2, UFC 3-301-0 |
| C_s | 0.142 | S _{DS} /R/I _E | | ASCE 7-10 | (12.8-2) |
| T<=TL therefore Cs need not to exceed | 0.330 | $S_{D1}/(T(R/I_E)$ |) | ASCE 7-10 | (12.8-3) |
| T <tl (12.8-4)="" a<="" n="" th="" therefore=""><th>N/A</th><th>$S_{D1}.T_L/T^2(R$</th><th>/I_E)</th><th>ASCE 7-10</th><th>(12.8-4)</th></tl> | N/A | $S_{D1}.T_L/T^2(R$ | /I _E) | ASCE 7-10 | (12.8-4) |
| C_s | 0.041 | 0.044S _{DS} .I _E | ≥ 0.01 | ASCE 7-10 | (12.8-5) |
| S1 < 0.6g (12.8-6) N/A | N/A | 0.5S ₁ /(R/I _E) | | ASCE 7-10 | (12.8-6) |
| Use C _s | 0.142 | | | | |
| Design Base Shear V | 0.142 W | Control | | ASCE 7-10 | (12.8-1) |
| Design Service Level Base Shear V | 0.1 W | | | | |

| | Seisı | mic Load | | | |
|-----------------|----------------------|---------------------|-----------|-----------------|----------------------|
| Level | W _x (lbs) | h _x (ft) | $W_x.h_x$ | C _{vx} | F _x (lbs) |
| 1st Level Plate | 31,398 | 9.1 | 285,098 | 0.374 | 3,218 |
| 2nd Level Plate | 31,398 | 9.1 | 285,098 | 0.374 | 3,218 |
| 3rd Level Plate | 23,799 | 8.1 | 192,298 | 0.252 | 2,171 |
| | 86,596 | $\Sigma W_x.h_x$ | 762,494 | | |

| Design Service Level Base Shear V | 8,608 | lbs | | |
|-----------------------------------|-------|--------|--------|--------|
| | Trar | sverse | Longit | udinal |
| Diaphragm Width | 37.00 | ft | 37.00 | ft |
| 1st Level Plate | 87.0 | plf | 87.0 | plf |
| 2nd Level Plate | 87.0 | plf | 87.0 | plf |
| 3rd Level Plate | 58.7 | plf | 58.7 | plf |

Established Basic Permit #
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| Project | Red Barn Lane - Duplex 1400 | Designer | DLS |
|----------|--|-------------|-----------|
| Location | NW Hogan Ln & Nels Nelson Rd NW, Breme | Project No. | 19-002c |
| Client | Envision Northwest, LLC | D | 10.14 10 |
| | ASCE 7-10 Snow Loads | Revised | 18-May-18 |

| | ASCE 7-10 7.3 FLA | T ROOF SNOW | V LOAD |
|---|--------------------------|-----------------|--|
| Ground Snow Load, p _g | 30.0 | PSF | ASCE 7-10 7.2 |
| Exposure Category | В | | ASCE 7-10 26.7.3 Exposure Categories |
| Exposure of Roof | Partially Exposed | | ASCE 7-10 Table 7-2 Exposure Factor |
| Thermal Condition | All structures except as | indicated below | |
| Risk Category | II | | ASCE 7-10 Table 1.5-1, UFC 3-301-01 Table 2-2 |
| Snow load importance factor, I _s | 1.0 | | ASCE 7-10 Table 1.5-2, UFC 3-301-01 Table 2-2 |
| Snow exposure factor, C _e | 1.00 | | ASCE 7-10 Table 7-2 Exposure Factor |
| Thermal factor, C _t | 1.00 | | ASCE 7-10 Table 7-3 Thermal Factor |
| Flat-roof snow load, p _f | 21.0 | PSF | ASCE 7-10 (7.3-1) 0.7C _e C _t I _s p _g |
| Min. Design Flat Roof Snow Load, p _m | 20.0 | PSF | ASCE 7-10 74 $p_g \le 20 \text{ PSF } I_s p_g, p_g > 20 \text{ PSF } 20I_s$ |
| Design Flat Roof Snow Load, p _f | 21.0 | PSF | |

| | ASCE 7-10 7.4 SLO | PE ROOF SNO | W LOAD |
|---|--------------------|-------------|---|
| Roof Pitch | 5 | :12 | |
| Roof Slope, O | 22.62 | 0 | |
| Roof Surface | All Other Surfaces | | |
| Warm Roof Slope Factor, C _s | 1.00 | | ASCE 7-10 Section 7.4.1, 7.4.2, 7.4.3 Figure(s) |
| Slope Roof Design Snow Load, p _s | 21.0 | PSF | ASCE-7-10 (74-1) C _{s*} p _f |

Established Basic Permit #
C:\Users\dista\Dropbox\PNW Project F les\2019 Projects\19-002C Red Barn Lane - Duplex\ENGR\19-002c Design Criteria 2018.xlsxSnow Load

19-03646



David L. Starkel Pacific Northwest Structural Group, Inc. 6193 NE Malbon Ct. Kingston, WA 98346



Location: WALL-3RD-1

Wall

[2015 International Building Code(2015 NDS)]

1.5 IN x 5.5 IN x 8.08 FT @ 16 O.C. #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 87.0%

Controlling Factor: Combined Stress Factor

Location: RFB1 Roof Beam

[2015 International Building Code(2015 NDS)]

(2) 1.5 IN x 5.5 IN x 3.33 FT #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 71.1% Controlling Factor: Moment

Location: RFB2 Roof Beam

[2015 International Building Code(2015 NDS)]

(2) 1.5 IN x 5.5 IN x 5.33 FT #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 219.2% Controlling Factor: Moment

Location: WALL-3RD-2

Wall

[2015 International Building Code(2015 NDS)]

1.5 IN x 5.5 IN x 8.08 FT @ 16 O.C. #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 87.5%

Controlling Factor: Combined Stress Factor

Location: WALL-3RD-3

Wall

[2015 International Building Code(2015 NDS)]

1.5 IN x 5.5 IN x 8.08 FT @ 16 O.C. #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 87.5%

Controlling Factor: Combined Stress Factor

Location: MLB3-1

Multi-Loaded Multi-Span Beam

[2015 International Building Code(2015 NDS)]

1.75 IN x 11.875 IN x 6.83 FT

LSL 2360 Fb-1.55E - Louisiana Pacific

Section Adequate By: 86.2% Controlling Factor: Moment

Location: JST3-1

[2015 International Building Code(2015 NDS)]

SERIES 18 / 11.875 - Louisiana Pacific x 10.83 FT @ 16 O.C.

Section Adequate By: 123.4% Controlling Factor: End Reaction

Location: JST3-2 Floor Joist

[2015 International Building Code(2015 NDS)]

ESERIES 56 / 11.875 - Louisians Pacificx 17.8<mark>8</mark> FT @ 16 O.C.

Controlling Factor: End Reaction

19-03646

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Location: JST3-3 Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 56 / 11.875 - Louisiana Pacific x 19.83 FT (17.8 + 2) @ 16 O.C.

Section Adequate By: 34.9% Controlling Factor: End Reaction

Location: JST3-4 Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 56 / 11.875 - Louisiana Pacific x 19.83 FT @ 16 O.C.

Section Adequate By: 52.2% Controlling Factor: Deflection

Location: JST3-5 Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 56 / 11.875 - Louisiana Pacific x 15.67 FT @ 16 O.C.

Section Adequate By: 105.7% Controlling Factor: End Reaction

Location: JST3-6 Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 56 / 11.875 - Louisiana Pacific x 14.17 FT @ 16 O.C.

Section Adequate By: 127.5% Controlling Factor: End Reaction

Location: MLB3-2

Multi-Loaded Multi-Span Beam

[2015 International Building Code(2015 NDS)]

3.5 IN x 6.0 IN x 5.33 FT

24F-V4 - Visually Graded Western Species - Dry Use

Section Adequate By: 59.5% Controlling Factor: Moment

Location: WALL-2ND-1

Wall

[2015 International Building Code(2015 NDS)]

1.5 IN x 5.5 IN x 8.08 FT @ 16 O.C. #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 87.5%

Controlling Factor: Combined Stress Factor

Location: WALL-2ND-2

Wall

[2015 International Building Code(2015 NDS)]

1.5 IN x 5.5 IN x 8.08 FT @ 16 O.C. #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 95.1%

Controlling Factor: Combined Stress Factor

Location: WALL-2ND-3

Wal

[2015 International Building Code(2015 NDS)]

1.5 IN x 5.5 IN x 8.08 FT @ 16 O.C. #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 95.1%

Controlling Factor: Combined Stress Factor



David L. Starkel Pacific Northwest Structural Group, Inc. 6193 NE Malbon Ct. Kingston, WA 98346



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Location: JST3-7 Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 18 / 11.875 - Louisiana Pacific x 10.75 FT @ 16 O.C.

Section Adequate By: 125.0% Controlling Factor: End Reaction

Location: MLB3-3

Multi-Loaded Multi-Span Beam

[2015 International Building Code(2015 NDS)] 1.75 IN x 11.25 IN x 6.5 FT (4.8 + 1.8) LSL 1730 Fb-1.35E - Louisiana Pacific Section Adequate By: 330.4%

Section Adequate By: 330.49 Controlling Factor: Moment

Location: JST3-8 Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 56 / 11.875 - Louisiana Pacific x 6.33 FT (4.6 + 1.8) @ 16 O.C.

Section Adequate By: 13.7% Controlling Factor: End Reaction

Location: MLB3-4

Multi-Loaded Multi-Span Beam

[2015 International Building Code(2015 NDS)]

3.5 IN x 11.875 IN x 17.83 FT LSL 2360 Fb-1.55E - Louisiana Pacific Section Adequate By: 48.1%

Controlling Factor: Deflection

Location: WALL-2ND-4

Wall

[2015 International Building Code(2015 NDS)]

1.5 IN x 5.5 IN x 8.08 FT @ 16 O.C. #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 87.5%

Controlling Factor: Combined Stress Factor

Location: MLB3-5

Multi-Loaded Multi-Span Beam

[2015 International Building Code(2015 NDS)]

3.5 IN x 6.0 IN x 5.33 FT

24F-V4 - Visually Graded Western Species - Dry Use

Section Adequate By: 42.7% Controlling Factor: Moment

Location: WALL-2ND-5

Wall

[2015 International Building Code(2015 NDS)]

1.5 IN x 5.5 IN x 8.08 FT @ 16 O.C. #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 87.5%

Controlling Factor: Combined Stress Factor

Location: JST2-2 Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 56 / 11.875 - Louisiana Pacific x 12.75 FT (11 + 1.8) @ 16 O.C.

Established Basic Permit #

19-03646

Location: JST2-1 Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 18 / 11.875 - Louisiana Pacific x 10.83 FT @ 16 O.C.

Section Adequate By: 153.3% Controlling Factor: End Reaction

Location: JST2-3 Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 18 / 11.875 - Louisiana Pacific x 6.92 FT @ 16 O.C.

Section Adequate By: 296.5% Controlling Factor: End Reaction

Location: JST2-4 Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 18 / 11.875 - Louisiana Pacific x 3.33 FT @ 16 O.C.

Section Adequate By: 723.9% Controlling Factor: End Reaction

Location: MLB2-1 GLB Multi-Loaded Multi-Span Beam [2015 International Building Code(2015 NDS)] 3.5 IN x 11.875 IN x 25.09 FT (12.4 + 12.7)

24F-V4 - Visually Graded Western Species - Dry Use

Section Adequate By: 45.0% Controlling Factor: Moment

Location: MLB2-1 LSL

Multi-Loaded Multi-Span Beam

[2015 International Building Code(2015 NDS)] 3.5 IN x 11.875 IN x 25.09 FT (12.4 + 12.7) LSL 2360 Fb-1.55E - Louisiana Pacific

Section Adequate By: 75.7% Controlling Factor: Moment

Location: FTG-PST-MLB2-1B

Footing

[2015 International Building Code(2015 NDS)] Footing Size: 2.0 FT x 2.0 FT x 10.00 IN

Reinforcement: #4 Bars @ 8.00 IN. O.C. E/W / (3) min.

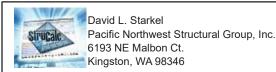
Section Footing Design Adequate

Location: PST-MLB2-1A

Column

[2015 International Building Code(2015 NDS)]

1.5 IN x 3.5 IN x 9.08 FT #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 16.4%





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Location: FTG-PST-MLB2-1A

Footing

[2015 International Building Code(2015 NDS)] Footing Size: 1.0 FT x 1.0 FT x 10.00 IN

Reinforcement in Long Direction: #4 Bars @ 5.50 IN. O.C. / (2) min.

Reinforcement in Short Direction-center band (Equal to width of short side): #4

Bars @ 5.50 IN. O.C. / (2) min.

Reinforcement in Short Direction-outside bands: #4 Bars @ 0.00 IN. O.C. / () Each

Section Footing Design Adequate

Location: WALL-1ST-1

Wall

[2015 International Building Code(2015 NDS)]

1.5 IN x 5.5 IN x 8.08 FT @ 16 O.C. #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 87.5%

Controlling Factor: Combined Stress Factor

Location: PST-MLB2-1B

Column

[2015 International Building Code(2015 NDS)]

5.5 IN x 5.5 IN x 9.08 FT #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 60.5%

Location: FTG-WALL-1ST-1

Footing

[2015 International Building Code(2015 NDS)]

Footing Size: 18.0 IN Wide x 8.0 IN Deep Continuous Footing With 8.0 IN Thick x

12.0 IN Tall Stemwall

LongitudinalReinforcement: (2) Continuous #4 Bars

TransverseReinforcement: #4 Bars @ 13.00 IN. O.C. (unnecessary)

Section Footing Design Adequate

Location: WALL-2ND-6

[2015 International Building Code(2015 NDS)]

1.5 IN x 5.5 IN x 8.08 FT @ 16 O.C. #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 87.5%

Controlling Factor: Combined Stress Factor

Location: MLB2-2

Multi-Loaded Multi-Span Beam

[2015 International Building Code(2015 NDS)]

1.75 IN x 11.875 IN x 6.5 FT

LSL 2360 Fb-1.55E - Louisiana Pacific

Section Adequate By: 226.3% Controlling Factor: Moment

Location: RFB3 Roof Beam

[2015 International Building Code(2015 NDS)]

3.5 IN x 7.25 IN x 8.33 FT

Location: RFB4 Roof Beam

[2015 International Building Code(2015 NDS)]

5.5 IN x 7.5 IN x 6.83 FT

#2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 242.3% Controlling Factor: Moment

Location: MLB2-3

Multi-Loaded Multi-Span Beam

[2015 International Building Code(2015 NDS)]

5.5 IN x 11.875 IN x 17.84 FT (10.9 + 6.9) / 30F - 30F-E

DF2 - Dry Use

Section Adequate By: 5.9% Controlling Factor: Shear

Location: PST-MLB2-3A

Column

[2015 International Building Code(2015 NDS)]

5.5 IN x 5.5 IN x 9.58 FT #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 36.2%

Location: PST-MLB2-3B

Column

[2015 International Building Code(2015 NDS)]

5.5 IN x 7.5 IN x 9.58 FT #1 - Douglas-Fir-Larch - Dry Use Section Adequate By: 11.0%

Location: PST-MLB2-3C

Column

[2015 International Building Code(2015 NDS)]

5.5 IN x 5.5 IN x 9.58 FT #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 67.0%

Location: FTG-PST-MLB2-3A

Footing

[2015 International Building Code(2015 NDS)] Footing Size: 2.5 FT x 2.5 FT x 10.00 IN

Reinforcement: #4 Bars @ 11.00 IN. O.C. E/W / (3) min.

Section Footing Design Adequate

Location: FTG-PST-MLB2-3C

[2015 International Building Code(2015 NDS)] Footing Size: 2.5 FT x 2.5 FT x 12.00 IN

Reinforcement: #4 Bars @ 7.00 IN. O.C. E/W / (4) min.

Section Footing Design Adequate





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Location: FTG-PST-MLB2-3B
Footing
[2015 International Building Code(2015 NDS)]
Footing Size: 3.5 FT x 3.5 FT x 10.00 IN
Reinforcement: #4 Bars @ 11.00 IN. O.C. E/W / (4) min.
Section Footing Design Adequate

Established Basic Permit #

19-03646

Wall

[2015 International Building Code(2015 NDS)]

1.5 IN x 5.5 IN x 8.08 FT @ 16 O.C. #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 87.0%

Controlling Factor: Combined Stress Factor





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DEFLECTIONS

Deflection due to lateral loads only: Defl = 0.06 IN = L/1638 Live Load Deflection Criteria: L/180

VERTICAL REACTIONS

 Live Load:
 Vert-LL-Rxn =
 575 lb

 Dead Load:
 Vert-DL-Rxn =
 464 lb

 Total Load:
 Vert-TL-Rxn =
 1039 lb

HORIZONTAL REACTIONS

Total Reaction at Top of Column: TL-Rxn-Top = 83 lb
Total Reaction at Bottom of Column: TL-Rxn-Bottom = 83 lb

WALL DATA

Total Stud Length:

Wall Dead Weight:
Unbraced Length (X-Axis) Lx:
Unbraced Length (Y-Axis) Ly:
Stud End Condition-K (e):
Axial Load Duration Factor
Lateral Load Duration Factor (Wind/Seismic)

8.08 ft
11 psf
15 psf
16 psf
17 psf
18 psf
18

STUD PROPERTIES

#2 - Douglas-Fir-Larch

Compressive Stress: Base Values Adjusted

Fc = 1350 psi Fc' = 1254 psi

Cd=1.60 Cf=1.10 Cp=0.53

Bending Stress (X-X Axis): Fbx = 900 psi Fbx' = 2153 psi Cd=1.60 CF=1.30 Cr=1.15 Cl=1.00

Bending Stress (Y-Y Axis): Fby = 900 psi Fby' = 2153 psi

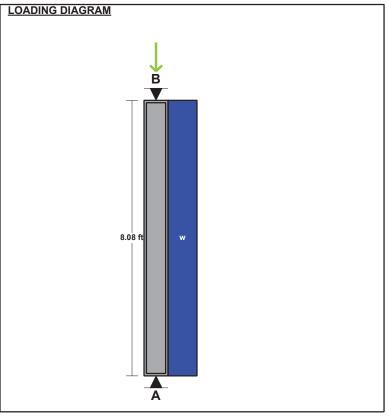
Cd=1.60 CF=1.30 Cr=1.15

Modulus of Elasticity: E = 1600 ksi E' = 1600 ksi

Stud Section (X-X Axis): dx =5.5 in Stud Section (Y-Y Axis): dy =1.5 in Area: A = 8.25 in2 Section Modulus (X-X Axis): Sx =7.56 in3 Section Modulus (Y-Y Axis): Sy = 2.06 in3 Slenderness Ratio: Lex/dx = 17.63Ley/dy =

Stud Calculations (Controlling Case Only):

Controlling Load Case: Axial Dead Load and Lateral loads (D + W or E) Actual Compressive Stress: Fc = 56 psi Allowable Compressive Stress: Fc' = 1254 psi Eccentricity Moment (X-X Axis): Mx-ex = 0 ft-lb Eccentricity Moment (Y-Y Axis): My-ey = 0 ft-lb Moment Due to Lateral Loads (X-X Axis): Mx =168 ft-lb Moment Due to Lateral Loads (Y-Y Axis): My = 0 ft-lb Bending Stress Lateral Loads Only (X-X Axis): Fbx = 266 psi Allowable Bending Stress (X-X Axis): Fbx' = 2153 psi Bending Stress Lateral Loads Only (Y-Y Axis): Fby = 0 psi Allowable Bending Stress (Y-Y Axis): Fby' = 2153 psi **Combined Stress Factor:** CSF = 0.13



WALL LOAD CALCULATOR

Live Load Dead Load **Tributary Width** Load Tracker: 0 plf DL = 0 plf LL = Roof: TA = 17.3 ft25 psf DL = 15 psf Upper Floor: 40 psf DL = 15 psf TA = 0 ft Upper Floor Height: 0 ft Middle Floor: 40 psf DL = II =15 psf TA = 0 ftMiddle Floor Height: 0 ft

Calculated Load: LL =431.3 plf DL =347.6 plf

AXIAL LOADING

 Live Load:
 PL =
 431 plf

 Dead Load:
 PD =
 348 plf

 Total Axial Load:
 PT =
 779 plf

LATERAL LOADING (Dy Face)
Uniform Lateral Load: wL-Lat = 15 psf

NOTES

Established Basic Permit #

19-03646

Location: RFB1 Roof Beam

[2015 International Building Code(2015 NDS)]

(2) 1.5 IN x 5.5 IN x 3.33 FT #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 71.1% Controlling Factor: Moment



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 DEFLECTIONS
 Center

 Live Load
 0.02
 IN L/2229

 Dead Load
 0.01
 in

 Total Load
 0.03
 IN L/1344

Live Load Deflection Criteria: L/240 Total Load Deflection Criteria: L/180

 REACTIONS
 A
 B

 Live Load
 718 lb
 718 lb

 Dead Load
 473 lb
 473 lb

 Total Load
 1191 lb
 1191 lb

 Bearing Length
 0.64 in
 0.64 in

BEAM DATA

Span Length 3.3 ft
Unbraced Length-Top 0 ft
Unbraced Length-Bottom 0 ft
Roof Pitch 5 :12
Roof Duration Factor 1.15

MATERIAL PROPERTIES

#2 - Douglas-Fir-Larch

Shear Stress: Fv = 180 psi Fv' = 207 psi Cd=1.15

Modulus of Elasticity: E = 1600 ksi E' = 1600 ksi Comp. $^{\perp}$ to Grain: Fc - $^{\perp}$ = 625 psi Fc - $^{\perp}$ = 625 psi

Controlling Moment: 991 ft-lb

1.665 ft from left support

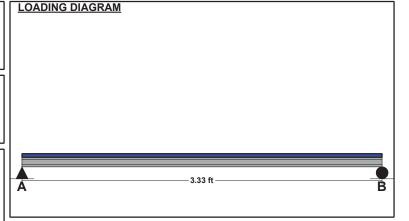
Created by combining all dead and live loads.

Controlling Shear: -881 lb

At a distance d from support.

Created by combining all dead and live loads.

Comparisons with required sections: Provided Req'd Section Modulus: 8.84 in3 15.13 in3 Area (Shear): 16.5 in2 6.38 in2 Moment of Inertia (deflection): 5.57 in4 41.59 in4 Moment: 991 ft-lb 1696 ft-lb Shear: -881 lb 2277 lb



ROOF LOADING Side One: Roof Live Load: LL = 25 psf Roof Dead Load: DL = 15 psf Tributary Width: TW = 17.3 ft Side Two: Roof Live Load: LL = 0 psf Roof Dead Load: DL = psf Tributary Width: TW = 0 ft

0 plf

WALL =

Wall Load:

SLOPE/PITCH ADJUSTED LENGTHS AND LOADS Adjusted Beam Length: Ladi = 3.33 ft Beam Self Weight: BSW = 4 plf Beam Uniform Live Load: wL = 431 plf Beam Uniform Dead Load: wD adj = 284 plf wT = Total Uniform Load: 715 plf

NOTES

Established Basic Permit #

19-03646

Location: RFB2 Roof Beam

[2015 International Building Code(2015 NDS)]

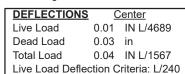
(2) 1.5 IN x 5.5 IN x 5.33 FT #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 219.2% Controlling Factor: Moment





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 REACTIONS
 A
 B

 Live Load
 133 lb
 133 lb

 Dead Load
 266 lb
 266 lb

 Total Load
 399 lb
 399 lb

 Bearing Length
 0.21 in
 0.21 in

Total Load Deflection Criteria: L/180

BEAM DATA

Span Length 5.3 ft
Unbraced Length-Top 0 ft
Unbraced Length-Bottom 0 ft
Roof Pitch 8 :12
Roof Duration Factor 1.15

MATERIAL PROPERTIES

#2 - Douglas-Fir-Larch

Shear Stress: Fv = 180 psi Fv' = 207 psi Cd=1.15

Modulus of Elasticity: E = 1600 ksi E' = 1600 ksi Comp. $^{\perp}$ to Grain: Fc - $^{\perp}$ = 625 psi Fc - $^{\perp}$ = 625 psi

Controlling Moment: 531 ft-lb

2.665 ft from left support

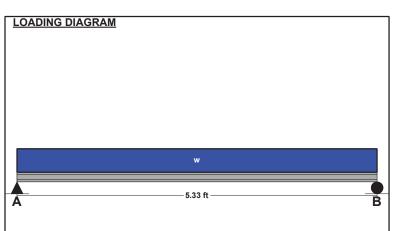
Created by combining all dead and live loads.

Controlling Shear: -335 lb

At a distance d from support.

Created by combining all dead and live loads.

Comparisons with required sections: Provided Req'd Section Modulus: 4.74 in3 15.13 in3 Area (Shear): 16.5 in2 2.43 in2 Moment of Inertia (deflection): 4.78 in4 41.59 in4 Moment: 531 ft-lb 1696 ft-lb Shear: -335 lb 2277 lb



ROOF LOADING Side One: Roof Live Load: LL = 25 psf Roof Dead Load: DL = 15 psf Tributary Width: TW = 2 ft Side Two: Roof Live Load: LL = 0 psf Roof Dead Load: DL = 0 psf Tributary Width: TW = 0 ft Wall Load: WALL = 60 plf

SLOPE/PITCH ADJUSTED LENGTHS AND LOADS Adjusted Beam Length: Ladi = 5.33 ft Beam Self Weight: BSW = 4 plf Beam Uniform Live Load: wL = 50 plf Beam Uniform Dead Load: wD adj = 100 plf Total Uniform Load: wT = 150 plf

NOTES

Established Basic Permit #

19-03646

Wall

[2015 International Building Code(2015 NDS)]

1.5 IN x 5.5 IN x 8.08 FT @ 16 O.C. #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 87.5%

Controlling Factor: Combined Stress Factor



of

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DEFLECTIONS

Deflection due to lateral loads only: Defl = 0.06 IN = L/1638 Live Load Deflection Criteria: L/180

VERTICAL REACTIONS

 Live Load:
 Vert-LL-Rxn =
 73 lb

 Dead Load:
 Vert-DL-Rxn =
 163 lb

 Total Load:
 Vert-TL-Rxn =
 236 lb

HORIZONTAL REACTIONS

Total Reaction at Top of Column: TL-Rxn-Top = 83 lb
Total Reaction at Bottom of Column: TL-Rxn-Bottom = 83 lb

WALL DATA

Total Stud Length:

Wall Dead Weight:
Unbraced Length (X-Axis) Lx:
Unbraced Length (Y-Axis) Ly:
Unbrace

STUD PROPERTIES

#2 - Douglas-Fir-Larch

Bending Stress (X-X Axis): Fbx = 900 psi Fbx' = 2153 psi

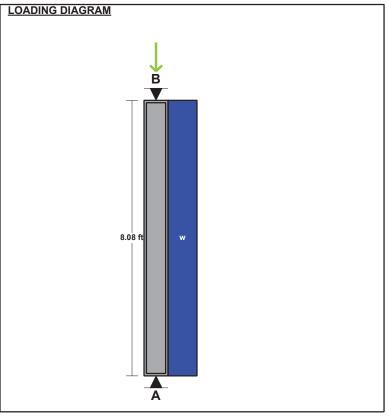
Cd=1.60 CF=1.30 Cr=1.15

Modulus of Elasticity: E = 1600 ksi E' = 1600 ksi

Stud Section (X-X Axis): dx =5.5 in Stud Section (Y-Y Axis): dy =1.5 in Area: A = 8.25 in2 Section Modulus (X-X Axis): Sx =7.56 in3 Section Modulus (Y-Y Axis): Sy = 2.06 in3 Slenderness Ratio: Lex/dx = 17.63Ley/dy =

Stud Calculations (Controlling Case Only):

Controlling Load Case: Axial Dead Load and Lateral loads (D + W or E) Actual Compressive Stress: Fc = 20 psi Allowable Compressive Stress: Fc' = 1254 psi Eccentricity Moment (X-X Axis): Mx-ex = 0 ft-lb Eccentricity Moment (Y-Y Axis): My-ey = 0 ft-lb Moment Due to Lateral Loads (X-X Axis): Mx =168 ft-lb Moment Due to Lateral Loads (Y-Y Axis): My = 0 ft-lb Bending Stress Lateral Loads Only (X-X Axis): Fbx = 266 psi Allowable Bending Stress (X-X Axis): Fbx' = 2153 psi Bending Stress Lateral Loads Only (Y-Y Axis): Fby = 0 psi Allowable Bending Stress (Y-Y Axis): Fby' = 2153 psi **Combined Stress Factor:** CSF = 0.13



WALL LOAD CALCULATOR

Live Load Dead Load **Tributary Width** Load Tracker: 0 plf DL = 0 plf LL = Roof: 2.2 ft 25 psf DL = 15 psf TA = Upper Floor: 40 psf DL = 15 psf TA = 0 ft Upper Floor Height: 0 ft Middle Floor: 40 psf DL = II =15 psf TA = 0 ftMiddle Floor Height: 0 ft

Calculated Load: LL = 55 plf DL =121.9 plf

AXIAL LOADING

 Live Load:
 PL =
 55 plf

 Dead Load:
 PD =
 122 plf

 Total Axial Load:
 PT =
 177 plf

LATERAL LOADING (Dy Face)
Uniform Lateral Load: wL-Lat = 15 psf

NOTES

Established Basic Permit #

19-03646

Wall

[2015 International Building Code(2015 NDS)]

1.5 IN x 5.5 IN x 8.08 FT @ 16 O.C. #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 87.5%

Controlling Factor: Combined Stress Factor





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DEFLECTIONS

Deflection due to lateral loads only: Defl = 0.06 IN = L/1638 Live Load Deflection Criteria: L/180

VERTICAL REACTIONS

 Live Load:
 Vert-LL-Rxn =
 73 lb

 Dead Load:
 Vert-DL-Rxn =
 163 lb

 Total Load:
 Vert-TL-Rxn =
 236 lb

HORIZONTAL REACTIONS

Total Reaction at Top of Column: TL-Rxn-Top = 83 lb
Total Reaction at Bottom of Column: TL-Rxn-Bottom = 83 lb

WALL DATA

Total Stud Length:

Wall Dead Weight:

Unbraced Length (X-Axis) Lx:

Unbraced Length (Y-Axis) Ly:

Stud End Condition-K (e):

Axial Load Duration Factor

Lateral Load Duration Factor (Wind/Seismic)

8.08 ft

9.08 ft

1.11 psf

1.12 ft

1.13 ft

1.15 ft

1

STUD PROPERTIES

#2 - Douglas-Fir-Larch

Base Values Adjusted

Compressive Stress: Fc = 1350 psi Fc' = 1254 psi

Cd=1.60 Cf=1.10 Cp=0.53

Bending Stress (X-X Axis): Fbx = 900 psi Fbx' = 2153 psi Cd=1.60 CF=1.30 Cr=1.15 Cl=1.00

Bending Stress (Y-Y Axis): Fby = 900 psi Fby' = 2153 psi

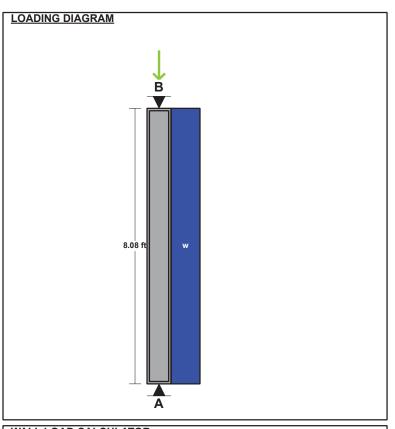
Cd=1.60 CF=1.30 Cr=1.15

Modulus of Elasticity: E = 1600 ksi E' = 1600 ksi

Stud Section (X-X Axis): dx =5.5 in Stud Section (Y-Y Axis): dy =1.5 in Area: A = 8.25 in2 Section Modulus (X-X Axis): Sx =7.56 in3 Section Modulus (Y-Y Axis): Sy = 2.06 in3 Slenderness Ratio: Lex/dx = 17.63Ley/dy =

Stud Calculations (Controlling Case Only):

Controlling Load Case: Axial Dead Load and Lateral loads (D + W or E) Actual Compressive Stress: Fc = 20 psi Allowable Compressive Stress: Fc' = 1254 psi Eccentricity Moment (X-X Axis): Mx-ex = 0 ft-lb Eccentricity Moment (Y-Y Axis): My-ey = 0 ft-lb Moment Due to Lateral Loads (X-X Axis): Mx =168 ft-lb Moment Due to Lateral Loads (Y-Y Axis): My = 0 ft-lb Bending Stress Lateral Loads Only (X-X Axis): Fbx = 266 psi Allowable Bending Stress (X-X Axis): Fbx' = 2153 psi Bending Stress Lateral Loads Only (Y-Y Axis): Fby = 0 psi Allowable Bending Stress (Y-Y Axis): Fby' = 2153 psi **Combined Stress Factor:** CSF = 0.13



WALL LOAD CALCULATOR

Live Load Dead Load **Tributary Width** Load Tracker: 0 plf DL = 0 plf LL = Roof: 2.2 ft 25 psf DL = 15 psf TA = Upper Floor: 40 psf DL = 15 psf TA = 0 ft Upper Floor Height: 0 ft Middle Floor: 40 psf DL = II =15 psf TA = 0 ftMiddle Floor Height: 0 ft

Calculated Load: LL = 55 plf DL =121.9 plf

AXIAL LOADING

 Live Load:
 PL =
 55 plf

 Dead Load:
 PD =
 122 plf

 Total Axial Load:
 PT =
 177 plf

LATERAL LOADING (Dy Face)
Uniform Lateral Load: wL-Lat = 15 psf

NOTES

Established Basic Permit #

19-03646

Location: MLB3-1

Multi-Loaded Multi-Span Beam

[2015 International Building Code(2015 NDS)]

1.75 IN x 11.875 IN x 6.83 FT

LSL 2360 Fb-1.55E - Louisiana Pacific

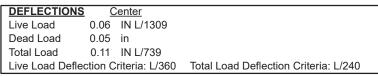
Section Adequate By: 86.2% Controlling Factor: Moment



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| ſ | REACTIONS | <u>A</u> | | <u>B</u> | |
|---|----------------|----------|----|----------|----|
| I | Live Load | 1653 | lb | 1653 | lb |
| l | Dead Load | 1277 | lb | 1277 | lb |
| ı | Total Load | 2930 | lb | 2930 | lb |
| ı | Bearing Length | 1.91 | in | 1.91 | in |

| BEAM DATA | <u>Ce</u> | nter |
|---------------------------|-----------|------|
| Span Length | 6.83 | ft |
| Unbraced Length-Top | 0 | ft |
| Unbraced Length-Bottom | 6.83 | ft |
| Live Load Duration Factor | 1.15 | |
| Notch Depth | 0.00 | |

MATERIAL PROPERTIES

LSL 2360 Fb-1.55E - Louisiana Pacific

Shear Stress: Fv = 410 psi Fv' = 472 psi

Cd=1.15

Modulus of Elasticity: E = 1550 ksi E' = 1550 ksi Comp. $^{\perp}$ to Grain: Fc - $^{\perp}$ = 875 psi Fc - $^{\perp}$ ' = 875 psi

Controlling Moment: 5003 ft-lb 3.41 Ft from left support of span 2 (Center Span)

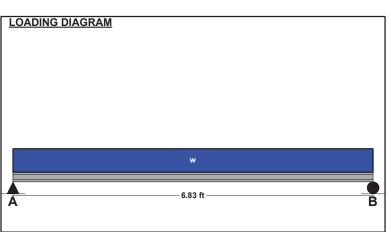
Created by combining all dead loads and live loads on span(s) 2

Controlling Shear: 2110 lb

At a distance d from left support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2

| Comparisons with required sections: | Req'd | Provided |
|-------------------------------------|------------|-----------------|
| Section Modulus: | 22.09 in3 | 41.13 in3 |
| Area (Shear): | 6.71 in2 | 20.78 in2 |
| Moment of Inertia (deflection): | 79.36 in4 | 244.21 in4 |
| Moment: | 5003 ft-lb | 9316 ft-lb |
| Shear: | 2110 lb | 6532 lb |



| UNIFORM LOADS | С | enter* | |
|----------------------|------|--------|------------------------------------|
| Uniform Live Load | 484 | plf | |
| Uniform Dead Load | 368 | plf | |
| Beam Self Weight | 6 | plf | |
| Total Uniform Load | 858 | plf | |
| * Load obtained from | Load | Tracke | r. See Summary Report for details. |

NOTES

Established Basic Permit #

19-03646

Location: JST3-1 Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 18 / 11.875 - Louisiana Pacific x 10.83 FT @ 16 O.C.

Section Adequate By: 123.4% Controlling Factor: End Reaction

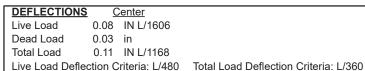




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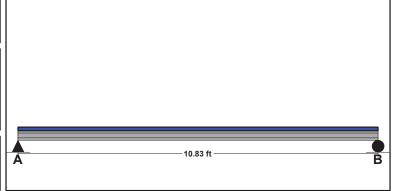
LOADING DIAGRAM

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| <u>REACTIONS</u> | <u>A</u> | <u>B</u> | |
|------------------|----------|----------|----|
| Live Load | 289 lb | 289 | lb |
| Dead Load | 108 lb | 108 | lb |
| Total Load | 397 lb | 397 | lb |
| Bearing Length | 1.75 in | 3.50 | in |
| Web Stiffeners | No | No | |

| SUPPORT LOADS | <u>A</u> | | <u>B</u> | |
|---------------|----------|-----|----------|-----|
| Live Load | 217 | plf | 217 | plf |
| Dead Load | 81 | plf | 81 | plf |
| Total Load | 298 | plf | 298 | plf |



I-JOIST PROPERTIES

SERIES 18 / 11.875 - Louisiana Pacific

Moment Cap: Base Values Adjusted
Mcap = 3100 ft-lb Mcap' = 3100 ft-lb

Cd = 1.00

Shear Stress: Vcap = 1335 lb Vcap' = 1335 lb

Cd = 1.00

Reaction A: Rcap = 887 lb Rcap' = 887 lb
Reaction B: Rcap = 1006 lb Rcap' = 1006 lb
E.l.: EI = 248 lb-in2 EI' = 248 lb-in2

Controlling Moment: 1075 ft-lb

5.41 Ft from left support of span 3 (Right Span) Created by combining all dead and live loads.

Controlling Shear: 397 lb

0.0 Ft from left support of span 2 (Center Span) Created by combining all dead and live loads.

 Comparisons with required sections:
 Req'd
 Provided

 E.I.:
 76 in2-lb E6
 248 in2-lb xE6

 Moment:
 1075 ft-lb
 3100 ft-lb

 Shear:
 397 lb
 1335 lb

| JOIST DATA | <u>Ce</u> | nter | | | | |
|--|-----------|------|--|--|--|--|
| Span Length | 10.83 | ft | | | | |
| Unbraced Length-Top | 0 | ft | | | | |
| Unbraced Length-Bottom | 0 | ft | | | | |
| Floor sheathing applied to top of joists-top of joists fully braced. | | | | | | |
| Floor Duration Factor 1.0 | 00 | | | | | |

 JOIST LOADING

 Uniform Floor Loading
 Center

 Live Load
 LL = 40 psf

 Dead Load
 DL = 15 psf

 Total Load
 TL = 55 psf

 TL Adj. For Joist Spacing wT = 73.3 plf

NOTES

Established Basic Permit #

19-03646

Location: JST3-2

Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 56 / 11.875 - Louisiana Pacific x 17.83 FT @ 16 O.C.

Section Adequate By: 80.8% Controlling Factor: End Reaction



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| DEFLECTIONS | <u>S</u> <u>Center</u> | |
|-----------------|------------------------|---------------------------------------|
| Live Load | 0.21 IN L/1007 | |
| Dead Load | 0.08 in | |
| Total Load | 0.29 IN L/733 | |
| Live Load Defle | ection Criteria: L/480 | Total Load Deflection Criteria: L/360 |

| <u>REACTIONS</u> | <u>A</u> | <u>B</u> |
|------------------|----------|----------|
| Live Load | 475 lb | 475 lb |
| Dead Load | 178 lb | 178 lb |
| Total Load | 653 lb | 653 lb |
| Bearing Length | 1.75 in | 1.75 in |
| Web Stiffeners | No | No |

| ٢ | SUPPORT LOADS | <u>A</u> | | <u>B</u> | |
|---|---------------|----------|-----|----------|-----|
| ı | Live Load | 356 | plf | 356 | plf |
| l | Dead Load | 134 | plf | 134 | plf |
| l | Total Load | 490 | plf | 490 | plf |



SERIES 56 / 11.875 - Louisiana Pacific

<u>Base Values</u> <u>Adjusted</u>

Moment Cap: Mcap = 10170 ft-lb Mcap' = 10170 ft-lb

Cd = 1.00

Shear Stress: Vcap = 2055 lb Vcap' = 2055 lb

Cd = 1.00

Reaction A: Rcap = 1182 lb Rcap' = 1182 lb Reaction B: Rcap = 1182 lb Rcap' = 668 lb-in2 EI' = 668 lb-in2

Controlling Moment: 2914 ft-lb

8.91 Ft from left support of span 3 (Right Span) Created by combining all dead and live loads.

Controlling Shear: 654 lb

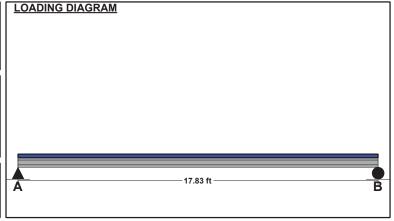
0.0 Ft from left support of span 2 (Center Span) Created by combining all dead and live loads.

 Comparisons with required sections:
 Req'd
 Provided

 E.I.:
 328 in2-lb E6
 668 in2-lb xE6

 Moment:
 2914 ft-lb
 10170 ft-lb

 Shear:
 654 lb
 2055 lb



| JOIST DATA | <u>C</u> e | nte | | | | |
|--|------------|-----|--|--|--|--|
| Span Length | 17.83 | ft | | | | |
| Unbraced Length-Top | 0 | ft | | | | |
| Unbraced Length-Bottom | 0 | ft | | | | |
| Floor sheathing applied to top of joists-top of joists fully braced. | | | | | | |
| Floor Duration Factor 1.0 | 00 | | | | | |

| | JOIST | LOADING |
|--|-------|---------|
|--|-------|---------|

| Uniform Floor Loading | <u>Cen</u> | <u>ter</u> |
|--------------------------------|------------|------------|
| Live Load LL = | 40 | psf |
| Dead Load DL = | 15 | psf |
| Total Load TL = | 55 | psf |
| TL Adj. For Joist Spacing wT = | 73.3 | plf |

NOTES

Established Basic Permit #

19-03646

Location: JST3-3 Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 56 / 11.875 - Louisiana Pacific x 19.83 FT (17.8 + 2) @ 16 O.C.

Section Adequate By: 34.9% Controlling Factor: End Reaction

| DEFLECTIONS | <u>Center</u> | | | Right |
|--------------------|---------------|----------------|--------|------------------------------------|
| Live Load | 0.21 | IN L/1007 | -0.07 | IN 2L/736 |
| Dead Load | 0.06 | in | -0.01 | in |
| Total Load | 0.27 | IN L/784 | -0.08 | IN 2L/610 |
| Live Load Deflect | ction C | riteria: L/480 |) Tota | al Load Deflection Criteria: L/360 |

| <u>REACTIONS</u> | <u>A</u> | | В | |
|------------------|----------|----|------|----|
| Live Load | 475 | lb | 669 | lb |
| Dead Load | 160 | lb | 399 | lb |
| Total Load | 635 | lb | 1068 | lb |
| Bearing Length | 3.50 | in | 3.50 | in |
| Web Stiffeners | No | | No | |

| SUPPORT LOADS | <u>A</u> | | <u>B</u> | |
|---------------|----------|-----|----------|-----|
| Live Load | 356 p | olf | 502 | plf |
| Dead Load | 120 p | olf | 299 | plf |
| Total Load | 476 r | olf | 801 | plf |

I-JOIST PROPERTIES

SERIES 56 / 11.875 - Louisiana Pacific

Reaction A: Rcap = 1441 lb Rcap' = 1441 lb
Reaction B: Rcap = 1441 lb Rcap' = 1441 lb
E.I.: EI = 668 lb-in2 EI' = 668 lb-in2

Controlling Moment: 2754 ft-lb

8.74 Ft from left support of span 3 (Right Span) Created by combining all dead and live loads.

Controlling Shear: -685 lb

18.0 Ft from left support of span 2 (Center Span) Created by combining all dead and live loads.

 Comparisons with required sections:
 Req'd
 Provided

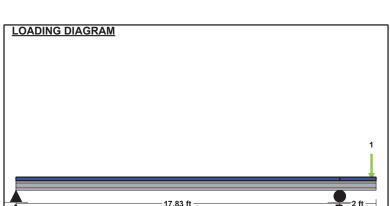
 E.I.:
 435 in2-lb E6
 668 in2-lb xE6

 Moment:
 2754 ft-lb
 10170 ft-lb

 Shear:
 -685 lb
 2055 lb



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| JOIST DATA | <u>Ce</u> | nter | : <u>R</u> i | ght | | | |
|----------------------------|-----------|------|--------------|----------|-------------|-------|--|
| Span Length | 17.83 | ft | 2 | ft | | | |
| Unbraced Length-Top | 0 | ft | 0 | ft | | | |
| Unbraced Length-Bottom | 0 | ft | 0 | ft | | | |
| Floor sheathing applied to | top of jo | ists | -top | of joist | s fully bra | aced. | |
| Floor Duration Factor 1.0 | 0 | | | | | | |

| JOIST LOADING | | | | | |
|------------------------------------|---------|-------------|-----------|------|------------|
| Uniform Floor Loading | | <u>Cent</u> | <u>er</u> | Rig | <u>ıht</u> |
| Live Load | LL = | 40 | psf | 40 | psf |
| Dead Load | DL = | 15 | psf | 15 | psf |
| Total Load | TL = | 55 | psf | 55 | psf |
| TL Adj. For Joist Spacin | ig wT = | 73.3 | plf | 73.3 | plf |
| Wall Loading | | | | | |
| Wall One | | | | | |
| Live Load ([⊥] to Joists | | 0 | plf | 55 | plf |
| Dead Load ([⊥] to Joist | s)D1 = | 0 | plf | 122 | plf |
| Load Location | X1 = | 0 | ft | 1.75 | ft |

NOTES

Established Basic Permit #

19-03646

Location: JST3-4 Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 56 / 11.875 - Louisiana Pacific x 19.83 FT @ 16 O.C.

Section Adequate By: 52.2% Controlling Factor: Deflection



page

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| <u>REACTIONS</u> | <u>A</u> | <u>B</u> | |
|------------------|----------|----------|----|
| Live Load | 529 lb | 529 | lb |
| Dead Load | 198 lb | 198 | lb |
| Total Load | 727 lb | 727 | lb |
| Bearing Length | 1.75 in | 1.75 | in |
| Web Stiffeners | No | No | |

| ĺ | SUPPORT LOADS | <u>A</u> | | <u>B</u> | |
|---|---------------|----------|-----|----------|-----|
| l | Live Load | 397 | plf | 397 | plf |
| ı | Dead Load | 149 | plf | 149 | plf |
| ı | Total Load | 545 | plf | 545 | plf |



SERIES 56 / 11.875 - Louisiana Pacific

<u>Base Values</u> <u>Adjusted</u>

Moment Cap: Mcap = 10170 ft-lb Mcap' = 10170 ft-lb

Cd = 1.00

Shear Stress: Vcap = 2055 lb Vcap' = 2055 lb

Cd = 1.00

 Reaction A:
 Rcap = 1182 lb
 Rcap' = 1182 lb

 Reaction B:
 Rcap = 1182 lb
 Rcap' = 1182 lb

 E.I.:
 EI = 668 lb-in2
 EI' = 668 lb-in2

Controlling Moment: 3605 ft-lb

9.91 Ft from left support of span 3 (Right Span) Created by combining all dead and live loads.

Controlling Shear: 727 lb

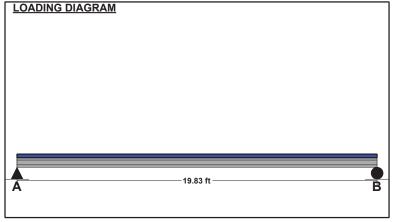
0.0 Ft from left support of span 2 (Center Span) Created by combining all dead and live loads.

 Comparisons with required sections:
 Req'd
 Provided

 E.I.:
 439 in2-lb E6
 668 in2-lb xE6

 Moment:
 3605 ft-lb
 10170 ft-lb

 Shear:
 727 lb
 2055 lb



| JOIST DATA | <u>Ce</u> | <u>enter</u> |
|----------------------------|-----------|-----------------------------------|
| Span Length | 19.83 | ft |
| Unbraced Length-Top | 0 | ft ft |
| Unbraced Length-Bottom | 0 | ft ft |
| Floor sheathing applied to | top of jo | oists-top of joists fully braced. |
| Floor Duration Factor 1.0 | 00 | |

| Uniform Floor Loading | | <u>Cent</u> | <u>er</u> |
|---------------------------|--------|-------------|-----------|
| Live Load | LL = | 40 | psf |
| Dead Load | DL = | 15 | psf |
| Total Load | TL = | 55 | psf |
| TL Adj. For Joist Spacing | = Tw g | 73.3 | plf |

NOTES

Established Basic Permit #

19-03646

Location: JST3-5

Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 56 / 11.875 - Louisiana Pacific x 15.67 FT @ 16 O.C.

Section Adequate By: 105.7% Controlling Factor: End Reaction



page

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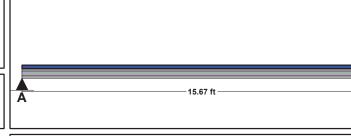
LOADING DIAGRAM

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| DEFLECTIONS | <u>Center</u> | |
|----------------------|-----------------|---------------------------------------|
| Live Load 0.13 | IN L/1423 | |
| Dead Load 0.05 | in | |
| Total Load 0.18 | IN L/1035 | |
| Live Load Deflection | Criteria: L/480 | Total Load Deflection Criteria: L/360 |

| <u>REACTIONS</u> | <u>A</u> | <u>B</u> |
|------------------|----------|----------|
| Live Load | 418 lb | 418 lb |
| Dead Load | 157 lb | 157 lb |
| Total Load | 575 lb | 575 lb |
| Bearing Length | 1.75 in | 1.75 ir |
| Web Stiffeners | No | No |

| ı | l . | | | | |
|---|---------------|-----|-----|-----|-----|
| į | | | | | |
| ı | SUPPORT LOADS | Α | | В | |
| | Live Load | | nlf | 314 | nlf |
| - | | 314 | μı | 314 | þΠ |
| ı | Dead Load | 118 | plf | 118 | plf |
| ı | Total Load | 431 | nlf | 431 | nlf |



I-JOIST PROPERTIES

SERIES 56 / 11.875 - Louisiana Pacific

Moment Cap: Base Values Adjusted

Mcap = 10170 ft-lb Cd = 1.00Maging Adjusted

Mcap' = 10170 ft-lb

Shear Stress: Vcap = 2055 lb Vcap' = 2055 lb

Cd = 1.00

Reaction A: Rcap = 1182 lb Rcap' = 1182 lb Reaction B: Rcap = 1182 lb Rcap' = 668 lb-in2 EI' = 668 lb-in2

Controlling Moment: 2251 ft-lb

7.84 Ft from left support of span 3 (Right Span) Created by combining all dead and live loads.

Controlling Shear: -575 lb

16.0 Ft from left support of span 2 (Center Span) Created by combining all dead and live loads.

 Comparisons with required sections:
 Req'd
 Provided

 E.I.:
 232 in2-lb E6
 668 in2-lb xE6

 Moment:
 2251 ft-lb
 10170 ft-lb

 Shear:
 -575 lb
 2055 lb

| JOIST DATA | Ce | nter | |
|------------------------------|-----------|-------|-----------------------------|
| | | | |
| Span Length | 15.67 | ft | |
| Unbraced Length-Top | Λ | ft | |
| Offbraced Leffgir-10p | U | 11 | |
| Unbraced Length-Bottom | 0 | ft | |
| • | | | |
| Floor sheathing applied to t | top of jo | ists- | top of joists fully braced. |
| Floor Duration Factor 1.0 | 0 | | |

| JOIST LOADING | | | | | |
|---------------------------|------|------|-----------|--|--|
| Uniform Floor Loading | | Cent | <u>er</u> | | |
| Live Load | LL = | 40 | psf | | |
| Dead Load | DL = | 15 | psf | | |
| Total Load | TL = | 55 | psf | | |
| TL Adj. For Joist Spacing | wT = | 73.3 | plf | | |

NOTES

Established Basic Permit #

19-03646

Location: JST3-6 Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 56 / 11.875 - Louisiana Pacific x 14.17 FT @ 16 O.C.

Section Adequate By: 127.5% Controlling Factor: End Reaction



page

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| DEFLECTION | <u>S</u> (| <u>Center</u> | |
|----------------|------------|----------------|---------------------------------------|
| Live Load | 0.09 | IN L/1850 | |
| Dead Load | 0.03 | in | |
| Total Load | 0.13 | IN L/1345 | |
| Live Load Defl | lection C | riteria: L/480 | Total Load Deflection Criteria: L/360 |

| REACTIONS | Α | B | |
|----------------|---------|---------|---|
| | | _ | |
| Live Load | 378 lb | 378 lb | 1 |
| | | | |
| Dead Load | 142 lb | 142 lb | 1 |
| | | | |
| Total Load | 520 lb | 520 lb | 1 |
| 1 | | | |
| Bearing Length | 1.75 in | 1.75 in | |
| 1 " | | | |
| Web Stiffeners | No | No | |
| | | | |

| SUPPORT | LOADS | 1 | | <u>B</u> | |
|------------|-------|-----|-----|----------|-----|
| Live Load | 28 | l p | olf | 284 | plf |
| Dead Load | I 10 | 7 p | olf | 107 | plf |
| Total Load | 39 |) p | olf | 390 | plf |



SERIES 56 / 11.875 - Louisiana Pacific

<u>Base Values</u> <u>Adjusted</u>

Moment Cap: Mcap = 10170 ft-lb Mcap' = 10170 ft-lb

Cd = 1.00

Shear Stress: Vcap = 2055 lb Vcap' = 2055 lb

Cd = 1.00

Reaction A: Rcap = 1182 lb Rcap' = 1182 lb Reaction B: Rcap = 1182 lb Rcap' =

Controlling Moment: 1841 ft-lb

7.09 Ft from left support of span 3 (Right Span) Created by combining all dead and live loads.

Controlling Shear: 520 lb

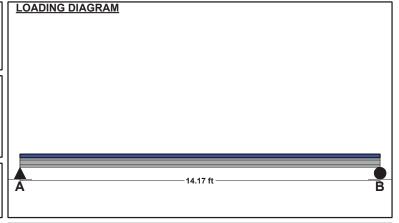
0.0 Ft from left support of span 2 (Center Span) Created by combining all dead and live loads.

 Comparisons with required sections:
 Req'd
 Provided

 E.I.:
 179 in2-lb E6
 668 in2-lb xE6

 Moment:
 1841 ft-lb
 10170 ft-lb

 Shear:
 520 lb
 2055 lb



| JOIST DATA | <u>C</u> e | <u>enter</u> |
|----------------------------|------------|-----------------------------------|
| Span Length | 14.17 | ft |
| Unbraced Length-Top | 0 |) ft |
| Unbraced Length-Bottom | 0 |) ft |
| Floor sheathing applied to | top of jo | oists-top of joists fully braced. |
| Floor Duration Factor 1.0 | 00 | |

| JOIST LOADING | | | | - |
|---------------------------|------|-------------|-----|---|
| Uniform Floor Loading | | <u>Cent</u> | er | |
| Live Load | LL = | 40 | psf | |
| Dead Load | DL = | 15 | psf | |
| Total Load | TL = | 55 | psf | |
| TL Adj. For Joist Spacing | wT = | 73.3 | plf | |

NOTES

Established Basic Permit #

19-03646

Location: MLB3-2

Multi-Loaded Multi-Span Beam

[2015 International Building Code(2015 NDS)]

3.5 IN x 6.0 IN x 5.33 FT

24F-V4 - Visually Graded Western Species - Dry Use

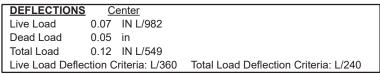
Section Adequate By: 59.5% Controlling Factor: Moment





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| REACTIONS | <u>A</u> | | <u>B</u> | |
|----------------|----------|----|----------|----|
| Live Load | 1062 | lb | 1038 | lb |
| Dead Load | 809 | lb | 760 | lb |
| Total Load | 1871 | lb | 1798 | lb |
| Bearing Length | 0.82 | in | 0.79 | in |

| BEAM DATA | <u>Ce</u> | <u>Center</u> | |
|---------------------------|-----------|---------------|--|
| Span Length | 5.33 | ft | |
| Unbraced Length-Top | 0 | ft | |
| Unbraced Length-Bottom | 5.33 | ft | |
| Live Load Duration Factor | 1.00 | | |
| Camber Adj. Factor | 1.5 | | |
| Camber Required | 0.08 | | |
| Notch Depth | 0.00 | | |

MATERIAL PROPERTIES

24F-V4 - Visually Graded Western Species

| | <u>Base v</u> | <u>raiues</u> | <u>Adjt</u> | <u>istea</u> |
|------------------------------|---------------|---------------|-------------|--------------|
| Bending Stress: | Fb = | 2400 psi | Controlle | d by: |
| | Fb_cmpr = | 1850 psi | Fb' = | 2400 psi |
| | Cd=1.00 | | | |
| Shear Stress: | Fv = | 265 psi | Fv' = | 265 psi |
| | Cd=1.00 | | | |
| Modulus of Elasticity: | E = | 1800 ksi | E' = | 1800 ksi |
| Comp. [⊥] to Grain: | Fc - | 650 psi | Fc - 上' = | 650 psi |

Controlling Moment: 2633 ft-lb 2.4 Ft from left support of span 2 (Center Span)

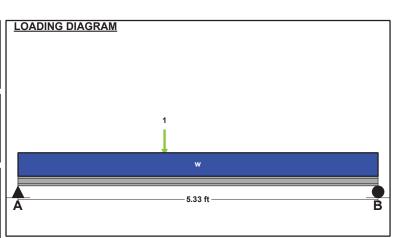
Created by combining all dead loads and live loads on span(s) 2

Controlling Shear: 1577 lb

At a distance d from left support of span 2 (Center Span)

Created by combining all dead loads and live loads on $\mbox{\rm span}(s)\,2$

| Comparisons with required sections: | Req'd | <u>Provided</u> |
|-------------------------------------|------------|-----------------|
| Section Modulus: | 13.17 in3 | 21 in3 |
| Area (Shear): | 8.93 in2 | 21 in2 |
| Moment of Inertia (deflection): | 27.54 in4 | 63 in4 |
| Moment: | 2633 ft-lb | 4200 ft-lb |
| Shear: | 1577 lb | 3710 lb |
| | | |



| UNIFORM LOADS | <u>C</u> | enter* | |
|----------------------|----------|--------|------------------------------------|
| Uniform Live Load | 369 | plf | |
| Uniform Dead Load | 240 | plf | |
| Beam Self Weight | 5 | plf | |
| Total Uniform Load | 614 | plf | |
| * Load obtained from | Load | Tracke | r. See Summary Report for details. |

POINT LOADS - CENTER SPAN

Load NumberOneLive Load133 lbDead Load266 lbLocation2.17 ft

A dimeted

* Load obtained from Load Tracker. See Summary Report for details.

NOTES

Established Basic Permit #

19-03646

Wall

[2015 International Building Code(2015 NDS)]

1.5 IN x 5.5 IN x 8.08 FT @ 16 O.C. #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 87.5%

Controlling Factor: Combined Stress Factor



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DEFLECTIONS

Deflection due to lateral loads only: Defl = 0.06 IN = L/1638 Live Load Deflection Criteria: L/180

VERTICAL REACTIONS

 Live Load:
 Vert-LL-Rxn =
 0 lb

 Dead Load:
 Vert-DL-Rxn =
 119 lb

 Total Load:
 Vert-TL-Rxn =
 119 lb

HORIZONTAL REACTIONS

Total Reaction at Top of Column: TL-Rxn-Top = 83 lb Total Reaction at Bottom of Column: TL-Rxn-Bottom = 83 lb

WALL DATA

STUD PROPERTIES

#2 - Douglas-Fir-Larch

Base Values Adjusted

Compressive Stress: Fc = 1350 psi Fc' = 1254 psi

Cd=1.60 Cf=1.10 Cp=0.53

Bending Stress (X-X Axis): Fbx = 900 psi Fbx' = 2153 psi Cd=1.60 CF=1.30 Cr=1.15 Cl=1.00

Bending Stress (Y-Y Axis): Fby = 900 psi Fby' = 2153 psi

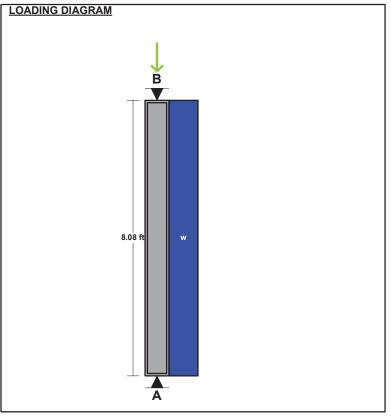
Cd=1.60 CF=1.30 Cr=1.15

Modulus of Elasticity: E = 1600 ksi E' = 1600 ksi

| Stud Section (X-X Axis): | dx = | 5.5 | in |
|-----------------------------|----------|-------|-----|
| Stud Section (Y-Y Axis): | dy = | 1.5 | in |
| Area: | A = | 8.25 | in2 |
| Section Modulus (X-X Axis): | Sx = | 7.56 | in3 |
| Section Modulus (Y-Y Axis): | Sy = | 2.06 | in3 |
| Slenderness Ratio: | Lex/dx = | 17.63 | |
| | Ley/dy = | 0 | |

Stud Calculations (Controlling Case Only):

Controlling Load Case: Axial Dead Load and Lateral loads (D + W or E) **Actual Compressive Stress:** Fc = 14 psi Allowable Compressive Stress: Fc' = 1254 psi Eccentricity Moment (X-X Axis): Mx-ex = 0 ft-lb Eccentricity Moment (Y-Y Axis): My-ey = 0 ft-lb Moment Due to Lateral Loads (X-X Axis): Mx =168 ft-lb Moment Due to Lateral Loads (Y-Y Axis): My = 0 ft-lb Bending Stress Lateral Loads Only (X-X Axis): Fbx = 266 psi Allowable Bending Stress (X-X Axis): Fbx' = 2153 psi Bending Stress Lateral Loads Only (Y-Y Axis): Fby = 0 psi Allowable Bending Stress (Y-Y Axis): Fby' = 2153 psi **Combined Stress Factor:** CSF = 0.12



WALL LOAD CALCULATOR

Tributary Width Live Load Dead Load Load Tracker: 0 plf DL = 0 plf LL = Roof: 0 ft 25 psf DL = 15 psf TA = Upper Floor: 40 psf DL = 15 psf TA = 0 ft Upper Floor Height: 0 ft Middle Floor: 40 psf DL = 0 ft II =15 psf TA = Middle Floor Height: 0 ft

Calculated Load: LL = 0 plf DL = 88.9 plf

AXIAL LOADING

 Live Load:
 PL =
 0 plf *

 Dead Load:
 PD =
 89 plf *

 Total Axial Load:
 PT =
 89 plf

* Load obtained from Load Tracker. See Summary Report for details.

LATERAL LOADING (Dy Face)
Uniform Lateral Load: wL-Lat = 15 psf

NOTES

Established Basic Permit #

19-03646

Wall

[2015 International Building Code(2015 NDS)]

1.5 IN x 5.5 IN x 8.08 FT @ 16 O.C. #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 95.1%

Controlling Factor: Combined Stress Factor





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DEFLECTIONS

Deflection due to lateral loads only: Defl = 0.02 IN = L/5046 Live Load Deflection Criteria: L/180

VERTICAL REACTIONS

 Live Load:
 Vert-LL-Rxn =
 0 lb

 Dead Load:
 Vert-DL-Rxn =
 119 lb

 Total Load:
 Vert-TL-Rxn =
 119 lb

HORIZONTAL REACTIONS

Total Reaction at Top of Column: TL-Rxn-Top = 27 lb
Total Reaction at Bottom of Column: TL-Rxn-Bottom = 27 lb

WALL DATA

Total Stud Length:

Wall Dead Weight:

Unbraced Length (X-Axis) Lx:

Unbraced Length (Y-Axis) Ly:

Stud End Condition-K (e):

Axial Load Duration Factor

Lateral Load Duration Factor (Wind/Seismic)

8.08 ft

9.08 ft

1.10 ft

1.

STUD PROPERTIES

#2 - Douglas-Fir-Larch

Base Values Adjusted

Compressive Stress: Fc = 1350 psi Fc' = 1182 psi

 $Cd=1.33 \ Cf=1.10 \ Cp=0.60$ Bending Stress (X-X Axis): Fbx = 900 psi Fbx' = 1790 psi

Cd=1.33 CF=1.30 Cr=1.15 Cl=1.00

Bending Stress (Y-Y Axis): Fby = 900 psi Fby' = 1790 psi

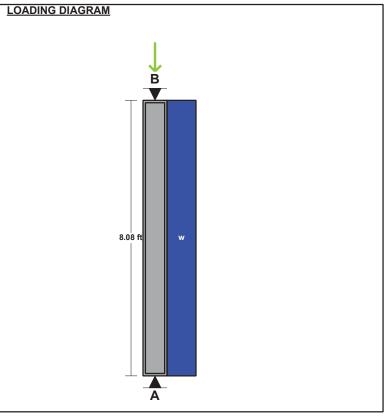
Cd=1.33 CF=1.30 Cr=1.15

Modulus of Elasticity: E = 1600 ksi E' = 1600 ksi

Stud Section (X-X Axis): dx =5.5 in Stud Section (Y-Y Axis): dy =1.5 in Area: A = 8.25 in2 Section Modulus (X-X Axis): Sx =7.56 in3 Section Modulus (Y-Y Axis): Sy = 2.06 in3 Slenderness Ratio: Lex/dx = 17.63Ley/dy =

Stud Calculations (Controlling Case Only):

Controlling Load Case: Axial Dead Load and Lateral loads (D + W or E) Actual Compressive Stress: Fc = 14 psi Allowable Compressive Stress: Fc' = 1182 psi Eccentricity Moment (X-X Axis): Mx-ex = 0 ft-lb Eccentricity Moment (Y-Y Axis): My-ey = 0 ft-lb Moment Due to Lateral Loads (X-X Axis): ft-lb Mx =54 Moment Due to Lateral Loads (Y-Y Axis): My = 0 ft-lb Bending Stress Lateral Loads Only (X-X Axis): Fbx = 86 psi Allowable Bending Stress (X-X Axis): Fbx' = 1790 psi Bending Stress Lateral Loads Only (Y-Y Axis): Fby = 0 psi Allowable Bending Stress (Y-Y Axis): Fby' = 1790 psi **Combined Stress Factor:** CSF = 0.05



WALL LOAD CALCULATOR

Tributary Width Live Load Dead Load Load Tracker: 0 plf DL = 0 plf LL = Roof: 0 ft 25 psf DL = 15 psf TA = Upper Floor: 40 psf DL = 15 psf TA = 0 ft Upper Floor Height: 0 ft Middle Floor: 40 psf DL = TA = 0 ft II =15 psf Middle Floor Height: 0 ft

Calculated Load: LL = 0 plf DL = 88.9 plf

AXIAL LOADING

Live Load: PL = 0 plf *
Dead Load: PD = 89 plf *
Total Axial Load: PT = 89 plf

* Load obtained from Load Tracker. See Summary Report for details.

LATERAL LOADING (Dy Face)
Uniform Lateral Load: wL-Lat = 5 psf

NOTES

Established Basic Permit #

19-03646

Wall

[2015 International Building Code(2015 NDS)]

1.5 IN x 5.5 IN x 8.08 FT @ 16 O.C. #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 95.1%

Controlling Factor: Combined Stress Factor





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DEFLECTIONS

Deflection due to lateral loads only: Defl = 0.02 IN = L/5046 Live Load Deflection Criteria: L/180

VERTICAL REACTIONS

 Live Load:
 Vert-LL-Rxn =
 0 lb

 Dead Load:
 Vert-DL-Rxn =
 108 lb

 Total Load:
 Vert-TL-Rxn =
 108 lb

HORIZONTAL REACTIONS

Total Reaction at Top of Column: TL-Rxn-Top = 27 lb
Total Reaction at Bottom of Column: TL-Rxn-Bottom = 27 lb

WALL DATA

Total Stud Length:

Wall Dead Weight:
Unbraced Length (X-Axis) Lx:
Unbraced Length (Y-Axis) Ly:
Stud End Condition-K (e):
Axial Load Duration Factor
Lateral Load Duration Factor (Wind/Seismic)

8.08 ft

the psf
the

STUD PROPERTIES

#2 - Douglas-Fir-Larch

Bending Stress (X-X Axis): Fbx = 900 psi Fbx' = 1790 psi

Cd=1.33 CF=1.30 Cr=1.15 Cl=1.00

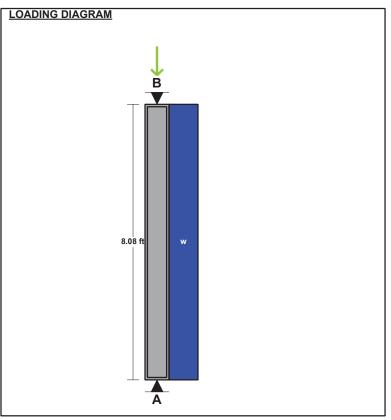
Bending Stress (Y-Y Axis): Fby = 900 psi Fby' = 1790 psi Cd=1.33 CF=1.30 Cr=1.15

Modulus of Elasticity: E = 1600 ksi E' = 1600 ksi

Stud Section (X-X Axis): dx =5.5 in Stud Section (Y-Y Axis): dy =1.5 in Area: A = 8.25 in2 Section Modulus (X-X Axis): Sx =7.56 in3 Section Modulus (Y-Y Axis): Sy = 2.06 in3 Slenderness Ratio: Lex/dx = 17.63Ley/dy =

Stud Calculations (Controlling Case Only):

Controlling Load Case: Axial Dead Load and Lateral loads (D + W or E) Actual Compressive Stress: Fc = 13 psi Allowable Compressive Stress: Fc' = 1182 psi Eccentricity Moment (X-X Axis): Mx-ex = 0 ft-lb Eccentricity Moment (Y-Y Axis): My-ey = 0 ft-lb Moment Due to Lateral Loads (X-X Axis): ft-lb Mx =54 Moment Due to Lateral Loads (Y-Y Axis): My = 0 ft-lb Bending Stress Lateral Loads Only (X-X Axis): Fbx = 86 psi Allowable Bending Stress (X-X Axis): Fbx' = 1790 psi Bending Stress Lateral Loads Only (Y-Y Axis): Fby = 0 psi Allowable Bending Stress (Y-Y Axis): Fby' = 1790 psi **Combined Stress Factor:** CSF = 0.05



WALL LOAD CALCULATOR

Tributary Width Live Load Dead Load Load Tracker: 0 plf DL = 0 plf LL = Roof: 0 ft 25 psf DL = 15 psf TA = Upper Floor: 40 psf DL = 15 psf TA = 0 ft Upper Floor Height: 0 ft Middle Floor: 40 psf DL = TA = 0 ft II =15 psf Middle Floor Height: 0 ft

Calculated Load: LL = 0 plf DL = 80.8 plf

AXIAL LOADING

 Live Load:
 PL =
 0 plf *

 Dead Load:
 PD =
 81 plf *

 Total Axial Load:
 PT =
 81 plf

* Load obtained from Load Tracker. See Summary Report for details.

LATERAL LOADING (Dy Face)
Uniform Lateral Load: wL-Lat = 5 psf

NOTES

Established Basic Permit #

19-03646

Location: JST3-7 Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 18 / 11.875 - Louisiana Pacific x 10.75 FT @ 16 O.C.

Section Adequate By: 125.0% Controlling Factor: End Reaction





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| REACTIONS | <u>A</u> | | <u>B</u> | |
|------------------|----------|----|----------|----|
| Live Load | 287 | lb | 287 | lb |
| Dead Load | 108 | lb | 108 | lb |
| Total Load | 395 | lb | 395 | lb |
| Bearing Length | 1.75 | in | 1.75 | in |
| Web Stiffeners | No | | No | |

| SUPPORT LOADS | <u>A</u> | | <u>B</u> | |
|---------------|----------|-----|----------|-----|
| Live Load | 215 | plf | 215 | plf |
| Dead Load | 81 | plf | 81 | plf |
| Total Load | 296 | plf | 296 | plf |



SERIES 18 / 11.875 - Louisiana Pacific

 $\frac{\text{Base Values}}{\text{Moment Cap:}} \qquad \frac{\text{Adjusted}}{\text{Mcap = 3100 ft-lb}} \\ \frac{\text{Adjusted}}{\text{Mcap' = 3100 ft-lb}}$

Cd = 1.00

Shear Stress: Vcap = 1335 lb Vcap' = 1335 lb

Cd = 1.00

 Reaction A:
 Rcap = 887 lb
 Rcap' = 887 lb

 Reaction B:
 Rcap = 887 lb
 Rcap' = 887 lb

 E.I.:
 EI = 248 lb-in2
 EI' = 248 lb-in2

Controlling Moment: 1059 ft-lb

5.38 Ft from left support of span 3 (Right Span) Created by combining all dead and live loads.

Controlling Shear: 394 lb

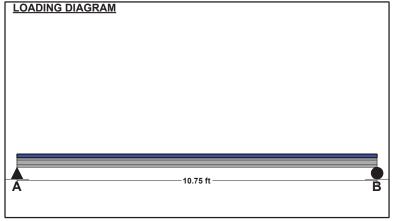
0.0 Ft from left support of span 2 (Center Span) Created by combining all dead and live loads.

 Comparisons with required sections:
 Req'd
 Provided

 E.I.:
 75 in2-lb E6
 248 in2-lb xE6

 Moment:
 1059 ft-lb
 3100 ft-lb

 Shear:
 394 lb
 1335 lb



| JOIST DATA | <u>Ce</u> | <u>enter</u> | |
|----------------------------|-----------|-----------------------------------|--|
| Span Length | 10.75 | ft | |
| Unbraced Length-Top | 0 | ft | |
| Unbraced Length-Bottom | 0 | ft | |
| Floor sheathing applied to | top of jo | oists-top of joists fully braced. | |
| Floor Duration Factor 1.0 | 00 | | |

| JOIST LOADING | | | |
|------------------------------|------|------|-----|
| Uniform Floor Loading | | Cent | er |
| Live Load | LL = | 40 | psf |
| Dead Load | DL = | 15 | psf |
| | | | |

Total Load TL = 55 psf TL Adj. For Joist Spacing wT = 73.3 plf

NOTES

Established Basic Permit #

19-03646

Location: MLB3-3

Multi-Loaded Multi-Span Beam

[2015 International Building Code(2015 NDS)]

1.75 IN x 11.25 IN x 6.5 FT (4.8 + 1.8) LSL 1730 Fb-1.35E - Louisiana Pacific

Section Adequate By: 330.4% Controlling Factor: Moment





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| DEFLECTIONS | <u> </u> | <u>Center</u> | | Right |
|-----------------|----------|----------------|-------|------------------------------------|
| Live Load | 0.01 | IN L/5695 | 0.01 | IN 2L/3430 |
| Dead Load | 0.00 | in | 0.01 | in |
| Total Load | 0.01 | IN L/6066 | 0.02 | IN 2L/2132 |
| Live Load Defle | ction C | riteria: L/360 |) Tot | al Load Deflection Criteria: L/240 |

| REACTIONS | <u>A</u> | | <u>B</u> | |
|------------------|----------|----|----------|----|
| Live Load | 582 | lb | 1036 | lb |
| Dead Load | 118 | lb | 739 | lb |
| Total Load | 700 | lb | 1775 | lb |
| Uplift (1.5 F.S) | -33 | lb | 0 | lb |
| Bearing Length | 0.53 | in | 1.35 | in |

| BEAM DATA | <u>Ce</u> | nter | R | ight |
|---------------------------|-----------|------|------|------|
| Span Length | 4.75 | ft | 1.75 | ft |
| Unbraced Length-Top | 0 | ft | 0 | ft |
| Unbraced Length-Bottom | 4.75 | ft | 1.75 | ft |
| Live Load Duration Factor | 1.00 | | | |
| Notch Depth | 0.00 | | | |

MATERIAL PROPERTIES

LSL 1730 Fb-1.35E - Louisiana Pacific

| Bending Stress: | Fb = | 1730 psi | Fb' = | 1485 psi |
|------------------------------|----------|--------------|-----------|----------|
| | Cd=1.00 |) CI=0.85 CF | =1.01 | |
| Shear Stress: | Fv = | 410 psi | Fv' = | 410 psi |
| | Cd=1.00 |) | | |
| Modulus of Elasticity: | E = | 1350 ksi | E' = | 1350 ksi |
| Comp. [⊥] to Grain: | Fc - ⊥ = | 750 psi | Fc - 上' = | 750 psi |

Base Values

<u>Adjusted</u>

Controlling Moment: -1061 ft-lb Over right support of span 2 (Center Span)

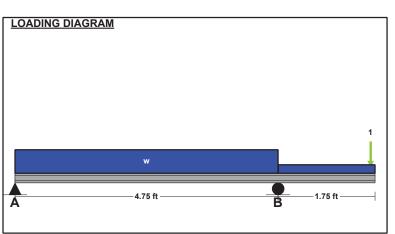
Created by combining all dead loads and live loads on span(s) 3

Controlling Shear: -727 lb

At a distance d from right support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2, 3

| Comparisons with required sections: | Req'd | <u>Provided</u> |
|-------------------------------------|-------------|-----------------|
| Section Modulus: | 8.58 in3 | 36.91 in3 |
| Area (Shear): | 2.66 in2 | 19.69 in2 |
| Moment of Inertia (deflection): | 23.38 in4 | 207.64 in4 |
| Moment: | -1061 ft-lb | 4567 ft-lb |
| Shear: | -727 lb | 5381 lb |



| UNIFORM LOADS | <u>C</u> | ente | r* | Right |
|----------------------|----------|------|---------|--------------------------------|
| Uniform Live Load | 245 | plf | 30 | plf |
| Uniform Dead Load | 91 | plf | 90 | plf |
| Beam Self Weight | 6 | plf | 6 | plf |
| Total Uniform Load | 342 | plf | 126 | plf |
| * Load obtained from | Load | Trac | ker. Se | ee Summary Report for details. |

| POINT LOAD: | <u>S - RIGHT</u> | SPAN |
|-------------|------------------|------|
| Load Number | <u>One</u> | |
| Live Load | 290 lb | |
| Dead Load | 230 lb | |
| Location | 1 67 ft | |

NOTES

Established Basic Permit #

19-03646

Location: JST3-8 Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 56 / 11.875 - Louisiana Pacific x 6.33 FT (4.6 + 1.8) @ 16 O.C.

Section Adequate By: 13.7% Controlling Factor: End Reaction

| DEFLECTIONS | <u>C</u> | <u>enter</u> | | Right |
|--------------------|----------|----------------|-------|---------------------------------|
| Live Load | -0.02 | IN L/3593 | -0.01 | IN 2L/2810 |
| Dead Load | -0.01 | in | -0.01 | in |
| Total Load | -0.03 | IN L/2040 | -0.03 | IN 2L/1584 |
| Live Load Deflect | ction Cr | riteria: L/480 | Tota | Load Deflection Criteria: L/360 |

| DEACTIONS | | | | |
|------------------|----------|----|----------|----|
| <u>REACTIONS</u> | <u>A</u> | | <u>B</u> | |
| Live Load | 122 | lb | 1018 | lb |
| Dead Load | -130 | lb | 721 | lb |
| Total Load | -8 | lb | 1739 | lb |
| Uplift (1.5 F.S) | -357 | lb | 0 | lb |
| Bearing Length | 3.50 | in | 3.50 | in |
| Web Stiffeners | Yes | | Yes | |

| SUPPORT LOADS | <u>A</u> | | <u>B</u> | |
|---------------|----------|-----|----------|-----|
| Live Load | 92 | plf | 764 | plf |
| Dead Load | -98 | plf | 541 | plf |
| Total Load | -6 | plf | 1304 | plf |

I-JOIST PROPERTIES

SERIES 56 / 11.875 - Louisiana Pacific

Cd = 1.00

Shear Stress: Vcap = 2055 lb Vcap' = 2055 lb Cd = 1.00

Reaction A: Rcap = 1976 lb Rcap' = 1976 lb Reaction B: Rcap = 1976 lb Rcap' = 1976 lb E.l.: EI = 668 lb-in2 EI' = 668 lb-in2

Controlling Moment: -1847 ft-lb

4.58 Ft from left support of span 3 (Right Span) Created by combining all dead and live loads.

Controlling Shear: 1167 lb

 $0.0\ Ft$ from left support of span 3 (Right Span) Created by combining all dead and live loads.

 Comparisons with required sections:
 Req'd
 Provided

 E.I.:
 152 in2-lb E6
 668 in2-lb xE6

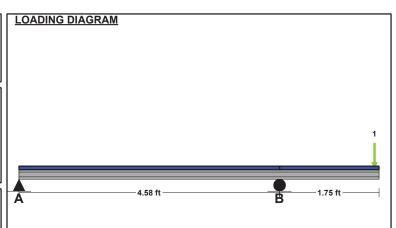
 Moment:
 -1847 ft-lb
 10170 ft-lb

 Shear:
 1167 lb
 2055 lb



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| JOIST DATA | Ce | nter | Ri | ight | |
|-----------------------------|----------|-------|---------|---------|------------------|
| | | | | _ | |
| Span Length | 4.58 | ft | 1.75 | ft | |
| | | - | _ | - | |
| Unbraced Length-Top | 0 | ft | 0 | ft | |
| Unbraced Length-Bottom | Λ | ft | 0 | ft | |
| Offibraced Lerigin-Bolloffi | U | 11 | U | 11 | |
| Floor sheathing applied to | top of i | oists | -top of | f joist | ts fully braced. |
| Floor Duration Factor 1.0 | · ΄ ΄ | | | • | • |
| Floor Duration Factor 1.0 | 10 | | | | |

| JOIST LOADING | | | | | |
|------------------------------------|--------|-------------|-----------|------|------------|
| Uniform Floor Loading | | <u>Cent</u> | <u>er</u> | Rig | <u>ıht</u> |
| Live Load | LL = | 40 | psf | 40 | psf |
| Dead Load | DL = | 15 | psf | 15 | psf |
| Total Load | TL = | 55 | psf | 55 | psf |
| TL Adj. For Joist Spacin | g wT = | 73.3 | plf | 73.3 | plf |
| Wall Loading | | | | | |
| Wall One | | | | | |
| Live Load ([⊥] to Joists | | 0 | plf | 431 | plf |
| Dead Load ([⊥] to Joist | s)D1 = | 0 | plf | 348 | plf |
| Load Location | X1 = | 0 | ft | 1.67 | ft |

NOTES

Established Basic Permit #

19-03646

Location: MLB3-4

Multi-Loaded Multi-Span Beam

[2015 International Building Code(2015 NDS)]

3.5 IN x 11.875 IN x 17.83 FT

LSL 2360 Fb-1.55E - Louisiana Pacific

Section Adequate By: 48.1% Controlling Factor: Deflection





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| DEFLECTIONS | <u>C</u> | <u>enter</u> | |
|-----------------|----------|----------------|---------------------------------------|
| Live Load | 0.40 | IN L/533 | |
| Dead Load | 0.03 | in | |
| Total Load | 0.43 | IN L/501 | |
| Live Load Defle | ection C | riteria: L/360 | Total Load Deflection Criteria: L/240 |

| REACTIONS | <u>A</u> | | <u>B</u> | |
|------------------|----------|----|----------|----|
| Live Load | 833 | lb | 1345 | lb |
| Dead Load | 195 | lb | -199 | lb |
| Total Load | 1028 | lb | 1146 | lb |
| Uplift (1.5 F.S) | 0 | lb | -199 | lb |
| Bearing Length | 0.34 | in | 0.37 | in |

| | BEAM DATA | <u>Ce</u> | nter | |
|---|---------------------------|-----------|------|--|
| ; | Span Length | 17.83 | ft | |
| | Unbraced Length-Top | 0 | ft | |
| | Unbraced Length-Bottom | 17.83 | ft | |
| | Live Load Duration Factor | 1.00 | | |
| L | Notch Depth | 0.00 | | |

MATERIAL PROPERTIES

LSL 2360 Fb-1.55E - Louisiana Pacific

Base Values **Adjusted** Bending Stress: Fb = 2360 psi Fb' = 2364 psi Cd=1.00 CF=1.00 Shear Stress: 410 psi Fv = 410 psi Cd=1.00 Modulus of Elasticity: E = 1550 ksi E' = 1550 ksi Comp. \perp to Grain: Fc - \perp = 875 psi $Fc - \bot' = 875 \text{ psi}$

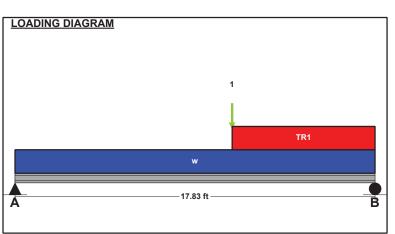
Controlling Moment: 6131 ft-lb 10.7 Ft from left support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2

Controlling Shear: -1076 lb

At a distance d from right support of span 2 (Center Span) Created by combining all dead loads and live loads on span(s) 2

| Comparisons with required sections: | Req'd | <u>Provided</u> |
|-------------------------------------|------------|-----------------|
| Section Modulus: | 31.13 in3 | 82.26 in3 |
| Area (Shear): | 3.94 in2 | 41.56 in2 |
| Moment of Inertia (deflection): | 329.87 in4 | 488.41 in4 |
| Moment: | 6131 ft-lb | 16202 ft-lb |
| Shear: | -1076 lb | 11360 lb |



| UNIFORM LOADS | <u>C</u> e | <u>enter</u> |
|--------------------|------------|--------------|
| Uniform Live Load | 53 | plf |
| Uniform Dead Load | 20 | plf |
| Beam Self Weight | 12 | plf |
| Total Uniform Load | 85 | plf |

POINT LOADS - CENTER SPAN

Load Number One *
Live Load 582 lb
Dead Load 118 lb
Location 10.75 ft

* Load obtained from Load Tracker. See Summary Report for details.

TRAPEZOIDAL LOADS - CENTER SPAN

Load Number One ' Left Live Load 92 plf -98 plf Left Dead Load Right Live Load 92 plf Right Dead Load -98 plf Load Start 10.75 ft Load End 17.83 ft 7.08 ft Load Length

NOTES

Established Basic Permit #

19-03646

Load obtained from Load Tracker. See Summary Report for details.

Wall

[2015 International Building Code(2015 NDS)]

1.5 IN x 5.5 IN x 8.08 FT @ 16 O.C. #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 87.5%

Controlling Factor: Combined Stress Factor



of

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DEFLECTIONS

Deflection due to lateral loads only: Defl = 0.06 IN = L/1638 Live Load Deflection Criteria: L/180

VERTICAL REACTIONS

 Live Load:
 Vert-LL-Rxn =
 0 lb

 Dead Load:
 Vert-DL-Rxn =
 119 lb

 Total Load:
 Vert-TL-Rxn =
 119 lb

HORIZONTAL REACTIONS

Total Reaction at Top of Column: TL-Rxn-Top = 83 lb Total Reaction at Bottom of Column: TL-Rxn-Bottom = 83 lb

WALL DATA

Total Stud Length:

Wall Dead Weight:
Unbraced Length (X-Axis) Lx:
Unbraced Length (Y-Axis) Ly:
Stud End Condition-K (e):
Axial Load Duration Factor
Lateral Load Duration Factor (Wind/Seismic)

8.08 ft
ft
0 ft
11.00 ft
12.00 ft
13.00 ft
14.00 ft
15.00 ft
16.00 ft

STUD PROPERTIES

#2 - Douglas-Fir-Larch

Base Values Adjusted

Compressive Stress: Fc = 1350 psi Fc' = 1254 psi

Cd=1.60 Cf=1.10 Cp=0.53

Bending Stress (X-X Axis): Fbx = 900 psi Fbx' = 2153 psi Cd=1.60 CF=1.30 Cr=1.15 Cl=1.00

Bending Stress (Y-Y Axis): Fby = 900 psi Fby' = 2153 psi

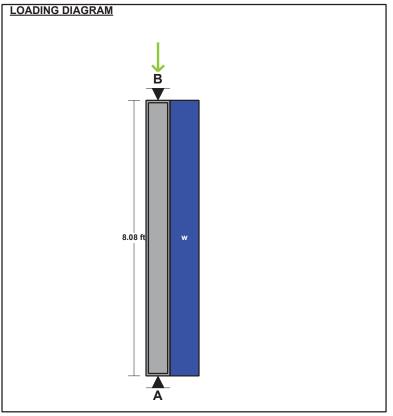
Cd=1.60 CF=1.30 Cr=1.15

Modulus of Elasticity: E = 1600 ksi E' = 1600 ksi

| Stud Section (X-X Axis): | dx = | 5.5 | in |
|-----------------------------|----------|-------|-----|
| Stud Section (Y-Y Axis): | dy = | 1.5 | in |
| Area: | A = | 8.25 | in2 |
| Section Modulus (X-X Axis): | Sx = | 7.56 | in3 |
| Section Modulus (Y-Y Axis): | Sy = | 2.06 | in3 |
| Slenderness Ratio: | Lex/dx = | 17.63 | |
| | Ley/dy = | 0 | |

Stud Calculations (Controlling Case Only):

Controlling Load Case: Axial Dead Load and Lateral loads (D + W or E) **Actual Compressive Stress:** Fc = 14 psi Allowable Compressive Stress: Fc' = 1254 psi Eccentricity Moment (X-X Axis): Mx-ex = 0 ft-lb Eccentricity Moment (Y-Y Axis): My-ey = 0 ft-lb Moment Due to Lateral Loads (X-X Axis): Mx =168 ft-lb Moment Due to Lateral Loads (Y-Y Axis): My = 0 ft-lb Bending Stress Lateral Loads Only (X-X Axis): Fbx = 266 psi Allowable Bending Stress (X-X Axis): Fbx' = 2153 psi Bending Stress Lateral Loads Only (Y-Y Axis): Fby = 0 psi Allowable Bending Stress (Y-Y Axis): Fby' = 2153 psi **Combined Stress Factor:** CSF = 0.12



WALL LOAD CALCULATOR

Tributary Width Live Load Dead Load Load Tracker: 0 plf DL = 0 plf LL = Roof: 0 ft 25 psf DL = 15 psf TA = Upper Floor: 40 psf DL = 15 psf TA = 0 ft Upper Floor Height: 0 ft 40 psf DL = TA = 0 ft Middle Floor: II =15 psf Middle Floor Height: 0 ft

0 plf DL = 88.9 plf

AXIAL LOADING

Calculated Load:

 Live Load:
 PL =
 0 plf *

 Dead Load:
 PD =
 89 plf *

 Total Axial Load:
 PT =
 89 plf

* Load obtained from Load Tracker. See Summary Report for details.

LL =

LATERAL LOADING (Dy Face)
Uniform Lateral Load: wL-Lat = 15 psf

NOTES

Established Basic Permit #

19-03646

Location: MLB3-5

Multi-Loaded Multi-Span Beam

[2015 International Building Code(2015 NDS)]

3.5 IN x 6.0 IN x 5.33 FT

24F-V4 - Visually Graded Western Species - Dry Use

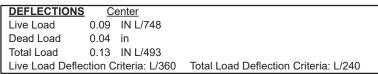
Section Adequate By: 42.7% Controlling Factor: Moment





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| <u>REACTIONS</u> | <u>A</u> | | <u>B</u> | |
|------------------|----------|----|----------|----|
| Live Load | 1362 | lb | 1157 | lb |
| Dead Load | 715 | lb | 679 | lb |
| Total Load | 2077 | lb | 1836 | lb |
| Bearing Length | 0.91 | in | 0.81 | in |

| BEAM DATA | <u>Ce</u> | nter |
|---------------------------|-----------|------|
| Span Length | 5.33 | ft |
| Unbraced Length-Top | 0 | ft |
| Unbraced Length-Bottom | 5.33 | ft |
| Live Load Duration Factor | 1.00 | |
| Camber Adj. Factor | 1.5 | |
| Camber Required | 0.07 | |
| Notch Depth | 0.00 | |

MATERIAL PROPERTIES

24F-V4 - Visually Graded Western Species

| | <u>Base v</u> | <u>'alues</u> | | <u>Adju</u> | <u>isted</u> | |
|------------------------------|---------------|---------------|-----|-------------|--------------|-----|
| Bending Stress: | Fb = | 2400 | psi | Controlle | d by: | |
| | Fb_cmpr = | 1850 | psi | Fb' = | 2400 | psi |
| | Cd=1.00 | | | | | |
| Shear Stress: | Fv = | 265 | psi | Fv' = | 265 | psi |
| | Cd=1.00 | | | | | |
| Modulus of Elasticity: | E = | 1800 | ksi | | 1800 | ksi |
| Comp. [⊥] to Grain: | Fc - | 650 | psi | Fc - 上' = | 650 | psi |

Controlling Moment: 2944 ft-lb 2.13 Ft from left support of span 2 (Center Span)

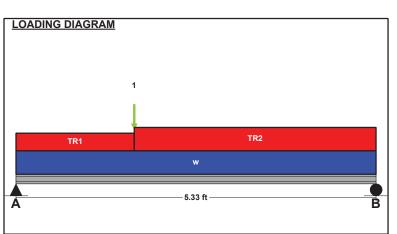
Created by combining all dead loads and live loads on span(s) 2

Controlling Shear: 1848 lb

At a distance d from left support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2

| Comparisons with required sections: | Req'd | Provided |
|-------------------------------------|------------|-----------------|
| Section Modulus: | 14.72 in3 | 21 in3 |
| Area (Shear): | 10.46 in2 | 21 in2 |
| Moment of Inertia (deflection): | 30.68 in4 | 63 in4 |
| Moment: | 2944 ft-lb | 4200 ft-lb |
| Shear: | 1848 lb | 3710 lb |



| UNIFORM LOADS | <u>C</u> | Center* | |
|----------------------|----------|---------|-----------------------------------|
| Uniform Live Load | 55 | plf | |
| Uniform Dead Load | 122 | plf | |
| Beam Self Weight | 5 | plf | |
| Total Uniform Load | 182 | plf | |
| * Load obtained from | Load | Tracker | : See Summary Report for details. |

| POINT LOAD | S - CENTE | R SPAN |
|-------------|-----------|--------|
| Load Number | One * | |
| Live Load | 833 lb | |
| Dead Load | 195 lb | |
| Location | 4 75 54 | |

| TRAPEZOIDAL I | LOADS - CENT | ER SPAN |
|----------------|---------------------|---------|
| Load Number | One * | Two * |
| Loft Live Load | 215 nlf | 281 nlf |

* Load obtained from Load Tracker. See Summary Report for details.

| Left Live Load | 215 plf | 284 plf |
|-----------------|---------|---------|
| Left Dead Load | 81 plf | 107 plf |
| Right Live Load | 215 plf | 284 plf |
| Right Dead Load | 81 plf | 107 plf |
| Load Start | 0 ft | 1.75 ft |
| Load End | 1.75 ft | 5.33 ft |
| Load Length | 1.75 ft | 3.58 ft |

^{*} Load obtained from Load Tracker. See Summary Report for details.

NOTES

Established Basic Permit #

19-03646

Wall

[2015 International Building Code(2015 NDS)]

1.5 IN x 5.5 IN x 8.08 FT @ 16 O.C. #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 87.5%

Controlling Factor: Combined Stress Factor



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DEFLECTIONS

Deflection due to lateral loads only: Defl = 0.06 IN = L/1638 Live Load Deflection Criteria: L/180

VERTICAL REACTIONS

 Live Load:
 Vert-LL-Rxn =
 0 lb

 Dead Load:
 Vert-DL-Rxn =
 119 lb

 Total Load:
 Vert-TL-Rxn =
 119 lb

HORIZONTAL REACTIONS

Total Reaction at Top of Column: TL-Rxn-Top = 83 lb Total Reaction at Bottom of Column: TL-Rxn-Bottom = 83 lb

WALL DATA

Total Stud Length:

Wall Dead Weight:
Unbraced Length (X-Axis) Lx:
Unbraced Length (Y-Axis) Ly:
Stud End Condition-K (e):

Axial Load Duration Factor
Under Stud End Condition Factor
Lateral Load Duration Factor (Wind/Seismic)

8.08 ft
8.08 ft
11 psf
11 psf
11 psf
12 psf
13 psf
14 psf
15 psf
16 psf
16 psf
16 psf
17 psf
18 p

STUD PROPERTIES

#2 - Douglas-Fir-Larch

Base Values Adjusted

Compressive Stress: Fc = 1350 psi Fc' = 1254 psi

Cd=1.60 Cf=1.10 Cp=0.53

Bending Stress (X-X Axis): Fbx = 900 psi Fbx' = 2153 psi Cd=1.60 CF=1.30 Cr=1.15 Cl=1.00

Bending Stress (Y-Y Axis): Fby = 900 psi Fby' = 2153 psi

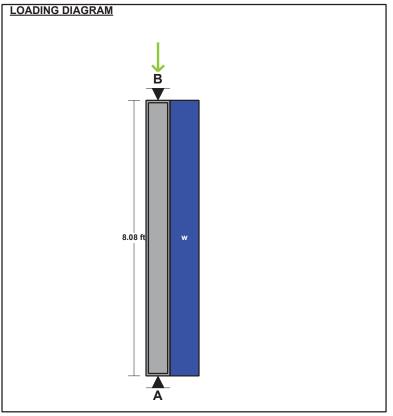
Cd=1.60 CF=1.30 Cr=1.15

Modulus of Elasticity: E = 1600 ksi E' = 1600 ksi

Stud Section (X-X Axis): dx =5.5 in Stud Section (Y-Y Axis): dy =1.5 in Area: A = 8.25 in2 Section Modulus (X-X Axis): Sx =7.56 in3 Section Modulus (Y-Y Axis): Sy = 2.06 in3 Slenderness Ratio: Lex/dx = 17.63Ley/dy =

Stud Calculations (Controlling Case Only):

Controlling Load Case: Axial Dead Load and Lateral loads (D + W or E) Actual Compressive Stress: Fc = 14 psi Allowable Compressive Stress: Fc' = 1254 psi Eccentricity Moment (X-X Axis): Mx-ex = 0 ft-lb Eccentricity Moment (Y-Y Axis): My-ey = 0 ft-lb Moment Due to Lateral Loads (X-X Axis): Mx =168 ft-lb Moment Due to Lateral Loads (Y-Y Axis): My = 0 ft-lb Bending Stress Lateral Loads Only (X-X Axis): Fbx = 266 psi Allowable Bending Stress (X-X Axis): Fbx' = 2153 psi Bending Stress Lateral Loads Only (Y-Y Axis): Fby = 0 psi Allowable Bending Stress (Y-Y Axis): Fby' = 2153 psi **Combined Stress Factor:** CSF = 0.12



WALL LOAD CALCULATOR

Tributary Width Live Load Dead Load Load Tracker: 0 plf DL = 0 plf LL = Roof: 0 ft 25 psf DL = 15 psf TA = Upper Floor: 40 psf DL = 15 psf TA = 0 ft Upper Floor Height: 0 ft Middle Floor: 40 psf DL = TA = 0 ft II =15 psf Middle Floor Height: 0 ft

Calculated Load: LL = 0 plf DL = 88.9 plf

AXIAL LOADING

 Live Load:
 PL =
 0 plf *

 Dead Load:
 PD =
 89 plf *

 Total Axial Load:
 PT =
 89 plf

* Load obtained from Load Tracker. See Summary Report for details.

LATERAL LOADING (Dy Face)
Uniform Lateral Load: wL-Lat = 15 psf

NOTES

Established Basic Permit #

19-03646

Location: JST2-2

Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 56 / 11.875 - Louisiana Pacific x 12.75 FT (11 + 1.8) @ 16 O.C.

Section Adequate By: 22.4% Controlling Factor: End Reaction

| DEFLECTIONS | <u>C</u> | <u>enter</u> | | Right |
|--------------------|----------|----------------|-------|---------------------------------|
| Live Load | 0.04 | IN L/3469 | 0.02 | IN 2L/2432 |
| Dead Load | -0.01 | in | -0.01 | in |
| Total Load | -0.04 | IN L/3621 | 0.03 | IN 2L/1564 |
| Live Load Deflec | ction Cr | riteria: L/480 | Tota | Load Deflection Criteria: L/360 |

| REACTIONS | <u>A</u> | | <u>B</u> | |
|------------------|----------|----|----------|----|
| Live Load | 293 | lb | 961 | lb |
| Dead Load | 41 | lb | 653 | lb |
| Total Load | 334 | lb | 1614 | lb |
| Uplift (1.5 F.S) | -55 | lb | 0 | lb |
| Bearing Length | 1.75 | in | 3.50 | in |
| Web Stiffeners | Yes | | Yes | |

| SUPPORT LOADS | <u>A</u> | | <u>B</u> | |
|---------------|----------|-----|----------|-----|
| Live Load | 220 | plf | 721 | plf |
| Dead Load | 31 | plf | 490 | plf |
| Total Load | 251 | plf | 1211 | plf |

I-JOIST PROPERTIES

SERIES 56 / 11.875 - Louisiana Pacific

Moment Cap: Base Values Adjusted

Mcap = 10170 ft-lb Cd = 1.00Maging Adjusted

Mcap' = 10170 ft-lb

Shear Stress: Vcap = 2055 lb Vcap' =

2055 lb

Controlling Moment: -1667 ft-lb

11.0 Ft from left support of span 3 (Right Span) Created by combining all dead and live loads.

Controlling Shear: 1059 lb

NOTES

0.0 Ft from left support of span 3 (Right Span) Created by combining all dead and live loads.

 Comparisons with required sections:
 Req'd
 Provided

 E.I.:
 154 in2-lb E6
 668 in2-lb xE6

 Moment:
 -1667 ft-lb
 10170 ft-lb

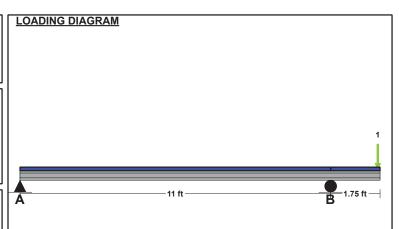
 Shear:
 1059 lb
 2055 lb



roup, Inc.

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| Ce | nter | Ri | aht | |
|-------|--------------|-----------------------------|---|--|
| | | | _ | |
| 11 | ft | 1.75 | ft | |
| _ | £. | 0 | £. | |
| U | π | U | π | |
| Ω | ft | Ο | ft | |
| 0 | 1.0 | U | 10 | |
| top c | of jois | sts-top | of jo | oists fully braced. |
| Α' | • | | • | • |
| U | | | | |
| | 11 0 0 | 0 ft 0 ft top of jois | 11 ft 1.75 0 ft 0 0 ft 0 top of joists-top | 11 ft 1.75 ft 0 ft 0 ft 0 ft 0 ft top of joists-top of jo |

| JOIST LOADING | | | | | |
|-----------------------------------|----------|------|-----------|------|-----------|
| Uniform Floor Loading | 3 | Cent | <u>er</u> | Rig | <u>ht</u> |
| Live Load | LL = | 40 | psf | 40 | psf |
| Dead Load | DL = | 15 | psf | 15 | psf |
| Total Load | TL = | 55 | psf | 55 | psf |
| TL Adj. For Joist Spaci | ing wT = | 73.3 | plf | 73.3 | plf |
| Wall Loading | | | | | |
| Wall One | | | | | |
| Live Load ([⊥] to Joist | s): L1 = | 0 | plf | 369 | plf |
| Dead Load ([⊥] to Jois | sts)D1 = | 0 | plf | 329 | plf |
| Load Location | X1 = | Ο | ft | 1 67 | ft |

Established Basic Permit #

19-03646

Location: JST2-1 Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 18 / 11.875 - Louisiana Pacific x 10.83 FT @ 16 O.C.

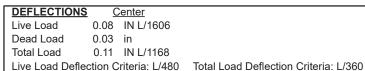
Section Adequate By: 153.3% Controlling Factor: End Reaction



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| <u>REACTIONS</u> | <u>A</u> | <u>B</u> | |
|------------------|----------|----------|----|
| Live Load | 289 lb | 289 | lb |
| Dead Load | 108 lb | 108 | lb |
| Total Load | 397 lb | 397 | lb |
| Bearing Length | 1.75 in | 3.50 | in |
| Web Stiffeners | Yes | No | |

| SUPPORT LOADS | <u>A</u> | | <u>B</u> | |
|---------------|----------|-----|----------|-----|
| Live Load | 217 | plf | 217 | plf |
| Dead Load | 81 | plf | 81 | plf |
| Total Load | 298 | plf | 298 | plf |



SERIES 18 / 11.875 - Louisiana Pacific

Moment Cap: $\frac{\text{Base Values}}{\text{Mcap = 3100 ft-lb}} \frac{\text{Adjusted}}{\text{Mcap' = 3100 ft-lb}}$ Cd = 1.00

Shear Stress: Vcap = 1335 lb Vcap' = 1335 lb

Cd = 1.00

Reaction A: Rcap = 1164 lb Rcap' = 1164 lb Reaction B: Rcap = 1006 lb Rcap' = 1006 lb E.l.: EI = 248 lb-in2 EI' = 248 lb-in2

Controlling Moment: 1075 ft-lb

5.41 Ft from left support of span 3 (Right Span) Created by combining all dead and live loads.

Controlling Shear: 397 lb

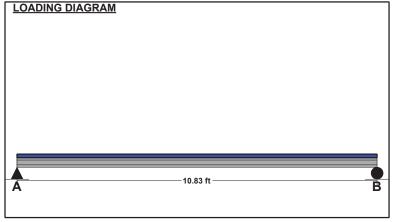
0.0 Ft from left support of span 2 (Center Span) Created by combining all dead and live loads.

 Comparisons with required sections:
 Req'd
 Provided

 E.I.:
 76 in2-lb E6
 248 in2-lb xE6

 Moment:
 1075 ft-lb
 3100 ft-lb

 Shear:
 397 lb
 1335 lb



| JOIST DATA | <u>Ce</u> | enter_ |
|----------------------------|-----------|-----------------------------------|
| Span Length | 10.83 | ft |
| Unbraced Length-Top | 0 | ft |
| Unbraced Length-Bottom | 0 | ft |
| Floor sheathing applied to | top of jo | pists-top of joists fully braced. |
| Floor Duration Factor 1. | 00 | |

JOIST LOADING

 Uniform Floor Loading
 Center

 Live Load
 LL = 40 psf

 Dead Load
 DL = 15 psf

 Total Load
 TL = 55 psf

 TL Adj. For Joist Spacing wT = 73.3 plf

NOTES

Established Basic Permit #

19-03646

Location: JST2-3 Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 18 / 11.875 - Louisiana Pacific x 6.92 FT @ 16 O.C.

Section Adequate By: 296.5% Controlling Factor: End Reaction



page

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LOADING DIAGRAM

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| ١ | DEFLECTION | <u> </u> | <u>Center</u> | |
|---|---------------|------------|----------------|---------------------------------------|
| ı | Live Load | 0.02 | IN L/4895 | |
| ı | Dead Load | 0.01 | in | |
| ı | Total Load | 0.02 | IN L/3560 | |
| ı | Live Load Def | flection C | riteria: L/480 | Total Load Deflection Criteria: L/360 |

| <u>REACTIONS</u> | <u>A</u> | | <u>B</u> | |
|------------------|----------|----|----------|----|
| Live Load | 185 | lb | 185 | lb |
| Dead Load | 69 | lb | 69 | lb |
| Total Load | 254 | lb | 254 | lb |
| Bearing Length | 1.75 | in | 3.50 | in |
| Web Stiffeners | Yes | | No | |

| SUPPORT LOADS | <u>A</u> | | <u>B</u> | |
|---------------|----------|-----|----------|-----|
| Live Load | 139 | plf | 139 | plf |
| Dead Load | 52 | plf | 52 | plf |
| Total Load | 191 | plf | 191 | plf |



Moment Cap: Mcap = 3100 ft-lb Mcap' = 3100 ft-lb Cd = 1.00

Shear Stress: Vcap = 1335 lb Vcap' = 1335 lb Cd = 1.00

Reaction A: Rcap = 1164 lb Rcap' = 1164 lb Reaction B: Rcap = 1006 lb Rcap' = 1006 lb E.l.: EI = 248 lb-in2 EI' = 248 lb-in2

Controlling Moment: 439 ft-lb 3.46 Ft from left support of span 3 (Right Span) Created by combining all dead and live loads.

Controlling Shear: 254 lb
0.0 Ft from left support of span 2 (Center Span)
Created by combining all dead and live loads.

 Comparisons with required sections:
 Req'd
 Provided

 E.I.:
 25 in2-lb E6
 248 in2-lb xE6

 Moment:
 439 ft-lb
 3100 ft-lb

 Shear:
 254 lb
 1335 lb

JOIST DATA

Span Length
6.92 ft
Unbraced Length-Top
0 ft
Unbraced Length-Bottom
0 ft
Floor sheathing applied to top of joists-top of joists fully braced.
Floor Duration Factor
1.00

6.92 ft

| JOIST LOADING | | | | |
|------------------------------|--------|------|-----|--|
| Uniform Floor Loading | | Cent | er | |
| Live Load | LL = | 40 | psf | |
| Dead Load | DL = | 15 | psf | |
| Total Load | TL = | 55 | psf | |
| TL Adi For Joist Spacino | = Tw r | 73.3 | nlf | |

NOTES

Established Basic Permit #

19-03646

Location: JST2-4 Floor Joist

[2015 International Building Code(2015 NDS)]

SERIES 18 / 11.875 - Louisiana Pacific x 3.33 FT @ 16 O.C.

Section Adequate By: 723.9% Controlling Factor: End Reaction



page

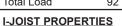
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| ١ | DEFLECTIONS | <u>s</u> c | <u>enter</u> | |
|---|-----------------|------------|----------------|---------------------------------------|
| ı | Live Load | 0.00 | IN L/MAX | |
| ı | Dead Load | 0.00 | in | |
| ı | Total Load | 0.00 | IN L/MAX | |
| ı | Live Load Defle | ection C | riteria: L/480 | Total Load Deflection Criteria: L/360 |

| <u>REACTIONS</u> | <u>A</u> | | <u>B</u> | |
|------------------|----------|----|----------|----|
| Live Load | 89 | lb | 89 | lb |
| Dead Load | 33 | lb | 33 | lb |
| Total Load | 122 | lb | 122 | lb |
| Bearing Length | 1.75 | in | 3.50 | in |
| Web Stiffeners | Yes | | No | |

| SUPPORT LOADS | <u>A</u> | | <u>B</u> | |
|---------------|----------|-----|----------|-----|
| Live Load | 67 | plf | 67 | plf |
| Dead Load | 25 | plf | 25 | plf |
| Total Load | 92 | plf | 92 | plf |



SERIES 18 / 11.875 - Louisiana Pacific

Moment Cap: $\frac{\text{Base Values}}{\text{Mcap = 3100 ft-lb}} \frac{\text{Adjusted}}{\text{Mcap' = 3100 ft-lb}}$ Cd = 1.00

Shear Stress: Vcap = 1335 lb Vcap' = 1335 lb

Cd = 1.00

Reaction A: Rcap = 1164 lb Rcap' = 1164 lb Reaction B: Rcap = 1006 lb Rcap' = 1006 lb E.l.: EI = 248 lb-in2 EI' = 248 lb-in2

Controlling Moment: 102 ft-lb

1.66 Ft from left support of span 3 (Right Span) Created by combining all dead and live loads.

Controlling Shear: -122 lb

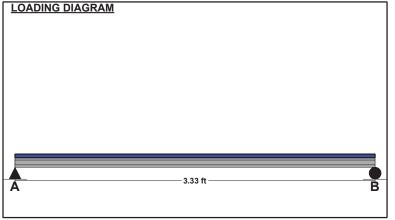
3.0 Ft from left support of span 2 (Center Span) Created by combining all dead and live loads.

 Comparisons with required sections:
 Req'd
 Provided

 E.I.:
 6 in2-lb E6
 248 in2-lb xE6

 Moment:
 102 ft-lb
 3100 ft-lb

 Shear:
 -122 lb
 1335 lb



| JOIST DATA | <u>Ce</u> | <u>enter</u> | |
|----------------------------|-----------|--------------------------------------|--|
| Span Length | 3.33 | 3 ft | |
| Unbraced Length-Top | 0 |) ft | |
| Unbraced Length-Bottom | 0 |) ft | |
| Floor sheathing applied to | top of j | f joists-top of joists fully braced. | |
| Floor Duration Factor 1.0 | 00 | | |

| JOIST LOADING | | | | |
|---------------------------|-------|-------------|-----------|--|
| Uniform Floor Loading | | <u>Cent</u> | <u>er</u> | |
| Live Load | LL = | 40 | psf | |
| Dead Load | DL = | 15 | psf | |
| Total Load | TL = | 55 | psf | |
| TL Adi, For Joist Spacino | = Twr | 73.3 | nlf | |

NOTES

Established Basic Permit #

19-03646

Location: MLB2-1 GLB

Multi-Loaded Multi-Span Beam [2015 International Building Code(2015 NDS)]

3.5 IN x 11.875 IN x 25.09 FT (12.4 + 12.7)

24F-V4 - Visually Graded Western Species - Dry Use

Section Adequate By: 45.0% Controlling Factor: Moment



page

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| 1 | DEFLECTIONS | <u>C</u> | enter enter | | Right |
|---|--------------------|----------|----------------|-------|------------------------------------|
| ı | Live Load | 0.12 | IN L/1214 | 0.16 | IN L/925 |
| ı | Dead Load | 0.01 | in | 0.05 | in |
| ı | Total Load | 0.13 | IN L/1111 | 0.21 | IN L/717 |
| ı | Live Load Deflect | ction C | riteria: L/360 |) Tot | al Load Deflection Criteria: L/240 |

| REACTIONS | <u>A</u> | | <u>B</u> | | <u>C</u> | |
|------------------|----------|----|----------|----|----------|----|
| Live Load | 1551 | lb | 5055 | lb | 1971 | lb |
| Dead Load | 433 | lb | 1533 | lb | 711 | lb |
| Total Load | 1984 | lb | 6588 | lb | 2682 | lb |
| Uplift (1.5 F.S) | -2 | lb | 0 | lb | 0 | lb |
| Bearing Length | 0.87 | in | 2.90 | in | 1.18 | in |

| BEAM DATA | <u>Ce</u> | nter | <u>R</u> | <u>ight</u> |
|---------------------------|-----------|------|----------|-------------|
| Span Length | 12.42 | ft | 12.67 | ft |
| Unbraced Length-Top | 0 | ft | 0 | ft |
| Unbraced Length-Bottom | 12.42 | ft | 12.67 | ft |
| Live Load Duration Factor | 1.00 | | | |
| Notch Depth | 0.00 | | | |

MATERIAL PROPERTIES

24F-V4 - Visually Graded Western Species

| | <u>Base V</u> | <u>′alues</u> | <u>Adjusted</u> | | |
|------------------------------|---------------------|---------------|-----------------------|----------|--|
| Bending Stress: | Fb = | 2400 psi | Controlled b | oy: | |
| | Fb_cmpr = | 1850 psi | Fb_cmpr' = | 1783 psi | |
| | Cd=1.00 C | =0.96 | | | |
| Shear Stress: | Fv = | 265 psi | Fv' = | 265 psi | |
| | Cd=1.00 | | | | |
| Modulus of Elasticity: | E = | 1800 ksi | E' = | 1800 ksi | |
| Comp. [⊥] to Grain: | Fc - ⊥ = | 650 psi | Fc - [⊥] ' = | 650 psi | |
| Comp. to Grain: | Fc - ' = | 650 psi | Fc - ' = | 650 psi | |

Controlling Moment: -8428 ft-lb Over left support of span 3 (Right Span)

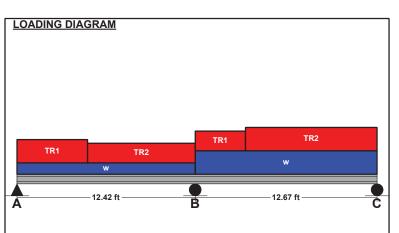
Created by combining all dead loads and live loads on span(s) 2, 3

Controlling Shear: 3278 lb

At a distance d from left support of span 3 (Right Span)

Created by combining all dead loads and live loads on span(s) 2, 3

| Comparisons with required sections: | Req'd | <u>Provided</u> |
|-------------------------------------|-------------|-----------------|
| Section Modulus: | 56.73 in3 | 82.26 in3 |
| Area (Shear): | 18.56 in2 | 41.56 in2 |
| Moment of Inertia (deflection): | 190.18 in4 | 488.41 in4 |
| Moment: | -8428 ft-lb | 12221 ft-lb |
| Shear: | 3278 lb | 7343 lb |



| | | | | 21.14 |
|----------------------|----------|--------|-------------|-------------------------------|
| UNIFORM LOADS | <u>C</u> | cente: | <u>r*</u> ! | Right* |
| Uniform Live Load | 67 | plf | 139 | plf |
| Uniform Dead Load | 25 | plf | 52 | plf |
| Beam Self Weight | 9 | plf | 9 | plf |
| Total Uniform Load | 101 | plf | 200 | plf |
| * Load obtained from | Load | Trac | ker. Se | e Summary Report for details. |

| TRAPEZOIDAL LO | OADS - CEN | TER SPAN | |
|-----------------|--------------|----------|--|
| Load Number | One * | Two * | |
| Left Live Load | 217 plf | 220 plf | |
| Left Dead Load | 81 plf | 31 plf | |
| Right Live Load | 217 plf | 220 plf | |
| Right Dead Load | 81 plf | 31 plf | |
| Load Start | 0 ft | 4.92 ft | |
| Load End | 4.92 ft | 12.42 ft | |
| Load Length | 4.92 ft | 7.5 ft | |
| RIGHT SPAN | | | |
| Load Number | <u>One</u> * | Two * | |
| Left Live Load | 220 plf | 217 plf | |
| Left Dead Load | 31 plf | 81 plf | |
| Right Live Load | 220 plf | 217 plf | |
| Right Dead Load | 31 plf | 81 plf | |
| Load Start | 0 ft | 3.5 ft | |
| Load End | 3.5 ft | 12.67 ft | |
| Load Length | 3.5 ft | 9.17 ft | |

* Load obtained from Load Tracker. See Summary Report for details.

NOTES

Established Basic Permit #

19-03646

Location: MLB2-1 LSL

Multi-Loaded Multi-Span Beam

[2015 International Building Code(2015 NDS)]

3.5 IN x 11.875 IN x 25.09 FT (12.4 + 12.7)

LSL 2360 Fb-1.55E - Louisiana Pacific

Section Adequate By: 75.7% Controlling Factor: Moment





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LOADING DIAGRAM

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| DEFLECTIONS | <u>Center</u> | | | Right |
|------------------|---------------|----------------|-------|------------------------------------|
| Live Load | 0.14 | IN L/1045 | 0.19 | IN L/796 |
| Dead Load | 0.02 | in | 0.06 | in |
| Total Load | 0.16 | IN L/951 | 0.25 | IN L/615 |
| Live Load Deflec | ction C | riteria: L/360 |) Tot | al Load Deflection Criteria: L/240 |

| REACTIONS | <u>A</u> | | <u>B</u> | | <u>C</u> | |
|----------------|----------|----|----------|----|----------|----|
| Live Load | 1551 | lb | 5055 | lb | 1971 | lb |
| Dead Load | 448 | lb | 1582 | lb | 726 | lb |
| Total Load | 1999 | lb | 6637 | lb | 2697 | lb |
| Bearing Length | 0.65 | in | 2.17 | in | 0.88 | in |

| BEAM DATA | <u>Ce</u> | nter | <u>R</u> | ight |
|---------------------------|-----------|------|----------|------|
| Span Length | 12.42 | ft | 12.67 | ft |
| Unbraced Length-Top | 0 | ft | 0 | ft |
| Unbraced Length-Bottom | 12.42 | ft | 12.67 | ft |
| Live Load Duration Factor | 1.00 | | | |
| Notch Depth | 0.00 | | | |

MATERIAL PROPERTIES

Comp. [⊥] to Grain:

NOTES

LSL 2360 Fb-1.55E - Louisiana Pacific

| | <u>Bas</u> | <u>e values</u> | <u>Adjusted</u> | |
|------------------------|------------|-----------------|-----------------|----------|
| Bending Stress: | Fb = | 2360 psi | Fb' = | 2176 psi |
| | Cd=1.0 | 00 CI=0.92 CI | ==1.00 | |
| Shear Stress: | Fv = | 410 psi | Fv' = | 410 psi |
| | Cd=1.0 | 00 | | |
| Modulus of Elasticity: | E = | 1550 ksi | E' = | 1550 ksi |

 $Fc - \bot = 875 \text{ psi}$ $Fc - \bot' = 875 \text{ psi}$

Controlling Moment: -8490 ft-lb Over left support of span 3 (Right Span)

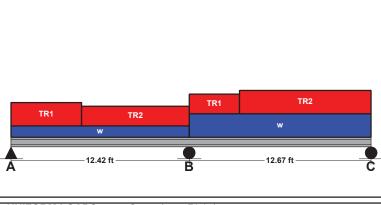
Created by combining all dead loads and live loads on span(s) 2, 3

Controlling Shear: 3300 lb

At a distance d from left support of span 3 (Right Span)

Created by combining all dead loads and live loads on span(s) 2, 3

| Comparisons with required sections: | Req'd | Provided |
|-------------------------------------|-------------|-------------|
| Section Modulus: | 46.83 in3 | 82.26 in3 |
| Area (Shear): | 12.07 in2 | 41.56 in2 |
| Moment of Inertia (deflection): | 220.86 in4 | 488.41 in4 |
| Moment: | -8490 ft-lb | 14914 ft-lb |
| Shear: | 3300 lb | 11360 lb |



| UNIFORM LOADS | | ente | r* | Right* | |
|----------------------|------|------|---------|--------------------|----------|
| DIVIII DIXIVI ECADO | _ | CHIC | | <u>vigrit</u> | |
| Uniform Live Load | 67 | plf | 139 | plf | |
| Uniform Dead Load | 25 | plf | 52 | plf | |
| Beam Self Weight | 12 | plf | 12 | plf | |
| Total Uniform Load | 104 | plf | 203 | plf | |
| * Load obtained from | Load | Trac | ker. Se | Summary Report for | details. |

| TRAPEZOIDAL LO | ADS CEN | TED CDAN | |
|-----------------|--------------|--------------|--|
| | | | |
| Load Number | <u>One</u> * | <u>Two</u> * | |
| Left Live Load | 217 plf | 220 plf | |
| Left Dead Load | 81 plf | 31 plf | |
| Right Live Load | 217 plf | 220 plf | |
| Right Dead Load | 81 plf | 31 plf | |
| Load Start | 0 ft | 4.92 ft | |
| Load End | 4.92 ft | 12.42 ft | |
| Load Length | 4.92 ft | 7.5 ft | |
| RIGHT SPAN | | | |
| Load Number | <u>One</u> * | <u>Two</u> * | |
| Left Live Load | 220 plf | 217 plf | |
| Left Dead Load | 31 plf | 81 plf | |
| Right Live Load | 220 plf | 217 plf | |
| Right Dead Load | 31 plf | 81 plf | |
| Load Start | 0 ft | 3.5 ft | |
| Load End | 3.5 ft | 12.67 ft | |
| Load Length | 3.5 ft | 9.17 ft | |

^{*} Load obtained from Load Tracker. See Summary Report for details.

Established Basic Permit #

19-03646

Project: 19-002c Framing Location: FTG-PST-MLB2-1B

Footing

[2015 International Building Code(2015 NDS)] Footing Size: 2.0 FT x 2.0 FT x 10.00 IN

Reinforcement: #4 Bars @ 8.00 IN. O.C. E/W / (3) min.

Section Footing Design Adequate



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FOOTING PROPERTIES Allowable Soil Bearing Pressure: Qs = 2500 psfConcrete Compressive Strength: F'c = 2500 psi Reinforcing Steel Yield Strength: Fy = 60000 psiConcrete Reinforcement Cover: 3 in

FOOTING SIZE

Width: W =2 ft Length: L= 2 ft Depth: Depth = 10 in Effective Depth to Top Layer of Steel: 6.25 in

COLUMN AND BASEPLATE SIZE

Column Type: Wood Column Width: m = 3.5 inColumn Depth: n = 3.5 in

FOOTING CALCULATIONS

Bearing Calculations:

Ultimate Bearing Pressure: Qu = 1652 psf Effective Allowable Soil Bearing Pressure: Qe = 2375 psf Required Footing Area: Areq = 2.78 sf Area Provided: 4.00 sf A = **Baseplate Bearing:** Bearing Required: 9953 lb Bear = Allowable Bearing: Bear-A = 33841 lb Beam Shear Calculations (One Way Shear): Beam Shear: Vu1 = 2385 lb Allowable Beam Shear: Vc1 = 11250 lb

Punching Shear Calculations (Two Way Shear):

Critical Perimeter: Bo = 39 in Vu2 = 8310 lb Punching Shear: Allowable Punching Shear (ACI 11-35): vc2-a = 54844 lb Allowable Punching Shear (ACI 11-36): 76875 lb vc2-b =Allowable Punching Shear (ACI 11-37): vc2-c = 36563 lb Controlling Allowable Punching Shear: vc2 = 36563 lb **Bending Calculations:** 29858 in-lb Mu =

Factored Moment:

Nominal Moment Strength: Mn = 187693 in-lb **Reinforcement Calculations:** Concrete Compressive Block Depth: 0.69 in a = Steel Required Based on Moment: As(1) =0.09 in2 Min. Code Req'd Reinf. Shrink./Temp. (ACI-10.5.4): As(2) = 0.43 in2 As-reqd = Controlling Reinforcing Steel: 0.43 in2

Selected Reinforcement:

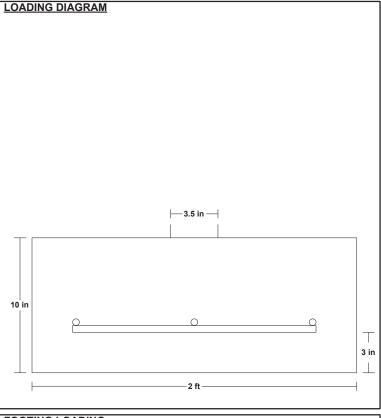
Reinforcement Area Provided: 0.59 in2 As =**Development Length Calculations:**

#4's @ 8.0 in. o.c. e/w (3) Min.

Development Length Required: Ld = 15 in Development Length Supplied: Ld-sup = 9 in

Note: Plain concrete adequate for bending,

therefore adequate development length not required.



FOOTING LOADING

Live Load: PL = 5055 lb * Dead Load: PD = 1554 lb * Total Load: PT = 6609 lb * Ultimate Factored Load: Pu = 9953 lbFooting plus soil above footing weight: Wt = 322 lb

* Load obtained from Load Tracker. See Summary Report for details.

NOTES

Established Basic Permit #

Project: 19-002c Framing Location: PST-MLB2-1A

Column

[2015 International Building Code(2015 NDS)]

1.5 IN x 3.5 IN x 9.08 FT #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 16.4%



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VERTICAL REACTIONS

 Live Load:
 Vert-LL-Rxn =
 1551 lb

 Dead Load:
 Vert-DL-Rxn =
 443 lb

 Total Load:
 Vert-TL-Rxn =
 1994 lb

COLUMN DATA

Total Column Length: 9.08 ft
Unbraced Length (X-Axis) Lx: 9.08 ft
Unbraced Length (Y-Axis) Ly: 0 ft
Column End Condition-K (e): 1
Axial Load Duration Factor 1.00

COLUMN PROPERTIES

#2 - Douglas-Fir-Larch

Compressive Stress: Base Values Adjusted

Fc = 1350 psi Fc' = 454 psi

Cd=1.00 Cf=1.15 Cp=0.29

Bending Stress (X-X Axis): Fbx = 900 psi Fbx' = 1350 psi

Cd=1.00 CF=1.50

Bending Stress (Y-Y Axis): Fby = 900 psi Fby' = 1350 psi

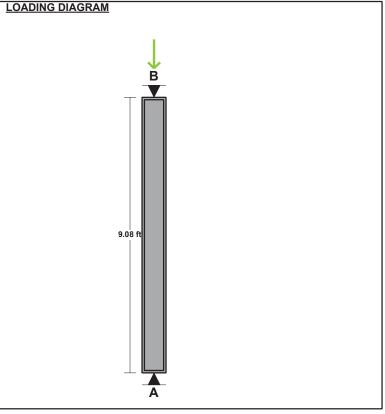
Cd=1.00 CF=1.50

Modulus of Elasticity: E = 1600 ksi E' = 1600 ksi

Column Section (X-X Axis): dx =3.5 in 1.5 in Column Section (Y-Y Axis): dy =Area: A = 5.25 in2 Section Modulus (X-X Axis): Sx = 3.06 in3 Section Modulus (Y-Y Axis): Sy = 1.31 in3 Slenderness Ratio: Lex/dx = 31.13 Ley/dy = 0

Column Calculations (Controlling Case Only):

Controlling Load Case: Axial Total Load Only (L + D) **Actual Compressive Stress:** Fc = 380 psi Allowable Compressive Stress: Fc' = 454 psi Eccentricity Moment (X-X Axis): Mx-ex = 0 ft-lb Eccentricity Moment (Y-Y Axis): My-ey = 0 ft-lb Moment Due to Lateral Loads (X-X Axis): 0 Mx =ft-lb Moment Due to Lateral Loads (Y-Y Axis): My = 0 ft-lb Bending Stress Lateral Loads Only (X-X Axis): Fbx = 0 psi Allowable Bending Stress (X-X Axis): Fbx' = 1350 psi Bending Stress Lateral Loads Only (Y-Y Axis): Fby = 0 psi Allowable Bending Stress (Y-Y Axis): Fby' = 1350 psi **Combined Stress Factor:** CSF = 0.84



AXIAL LOADING

Live Load: PL = 1551 lb *
Dead Load: PD = 433 lb *
Column Self Weight: CSW = 10 lb
Total Axial Load: PT = 1994 lb

* Load obtained from Load Tracker. See Summary Report for details.

NOTES

Established Basic Permit #

19-03646

Project: 19-002c Framing Location: FTG-PST-MLB2-1A

Footing

[2015 International Building Code(2015 NDS)] Footing Size: 1.0 FT x 1.0 FT x 10.00 IN

Reinforcement in Long Direction: #4 Bars @ 5.50 IN. O.C. / (2) min.

Reinforcement in Short Direction-center band (Equal to width of short side): #4

Bars @ 5.50 IN. O.C. / (2) min.

Reinforcement in Short Direction-outside bands: #4 Bars @ 0.00 IN. O.C. / ()

Fach band

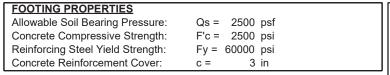
Section Footing Design Adequate





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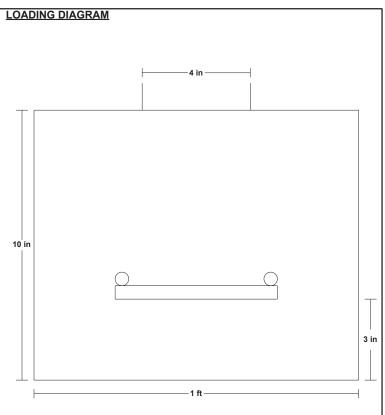
FOOTING SIZE W = 1 ft Width: Length: L= 1 ft Depth: Depth = 10 in Effective Depth to Top Layer of Steel: d = 6.25 in

COLUMN AND BASEPLATE SIZE

Other Column Type: Column Width: m = 4 inColumn Depth: n = 4 in

FOOTING CALCULATIONS

| Bearing Calculations: | | | |
|--|----------|-------|-----|
| Ultimate Bearing Pressure: | Qu = | 1994 | psf |
| Effective Allowable Soil Bearing Pressure: | Qe = | 2375 | psf |
| Required Footing Area: | Areq = | 0.84 | sf |
| Area Provided: | A = | 1.00 | sf |
| Baseplate Bearing: | | | |
| Bearing Required: | Bear = | 3013 | lb |
| Allowable Bearing: | Bear-A = | 44200 | lb |
| Beam Shear Calculations (One Way Shear): | | | |
| Beam Shear: | Vu1 = | 0 | lb |
| Allowable Beam Shear: | Vc1 = | 5625 | lb |
| Punching Shear Calculations (Two Way Shear): | | | |
| Critical Perimeter: | Bo = | 41 | in |
| Punching Shear: | Vu2 = | 815 | lb |
| Allowable Punching Shear (ACI 11-35): | vc2-a = | 57656 | lb |
| Allowable Punching Shear (ACI 11-36): | vc2-b = | 77813 | lb |
| Allowable Punching Shear (ACI 11-37): | vc2-c = | 38438 | lb |



FOOTING LOADING Live Load: PL = 1551 lb * Dead Load: PD = 443 lb * Total Load: PT = 1994 lb * Ultimate Factored Load: Pu = 3013 lbFooting plus soil above footing weight: Wt = 81 lb * Load obtained from Load Tracker. See Summary Report for details.

Bending Calculations:

Factored Moment: Mu =4520 in-lb Nominal Moment Strength: Mn = 122682 in-lb **Reinforcement Calculations:**

vc2 =

38438 lb

Controlling Allowable Punching Shear:

Concrete Compressive Block Depth: a = 0.92 in Steel Required Based on Moment: As(1) =0.01 in2 Min. Code Reg'd Reinf. Shrink./Temp. (ACI-10.5.4): As(2) = 0.22 in2 Controlling Reinforcing Steel: As-reqd = 0.22 in2 Short Dir: #4's @ 5.5 in. o.c.(2) Min. Selected Reinforcement: Reinforcement Area Provided: 0.39 in2 As =

Development Length Calculations:

Development Length Required: Ld = 15 in Development Length Supplied: Ld-sup = 3 in

Established Basic Remitons

therefore adequate development length not required.

Long Direction:

Bending Calculations:

Factored Moment: 4520 in-lb Mu = 122739 in-lb Nominal Moment Strength: Mn = Reinforcement Calculations: Concrete Compressive Block Depth: 0.92 in Steel Required Based on Moment: As(1) =0.01 in2 Min. Code Reg'd Reinf. Shrink./Temp. (ACI-10.5.4): As(2) = 0.22 in2 Controlling Reinforcing Steel: As-reqd = 0.22 in2 Selected Reinforcement: Long Dir: #4's @ 5.5 in. o.c.(2) Min. Reinforcement Area Provided: 0.39 in2 As =

Development Length Calculations:

Development Length Required: Ld = 15 in **Development Length Supplied:** Ld-sup = 3 in

Project: 19-002c Framing Location: WALL-1ST-1

Wall

[2015 International Building Code(2015 NDS)]

1.5 IN x 5.5 IN x 8.08 FT @ 16 O.C. #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 87.5%

Controlling Factor: Combined Stress Factor





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DEFLECTIONS

Deflection due to lateral loads only: Defl = 0.06 IN = L/1638 Live Load Deflection Criteria: L/180

VERTICAL REACTIONS

Live Load: Vert-LL-Rxn = 0 lb Dead Load: Vert-DL-Rxn = 119 lb Total Load: Vert-TL-Rxn = 119 lb

HORIZONTAL REACTIONS

Total Reaction at Top of Column: TL-Rxn-Top = 83 lb Total Reaction at Bottom of Column: TL-Rxn-Bottom = 83 lb

WALL DATA

Total Stud Length: 8.08 ft Wall Dead Weight: 11 psf Unbraced Length (X-Axis) Lx: 8.08 ft Unbraced Length (Y-Axis) Ly: 0 ft Stud End Condition-K (e): 1 **Axial Load Duration Factor** 1.00 Lateral Load Duration Factor (Wind/Seismic)

STUD PROPERTIES

#2 - Douglas-Fir-Larch

Base Values **Adjusted** Compressive Stress: Fc = 1350 psi Fc' = 1254 psi

Cd=1.60 Cf=1.10 Cp=0.53

Bending Stress (X-X Axis): Fbx = 900 psi Fbx' = 2153 psi Cd=1.60 CF=1.30 Cr=1.15 Cl=1.00

Bending Stress (Y-Y Axis): Fby = 900 psi Fby' = 2153 psi

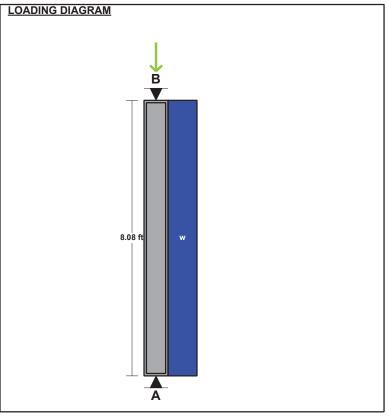
Cd=1.60 CF=1.30 Cr=1.15

Modulus of Elasticity: E = 1600 ksi E' = 1600 ksi

Stud Section (X-X Axis): dx =5.5 in Stud Section (Y-Y Axis): dy =1.5 in Area: A = 8.25 in2 Section Modulus (X-X Axis): Sx =7.56 in3 Section Modulus (Y-Y Axis): Sy = 2.06 in3 Slenderness Ratio: Lex/dx = 17.63Ley/dy =

Stud Calculations (Controlling Case Only):

Controlling Load Case: Axial Dead Load and Lateral loads (D + W or E) Actual Compressive Stress: Fc = 14 psi Allowable Compressive Stress: Fc' = 1254 psi Eccentricity Moment (X-X Axis): Mx-ex = 0 ft-lb Eccentricity Moment (Y-Y Axis): My-ey = 0 ft-lb Moment Due to Lateral Loads (X-X Axis): Mx =168 ft-lb Moment Due to Lateral Loads (Y-Y Axis): My = 0 ft-lb Bending Stress Lateral Loads Only (X-X Axis): Fbx = 266 psi Allowable Bending Stress (X-X Axis): Fbx' = 2153 psi Bending Stress Lateral Loads Only (Y-Y Axis): Fby = 0 psi Allowable Bending Stress (Y-Y Axis): Fby' = 2153 psi **Combined Stress Factor:** CSF = 0.12



WALL LOAD CALCULATOR

Tributary Width Live Load Dead Load Load Tracker: 0 plf DL = 0 plf LL = Roof: 0 ft 25 psf DL = 15 psf TA = Upper Floor: 40 psf DL = 15 psf TA = 0 ft Upper Floor Height: 0 ft Middle Floor: 40 psf DL = TA = 0 ft II =15 psf Middle Floor Height: 0 ft

Calculated Load: 0 plf DL = 88.9 plf

LL =

AXIAL LOADING

Live Load: PL = 0 plf * Dead Load: PD = 89 plf * PT = Total Axial Load: 89 plf

* Load obtained from Load Tracker. See Summary Report for details.

LATERAL LOADING (Dy Face) Uniform Lateral Load: wL-Lat = 15 psf

NOTES

Established Basic Permit #

Project: 19-002c Framing Location: PST-MLB2-1B

Column

[2015 International Building Code(2015 NDS)]

5.5 IN x 5.5 IN x 9.08 FT #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 60.5%





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VERTICAL REACTIONS

 Live Load:
 Vert-LL-Rxn =
 5055
 lb

 Dead Load:
 Vert-DL-Rxn =
 1593
 lb

 Total Load:
 Vert-TL-Rxn =
 6648
 lb

COLUMN DATA

Total Column Length: 9.08 ft Unbraced Length (X-Axis) Lx: 9.08 ft Unbraced Length (Y-Axis) Ly: 9.08 ft Column End Condition-K (e): 1 Axial Load Duration Factor 1.00

COLUMN PROPERTIES

#2 - Douglas-Fir-Larch

 $\frac{\text{Base Values}}{\text{Compressive Stress:}} \qquad \frac{\text{Adjusted}}{\text{Fc = 700 psi}} \quad \frac{\text{Adjusted}}{\text{Fc' = 556 psi}}$

Cd=1.00 Cp=0.79

Bending Stress (X-X Axis): Fbx = 750 psi Fbx' = 750 psi

Cd=1.00 CF=1.00

Bending Stress (Y-Y Axis): Fby = 750 psi Fby' = 750 psi

Cd=1.00 CF=1.00

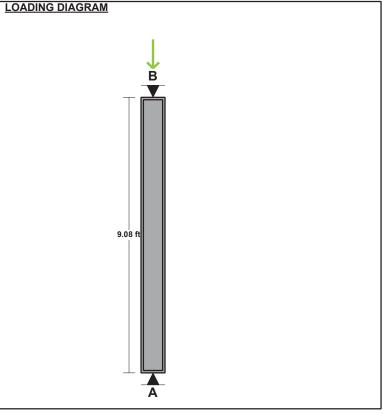
Modulus of Elasticity: E = 1300 ksi E' = 1300 ksi

5.5 in Column Section (X-X Axis): dx =Column Section (Y-Y Axis): dy =5.5 in Area: A = 30.25 in2 Section Modulus (X-X Axis): Sx =27.73 in3 Section Modulus (Y-Y Axis): Sy = 27.73 Slenderness Ratio: Lex/dx = 19.81

Ley/dy = 19.81

Column Calculations (Controlling Case Only):

Controlling Load Case: Axial Total Load Only (L + D) **Actual Compressive Stress:** Fc = 220 psi Allowable Compressive Stress: Fc' = 556 psi Eccentricity Moment (X-X Axis): Mx-ex = 0 ft-lb Eccentricity Moment (Y-Y Axis): My-ey = 0 ft-lb Moment Due to Lateral Loads (X-X Axis): Mx =0 ft-lb Moment Due to Lateral Loads (Y-Y Axis): My = 0 ft-lb Bending Stress Lateral Loads Only (X-X Axis): Fbx = 0 psi Allowable Bending Stress (X-X Axis): Fbx' = 750 psi Bending Stress Lateral Loads Only (Y-Y Axis): Fby = 0 psi Allowable Bending Stress (Y-Y Axis): Fby' = 750 psi **Combined Stress Factor:** CSF = 0.4



AXIAL LOADING

 Live Load:
 PL =
 5055 lb *

 Dead Load:
 PD =
 1533 lb *

 Column Self Weight:
 CSW =
 60 lb

 Total Axial Load:
 PT =
 6648 lb

* Load obtained from Load Tracker. See Summary Report for details.

NOTES

Established Basic Permit #

19-03646

Project: 19-002c Framing Location: FTG-WALL-1ST-1

Footing

[2015 International Building Code(2015 NDS)]

Footing Size: 18.0 IN Wide x 8.0 IN Deep Continuous Footing With 8.0 IN Thick

x 12.0 IN Tall Stemwall

LongitudinalReinforcement: (2) Continuous #4 Bars

TransverseReinforcement: #4 Bars @ 13.00 IN. O.C. (unnecessary)

Section Footing Design Adequate



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FOOTING PROPERTIES

Allowable Soil Bearing Pressure: Qs = 2500 psf Concrete Compressive Strength: F'c = 2500 psi Reinforcing Steel Yield Strength: Fy = 60000 psi Concrete Reinforcement Cover: c = 3 in

FOOTING SIZE

Width: W = 18 in Depth: Depth = 8 in Effective Depth to Top Layer of Steel: d = 4.25 in

STEMWALL SIZE

Stemwall Width: 8 in Stemwall Height: 12 in Stemwall Weight: 150 pcf

FOOTING CALCULATIONS

Bearing Calculations:

Ultimate Bearing Pressure: Qu = 933 psf 2400 psf Effective Allowable Soil Bearing Pressure: Oe = Width Required: Wrea = 0.58 ft Beam Shear Calculations (One Way Shear): Beam Shear: Vu1 = 82 lb Allowable Beam Shear: Vc1 = 3825 lb

Transverse Direction:

Bending Calculations:

Factored Moment: Mu = 1367 in-lb
Nominal Moment Strength: Mn = 0 in-lb
Reinforcement Calculations:
Concrete Compressive Block Depth: a = 0.41 in

Steel Required Based on Moment: As(1) = 0.01 in2 Min. Code Req'd Reinf. Shrink./Temp. (ACI-10.5.4)As(2) = 0.17 in2 Controlling Reinforcing Steel: As-reqd = 0.17 in2 Selected Reinforcement: Trans: #4's @ 13.0 in. o.c. Reinforcement Area Provided: As = 0.17 in2

Development Length Calculations:

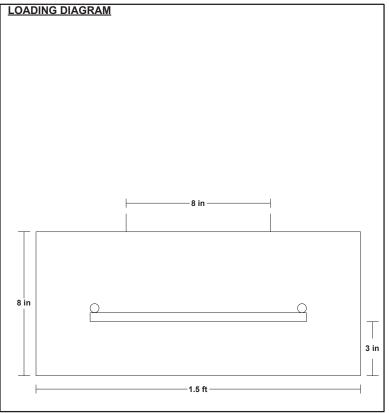
Development Length Required: Ld = 15 in Development Length Supplied: Ld-sup = 2 in

Longitudinal Direction:

Reinforcement Calculations:

Min. Code Req'd Reinf. Shrink./Temp. (ACI-10.5.4): As(2) = 0.26 in2 Controlling Reinforcing Steel: As-reqd = 0.26 in2 Selected Reinforcement: Longitudinal: (2) Cont. #4 Bars Reinforcement Area Provided: As = 0.39 in2

NOTES



FOOTING LOADING

Live Load: PL = 721 plf *
Dead Load: PD = 579 plf *
Total Load: PT = 1400 plf *
Ultimate Factored Load: Pu = 1968 plf

* Load obtained from Load Tracker. See Summary Report for details.

Established Basic Permit #

19-03646

Project: 19-002c Framing Location: WALL-2ND-6

Wall

[2015 International Building Code(2015 NDS)]

1.5 IN x 5.5 IN x 8.08 FT @ 16 O.C. #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 87.5%

Controlling Factor: Combined Stress Factor



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DEFLECTIONS

Deflection due to lateral loads only: Defl = 0.06 IN = L/1638 Live Load Deflection Criteria: L/180

VERTICAL REACTIONS

 Live Load:
 Vert-LL-Rxn =
 0 lb

 Dead Load:
 Vert-DL-Rxn =
 108 lb

 Total Load:
 Vert-TL-Rxn =
 108 lb

HORIZONTAL REACTIONS

Total Reaction at Top of Column: TL-Rxn-Top = 83 lb
Total Reaction at Bottom of Column: TL-Rxn-Bottom = 83 lb

WALL DATA

Total Stud Length:

Wall Dead Weight:
Unbraced Length (X-Axis) Lx:
Unbraced Length (Y-Axis) Ly:
Stud End Condition-K (e):
Axial Load Duration Factor
Lateral Load Duration Factor (Wind/Seismic)

8.08 ft
10 psf
11 psf
12 psf
13 psf
14 psf
15 psf
16 psf
16 psf
17 psf
18 psf
18

STUD PROPERTIES

#2 - Douglas-Fir-Larch

Base Values Adjusted

Compressive Stress: Fc = 1350 psi Fc' = 1254 psi

Cd=1.60 Cf=1.10 Cp=0.53

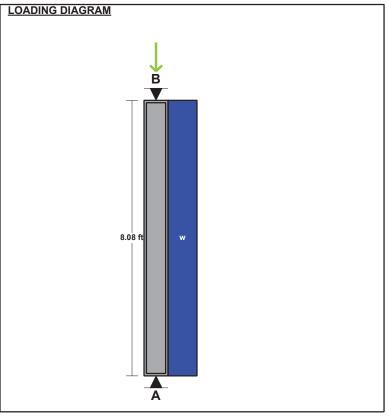
Bending Stress (X-X Axis): Fbx = 900 psi Fbx' = 2153 psi Cd=1.60 CF=1.30 Cr=1.15 Cl=1.00

Bending Stress (Y-Y Axis): Fby = 900 psi Fby' = 2153 psi

Stud Section (X-X Axis): dx =5.5 in Stud Section (Y-Y Axis): dy =1.5 in Area: A = 8.25 in2 Section Modulus (X-X Axis): Sx =7.56 in3 Section Modulus (Y-Y Axis): Sy = 2.06 in3 Slenderness Ratio: Lex/dx = 17.63Ley/dy =

Stud Calculations (Controlling Case Only):

Controlling Load Case: Axial Dead Load and Lateral loads (D + W or E) Actual Compressive Stress: Fc = 13 psi Allowable Compressive Stress: Fc' = 1254 psi Eccentricity Moment (X-X Axis): Mx-ex = 0 ft-lb Eccentricity Moment (Y-Y Axis): My-ey = 0 ft-lb Moment Due to Lateral Loads (X-X Axis): Mx =168 ft-lb Moment Due to Lateral Loads (Y-Y Axis): My = 0 ft-lb Bending Stress Lateral Loads Only (X-X Axis): Fbx = 266 psi Allowable Bending Stress (X-X Axis): Fbx' = 2153 psi Bending Stress Lateral Loads Only (Y-Y Axis): Fby = 0 psi Allowable Bending Stress (Y-Y Axis): Fby' = 2153 psi **Combined Stress Factor:** CSF = 0.12



WALL LOAD CALCULATOR

Tributary Width Live Load Dead Load Load Tracker: 0 plf DL = 0 plf LL = Roof: 0 ft 25 psf DL = 15 psf TA = Upper Floor: 40 psf DL = 15 psf TA = 0 ft Upper Floor Height: 0 ft Middle Floor: 40 psf DL = TA = 0 ft II =15 psf Middle Floor Height: 0 ft

0 plf DL = 80.8 plf

AXIAL LOADING

Calculated Load:

Live Load: PL = 0 plf *
Dead Load: PD = 81 plf *
Total Axial Load: PT = 81 plf

* Load obtained from Load Tracker. See Summary Report for details.

LL =

LATERAL LOADING (Dy Face)
Uniform Lateral Load: wL-Lat = 15 psf

NOTES

Established Basic Permit #

19-03646

Location: MLB2-2

Multi-Loaded Multi-Span Beam

[2015 International Building Code(2015 NDS)]

1.75 IN x 11.875 IN x 6.5 FT

LSL 2360 Fb-1.55E - Louisiana Pacific

Section Adequate By: 226.3% Controlling Factor: Moment



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| _ | | | | | |
|---|------------------|----------|----|----------|----|
| ı | <u>REACTIONS</u> | <u>A</u> | | <u>B</u> | |
| ı | Live Load | 645 | lb | 645 | lb |
| l | Dead Load | 883 | lb | 883 | lb |
| l | Total Load | 1528 | lb | 1528 | lb |
| l | Bearing Length | 1.00 | in | 1.00 | in |

| BEAM DATA | <u>Ce</u> | nter |
|---------------------------|-----------|------|
| Span Length | 6.5 | ft |
| Unbraced Length-Top | 0 | ft |
| Unbraced Length-Bottom | 6.5 | ft |
| Live Load Duration Factor | 1.0 | 0 |
| Notch Depth | 0.0 | 0 |

MATERIAL PROPERTIES

LSL 2360 Fb-1.55E - Louisiana Pacific

Shear Stress: Fv = 410 psi Fv' = 410 psi

Cd=1.00

Modulus of Elasticity: E = 1550 ksi E' = 1550 ksi Comp. $^{\perp}$ to Grain: Fc - $^{\perp}$ = 875 psi Fc - $^{\perp}$ ' = 875 psi

Controlling Moment: 2483 ft-lb 3.25 Ft from left support of span 2 (Center Span)

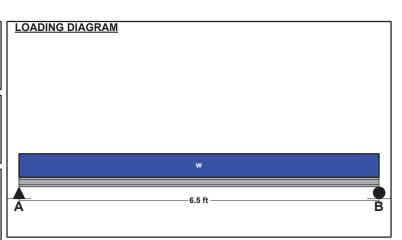
Created by combining all dead loads and live loads on span(s) 2

Controlling Shear: 1069 lb

At a distance d from left support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2

| Comparisons with required sections: | Req'd | Provided |
|-------------------------------------|------------|-----------------|
| Section Modulus: | 12.6 in3 | 41.13 in3 |
| Area (Shear): | 3.91 in2 | 20.78 in2 |
| Moment of Inertia (deflection): | 37.47 in4 | 244.21 in4 |
| Moment: | 2483 ft-lb | 8101 ft-lb |
| Shear: | 1069 lb | 5680 lb |



| UNIFORM LOADS | <u>C</u> | enter* | |
|----------------------|----------|--------|------------------------------------|
| Uniform Live Load | 199 | plf | |
| Uniform Dead Load | 266 | plf | |
| Beam Self Weight | 6 | plf | |
| Total Uniform Load | 470 | plf | |
| * Load obtained from | Load | Tracke | r. See Summary Report for details. |

NOTES

Established Basic Permit #

19-03646

Location: RFB3 Roof Beam

[2015 International Building Code(2015 NDS)]

3.5 IN x 7.25 IN x 8.33 FT #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 150.0% Controlling Factor: Moment



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Side One:

Roof Live Load: LL =

Roof Dead Load: DL =

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DEFLECTIONSCenterLive Load0.06IN L/1751Dead Load0.04inTotal Load0.10IN L/1035Live Load Deflection Criteria: L/240

 REACTIONS
 A
 B

 Live Load
 390 lb
 390 lb

 Dead Load
 270 lb
 270 lb

 Total Load
 660 lb
 660 lb

 Bearing Length
 0.30 in
 0.30 in

Total Load Deflection Criteria: L/180

BEAM DATA Span Length

MATERIAL PROPERTIES

#2 - Douglas-Fir-Larch

Shear Stress: Fv = 180 psi Fv' = 207 psi Cd=1.15

Modulus of Elasticity: E = 1600 ksi E' = 1600 ksi Comp. $^{\perp}$ to Grain: Fc - $^{\perp}$ = 625 psi Fc - $^{\perp}$ ' = 625 psi

Controlling Moment: 1375 ft-lb

4.165 ft from left support

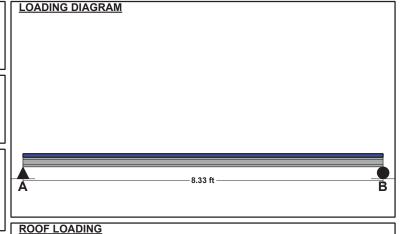
Created by combining all dead and live loads.

Controlling Shear: -568 lb

At a distance d from support.

Created by combining all dead and live loads.

Comparisons with required sections: Reg'd **Provided** Section Modulus: 12.26 in3 30.66 in3 Area (Shear): 4.12 in2 25.38 in2 Moment of Inertia (deflection): 19.33 in4 111.15 in4 Moment: 1375 ft-lb 3438 ft-lb Shear: -568 lb 3502 lb



Tributary Width: TW = 3.8 ft
Side Two:
Roof Live Load: LL = 0 psf
Roof Dead Load: DL = 0 psf
Tributary Width: TW = 0 ft

25 psf

15 psf

Wall Load: WALL = 0 plf

Adjusted Beam Length: Ladj = 8.33 ft
Beam Self Weight: BSW = 6 plf

Beam Uniform Live Load: wL = 94 plf
Beam Uniform Dead Load: wD_adj = 65 plf
Total Uniform Load: wT = 159 plf

NOTES

Established Basic Permit #

19-03646

Location: RFB4 Roof Beam

[2015 International Building Code(2015 NDS)]

5.5 IN x 7.5 IN x 6.83 FT #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 242.3% Controlling Factor: Moment



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LOADING DIAGRAM

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DEFLECTIONS Center Live Load 0.02 IN L/3888 Dead Load 0.02 in Total Load 0.04 IN L/2267 Live Load Deflection Criteria: L/240

Total Load Deflection Criteria: L/180 **REACTIONS** 370 lb 370 lb Live Load Dead Load 264 lb 264 lb Total Load 634 lb 634 lb Bearing Length 0.18 in 0.18 in

BEAM DATA

6.8 ft Span Length Unbraced Length-Top 0 ft Unbraced Length-Bottom 0 ft Roof Pitch 4 .12 Roof Duration Factor 1.15

MATERIAL PROPERTIES

#2 - Douglas-Fir-Larch

Base Values <u>Adjusted</u> 750 psi Bending Stress: Fb = 863 psi Cd=1.15 CF=1.00

Shear Stress: Fv = 170 psi 196 psi Cd=1.15

Modulus of Elasticity: E = 1300 ksi E' = 1300 ksi Comp. [⊥] to Grain: Fc - \perp = 625 psi $Fc - \frac{1}{2} = 625 \text{ psi}$

Controlling Moment: 1083 ft-lb

3.415 ft from left support

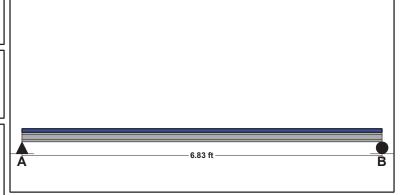
Created by combining all dead and live loads.

Controlling Shear:

At a distance d from support.

Created by combining all dead and live loads.

Comparisons with required sections: Reg'd **Provided** Section Modulus: 15.06 in3 51.56 in3 Area (Shear): 3.99 in2 41.25 in2 Moment of Inertia (deflection): 15.35 in4 193.36 in4 Moment: 1083 ft-lb 3706 ft-lb Shear: 520 lb 5376 lb



ROOF LOADING Side One: Roof Live Load: LL =

25 psf Roof Dead Load: DL = 15 psf Tributary Width: TW = 4.3 ft Side Two: Roof Live Load: LL = 0 psf Roof Dead Load: DL = psf Tributary Width: TW = 0 ft

Wall Load: WALL = 0 plf

SLOPE/PITCH ADJUSTED LENGTHS AND LOADS

Adjusted Beam Length: Ladi = 6.83 ft Beam Self Weight: BSW = 9 plf Beam Uniform Live Load: wL = 108 plf Beam Uniform Dead Load: wD adj = 77 plf wT = Total Uniform Load: 186 plf

NOTES

Established Basic Permit #

19-03646

Location: MLB2-3

Multi-Loaded Multi-Span Beam

[2015 International Building Code(2015 NDS)]

5.5 IN x 11.875 IN x 17.84 FT (10.9 + 6.9) / 30F - 30F-E

DF2 - Dry Use

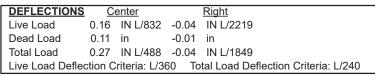
Section Adequate By: 5.9% Controlling Factor: Shear



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| REACTIONS | <u>A</u> | | <u>B</u> | | <u>C</u> | |
|------------------|----------|----|----------|----|----------|----|
| Live Load | 5757 | lb | 14470 | lb | 3890 | lb |
| Dead Load | 4510 | lb | 11880 | lb | 1846 | lb |
| Total Load | 10267 | lb | 26350 | lb | 5736 | lb |
| Uplift (1.5 F.S) | 0 | lb | 0 | lb | -411 | lb |
| Bearing Length | 2.87 | in | 7.37 | in | 1.60 | in |

| BEAM DATA | <u>Ce</u> | nter | R | <u>ight</u> |
|---------------------------|-----------|------|------|-------------|
| Span Length | 10.92 | ft | 6.92 | ft |
| Unbraced Length-Top | 0 | ft | 0 | ft |
| Unbraced Length-Bottom | 10.92 | ft | 6.92 | ft |
| Live Load Duration Factor | 1.15 | | | |
| Notch Depth | 0.00 | | | |

MATERIAL PROPERTIES

30F - 30F-E/DF2

Comp. [⊥] to Grain:

| | Base V | <u>/alues</u> | | <u>Adjus</u> | ted | |
|------------------------|------------|---------------|-----|--------------|------|-----|
| Bending Stress: | Fb = | 3000 p | osi | Controlled b | y: | |
| | Fb_cmpr = | 3000 p | osi | Fb_cmpr' = | 3424 | psi |
| | Cd=1.15 Ci | l=0.99 | | | | |
| Shear Stress: | Fv = | 265 p | osi | Fv' = | 305 | psi |
| | Cd=1.15 | | | | | |
| Modulus of Elasticity: | E = | 2100 k | (si | E' = | 2100 | ksi |

650 psi Fc - [⊥]' =

650 psi

Controlling Moment: -25950 ft-lb 10.92 Ft from left support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2, 3

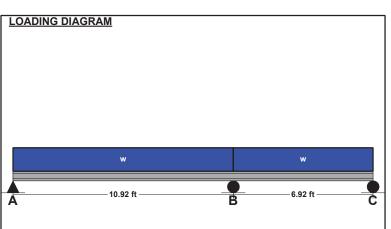
Fc - \perp =

Controlling Shear: -12527 lb

At a distance d from right support of span 2 (Center Span)

Created by combining all dead loads and live loads on span(s) 2, 3

| Comparisons with required sections: | Req'd | <u>Provided</u> |
|-------------------------------------|--------------|-----------------|
| Section Modulus: | 90.95 in3 | 129.26 in3 |
| Area (Shear): | 61.66 in2 | 65.31 in2 |
| Moment of Inertia (deflection): | 377.17 in4 | 767.51 in4 |
| Moment: | -25950 ft-lb | 36881 ft-lb |
| Shear: | -12527 lb | 13269 lb |



| UNIFORM LOADS | <u>C</u> | Cente | r | Right* | |
|--|----------|-------|------|--------|--|
| Uniform Live Load | 1245 | plf | 1245 | plf | |
| Uniform Dead Load | 1008 | plf | 1008 | plf | |
| Beam Self Weight | 14 | plf | 14 | plf | |
| Total Uniform Load | 2267 | plf | 2267 | plf | |
| * Load obtained from Load Tracker. See Summary Report for details. | | | | | |

NOTES

Established Basic Permit #

19-03646

Project: 19-002c Framing Location: PST-MLB2-3A

Column

[2015 International Building Code(2015 NDS)]

5.5 IN x 5.5 IN x 9.58 FT #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 36.2%





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VERTICAL REACTIONS

Live Load: Vert-LL-Rxn = 5757 lb Dead Load: Vert-DL-Rxn = 4573 Total Load: Vert-TL-Rxn = 10330 lb

COLUMN DATA

9.58 ft Total Column Length: Unbraced Length (X-Axis) Lx: 9.58 ft Unbraced Length (Y-Axis) Ly: 9.58 ft Column End Condition-K (e): 1 **Axial Load Duration Factor** 1.00

COLUMN PROPERTIES

#2 - Douglas-Fir-Larch

Base Values Adjusted Fc' = Compressive Stress: Fc = 700 psi 536 psi

Cd=1.00 Cp=0.77

Bending Stress (X-X Axis): Fbx = 750 psi Fbx' = 750 psi

Cd=1.00 CF=1.00

Bending Stress (Y-Y Axis): Fby = 750 psi Fby' = 750 psi

Cd=1.00 CF=1.00

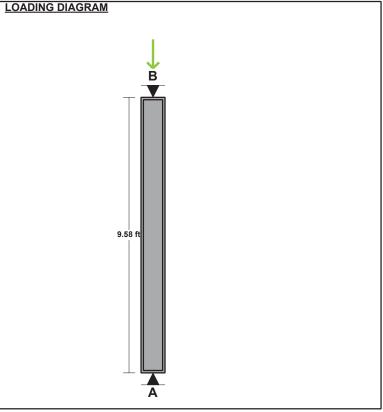
Modulus of Elasticity: E = 1300 ksi E' = 1300 ksi

5.5 in Column Section (X-X Axis): dx =Column Section (Y-Y Axis): dy =5.5 in Area: A = 30.25 in2 Section Modulus (X-X Axis): Sx = 27.73 in3 Section Modulus (Y-Y Axis): Sy = 27.73 Slenderness Ratio: Lex/dx = 20.9

Ley/dy = 20.9

Column Calculations (Controlling Case Only):

Controlling Load Case: Axial Total Load Only (L + D) **Actual Compressive Stress:** Fc = 341 psi Allowable Compressive Stress: Fc' = 536 psi Eccentricity Moment (X-X Axis): Mx-ex = 0 ft-lb Eccentricity Moment (Y-Y Axis): My-ey = 0 ft-lb Moment Due to Lateral Loads (X-X Axis): Mx =0 ft-lb Moment Due to Lateral Loads (Y-Y Axis): My = 0 ft-lb Bending Stress Lateral Loads Only (X-X Axis): Fbx = 0 psi Allowable Bending Stress (X-X Axis): Fbx' = 750 psi Bending Stress Lateral Loads Only (Y-Y Axis): Fby = 0 psi Allowable Bending Stress (Y-Y Axis): Fby' = 750 psi CSF = **Combined Stress Factor:** 0.64



AXIAL LOADING

Live Load: 5757 lb * PI = Dead Load: PD = 4510 lb * Column Self Weight: CSW = 63 lb Total Axial Load: PT = 10330 lb

* Load obtained from Load Tracker. See Summary Report for details.

NOTES

Established Basic Permit #

Project: 19-002c Framing Location: PST-MLB2-3B

Column

[2015 International Building Code(2015 NDS)]

5.5 IN x 7.5 IN x 9.58 FT #1 - Douglas-Fir-Larch - Dry Use Section Adequate By: 11.0%



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VERTICAL REACTIONS

 Live Load:
 Vert-LL-Rxn =
 14470 lb

 Dead Load:
 Vert-DL-Rxn =
 11966 lb

 Total Load:
 Vert-TL-Rxn =
 26436 lb

COLUMN DATA

Total Column Length: 9.58 ft
Unbraced Length (X-Axis) Lx: 9.58 ft
Unbraced Length (Y-Axis) Ly: 9.58 ft
Column End Condition-K (e): 1
Axial Load Duration Factor 1.00

COLUMN PROPERTIES

#1 - Douglas-Fir-Larch

Cd=1.00 Cp=0.72

Bending Stress (X-X Axis): Fbx = 1200 psi Fbx' = 1200 psi

Cd=1.00 CF=1.00

Bending Stress (Y-Y Axis): Fby = 1200 psi Fby' = 1200 psi

Cd=1.00 CF=1.00

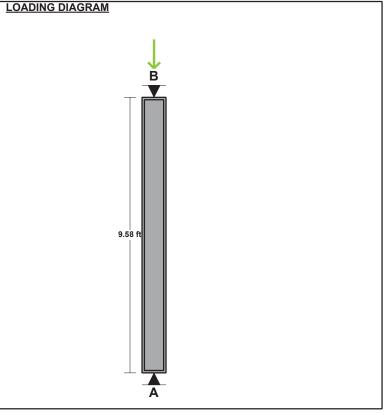
Modulus of Elasticity: E = 1600 ksi E' = 1600 ksi

Column Section (X-X Axis): dx =7.5 in 5.5 in Column Section (Y-Y Axis): dy =Area: A = 41.25 in2 Section Modulus (X-X Axis): Sx = 51.56 in3 Section Modulus (Y-Y Axis): Sy = 37.81 Slenderness Ratio: Lex/dx = 15.33

Ley/dy = 20.9

Column Calculations (Controlling Case Only):

Controlling Load Case: Axial Total Load Only (L + D) **Actual Compressive Stress:** Fc = 641 psi Allowable Compressive Stress: Fc' = 720 psi Eccentricity Moment (X-X Axis): Mx-ex = ft-lb Eccentricity Moment (Y-Y Axis): My-ey = 0 ft-lb Moment Due to Lateral Loads (X-X Axis): 0 Mx =ft-lb Moment Due to Lateral Loads (Y-Y Axis): My = 0 ft-lb Bending Stress Lateral Loads Only (X-X Axis): Fbx = 0 psi Allowable Bending Stress (X-X Axis): Fbx' = 1200 psi Bending Stress Lateral Loads Only (Y-Y Axis): Fby = 0 psi Allowable Bending Stress (Y-Y Axis): Fby' = 1200 psi **Combined Stress Factor:** CSF = 0.89



AXIAL LOADING

Live Load: PL = 14470 lb *
Dead Load: PD = 11880 lb *
Column Self Weight: CSW = 86 lb
Total Axial Load: PT = 26436 lb

* Load obtained from Load Tracker. See Summary Report for details.

NOTES

Established Basic Permit #

19-03646

Project: 19-002c Framing Location: PST-MLB2-3C

Column

[2015 International Building Code(2015 NDS)]

5.5 IN x 5.5 IN x 9.58 FT #2 - Douglas-Fir-Larch - Dry Use Section Adequate By: 67.0%





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VERTICAL REACTIONS

 Live Load:
 Vert-LL-Rxn =
 3890 lb

 Dead Load:
 Vert-DL-Rxn =
 1909 lb

 Total Load:
 Vert-TL-Rxn =
 5799 lb

COLUMN DATA

Total Column Length: 9.58 ft
Unbraced Length (X-Axis) Lx: 9.58 ft
Unbraced Length (Y-Axis) Ly: 9.58 ft
Column End Condition-K (e): 1
Axial Load Duration Factor 1.15

COLUMN PROPERTIES

#2 - Douglas-Fir-Larch

 $\frac{\text{Base Values}}{\text{Compressive Stress:}} \qquad \frac{\text{Adjusted}}{\text{Fc = 700 psi}} \quad \frac{\text{Adjusted}}{\text{Fc' = 582 psi}}$

Cd=1.15 Cp=0.72

Bending Stress (X-X Axis): Fbx = 750 psi Fbx' = 863 psi

Cd=1.15 CF=1.00

Bending Stress (Y-Y Axis): Fby = 750 psi Fby' = 863 psi

Cd=1.15 CF=1.00

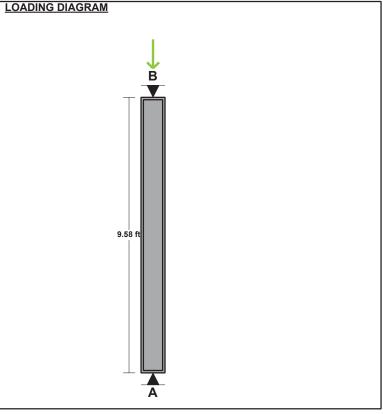
Modulus of Elasticity: E = 1300 ksi E' = 1300 ksi

Column Section (X-X Axis): dx =5.5 in 5.5 in Column Section (Y-Y Axis): dy =Area: A = 30.25 in2 Section Modulus (X-X Axis): Sx = 27.73 in3 Section Modulus (Y-Y Axis): Sy = 27.73 Slenderness Ratio: Lex/dx = 20.9

Ley/dy = 20.9

Column Calculations (Controlling Case Only):

Controlling Load Case: Axial Total Load Only (L + D) **Actual Compressive Stress:** Fc = 192 psi Allowable Compressive Stress: Fc' = 582 psi Eccentricity Moment (X-X Axis): Mx-ex = 0 ft-lb Eccentricity Moment (Y-Y Axis): My-ey = 0 ft-lb Moment Due to Lateral Loads (X-X Axis): 0 Mx =ft-lb Moment Due to Lateral Loads (Y-Y Axis): My = 0 ft-lb Bending Stress Lateral Loads Only (X-X Axis): Fbx = 0 psi Allowable Bending Stress (X-X Axis): Fbx' = 863 psi Bending Stress Lateral Loads Only (Y-Y Axis): Fby = 0 psi Allowable Bending Stress (Y-Y Axis): Fby' = 863 psi CSF = **Combined Stress Factor:** 0.33



AXIAL LOADING

Live Load: PL = 3890 lb *
Dead Load: PD = 1846 lb *
Column Self Weight: CSW = 63 lb
Total Axial Load: PT = 5799 lb

* Load obtained from Load Tracker. See Summary Report for details.

NOTES

Established Basic Permit #

19-03646

Project: 19-002c Framing Location: FTG-PST-MLB2-3A

Footing

[2015 International Building Code(2015 NDS)] Footing Size: 2.5 FT x 2.5 FT x 10.00 IN

Reinforcement: #4 Bars @ 11.00 IN. O.C. E/W / (3) min.

Section Footing Design Adequate





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FOOTING PROPERTIES Allowable Soil Bearing Pressure: Qs = 2500 psfConcrete Compressive Strength: F'c = 2500 psi Reinforcing Steel Yield Strength: Fy = 60000 psiConcrete Reinforcement Cover: 3 in

FOOTING SIZE Width: W =2.5 ft Length: L= 2.5 ft Depth: Depth = 10 in Effective Depth to Top Layer of Steel: d = 6.25 in

COLUMN AND BASEPLATE SIZE

Column Type: Steel Column Width: 4 in Column Depth: 4 in Baseplate Width: bsw = 6 inBaseplate Length: bsl = 6 in

FOOTING CALCULATIONS

| Bearing Calculations: | | |
|--|----------|----------|
| Ultimate Bearing Pressure: | Qu = | 1653 psf |
| Effective Allowable Soil Bearing Pressure: | Qe = | 2375 psf |
| Required Footing Area: | Areq = | 4.35 sf |
| Area Provided: | A = | 6.25 sf |
| Baseplate Bearing: | | |
| Bearing Required: | Bear = | 14699 lb |
| Allowable Bearing: | Bear-A = | 99450 lb |
| Beam Shear Calculations (One Way Shear): | | |
| Beam Shear: | Vu1 = | 3062 lb |
| Allowable Beam Shear: | Vc1 = | 14063 lb |
| | | |

Punching Shear Calculations (Two Way Shear): Critical Perimeter: Bo = 45 in Punching Shear: Vu2 = 12632 lb Allowable Punching Shear (ACI 11-35): vc2-a = 63281 lb Allowable Punching Shear (ACI 11-36): vc2-b =79688 lb 42188 lb Allowable Punching Shear (ACI 11-37): vc2-c = Controlling Allowable Punching Shear: 42188 lb vc2 =

Bending Calculations: Factored Moment: Mu = 38278 in-lb Nominal Moment Strength: Mn = 189895 in-lb

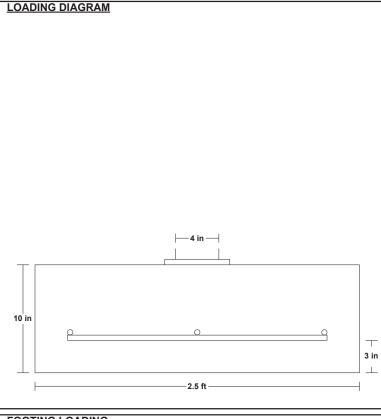
Reinforcement Calculations: Concrete Compressive Block Depth: a = 0.55 in Steel Required Based on Moment: As(1) =0.11 in2 Min. Code Req'd Reinf. Shrink./Temp. (ACI-10.5.4): As(2) = 0.54 in2 Controlling Reinforcing Steel: 0.54 in2 As-regd = Selected Reinforcement: #4's @ 11.0 in. o.c. e/w (3) Min. Reinforcement Area Provided: 0.59 in2 As =

Development Length Calculations:

Development Length Required: I d = 15 in Development Length Supplied: Ld-sup = 9.5 in

Note: Plain concrete adequate for bending,

therefore adequate development length not required.



FOOTING LOADING

Live Load: PL = 5757 lb * Dead Load: PD = 4573 lb * Total Load: PT = 10330 lb * Ultimate Factored Load: Pu = 14699 lb Footing plus soil above footing weight: Wt = 503 lb * Load obtained from Load Tracker. See Summary Report for details.

NOTES

Established Basic Permit #

Project: 19-002c Framing Location: FTG-PST-MLB2-3C

Footing

[2015 International Building Code(2015 NDS)] Footing Size: 2.5 FT x 2.5 FT x 12.00 IN

Reinforcement: #4 Bars @ 7.00 IN. O.C. E/W / (4) min.

Section Footing Design Adequate





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FOOTING PROPERTIES Allowable Soil Bearing Pressure: Qs = 2500 psfConcrete Compressive Strength: F'c = 2500 psi Reinforcing Steel Yield Strength: Fy = 60000 psiConcrete Reinforcement Cover: 3 in

FOOTING SIZE

Width: W = 2.5 ft Length: I = 2.5 ft Depth: Depth = 12 in Effective Depth to Top Layer of Steel: d = 8.25 in

COLUMN AND BASEPLATE SIZE

Column Type: Concrete Column Width: m = 4 inColumn Depth: n = 4 in

FOOTING CALCULATIONS

Bearing Calculations:

Ultimate Bearing Pressure: Qu = 1856 psf Effective Allowable Soil Bearing Pressure: Qe = 2350 psf Required Footing Area: Areq = 4.94 sf Area Provided: 6.25 sf A = **Baseplate Bearing:** Bearing Required: 17030 lb Bear = Allowable Bearing: Bear-A = 44200 lb Beam Shear Calculations (One Way Shear): Beam Shear: Vu1 = 2696 lb Allowable Beam Shear: Vc1 = 18563 lb Punching Shear Calculations (Two Way Shear): Critical Perimeter: Bo = 49 in

Vu2 = 14190 lb Punching Shear: Allowable Punching Shear (ACI 11-35): vc2-a = 90956 lb Allowable Punching Shear (ACI 11-36): 132413 lb vc2-b =Allowable Punching Shear (ACI 11-37): vc2-c = 60638 lb Controlling Allowable Punching Shear: vc2 = 60638 lb **Bending Calculations:** 47967 in-lb Mu =

Factored Moment:

Nominal Moment Strength: Mn = 334058 in-lb **Reinforcement Calculations:** Concrete Compressive Block Depth: 0.74 in a = Steel Required Based on Moment: As(1) =0.11 in2 Min. Code Req'd Reinf. Shrink./Temp. (ACI-10.5.4): As(2) = 0.65 in2

Controlling Reinforcing Steel: As-reqd = Selected Reinforcement: #4's @ 7.0 in. o.c. e/w (4) Min.

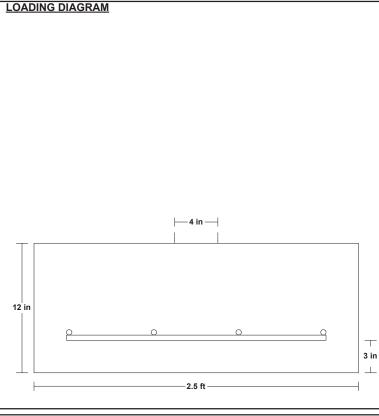
Development Length Calculations:

Reinforcement Area Provided:

Development Length Required: Ld = 15 in Development Length Supplied: Ld-sup = 10 in

Note: Plain concrete adequate for bending,

therefore adequate development length not required.



FOOTING LOADING

Live Load: 7780 lb * Dead Load: PD = 3818 lb 3 Total Load: PT = 11598 lb * Ultimate Factored Load: Pu = 17030 lb Footing plus soil above footing weight: Wt = 604 lb * Load obtained from Load Tracker. See Summary Report for details.

NOTES

Established Basic Permit #

Permit Number: 20-04893

0.65 in2

0.79 in2

As =

Project: 19-002c Framing Location: FTG-PST-MLB2-3B

Footing

[2015 International Building Code(2015 NDS)] Footing Size: 3.5 FT x 3.5 FT x 10.00 IN

Reinforcement: #4 Bars @ 11.00 IN. O.C. E/W / (4) min.

Section Footing Design Adequate





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FOOTING PROPERTIES Allowable Soil Bearing Pressure: Qs = 2500 psf Concrete Compressive Strength: F'c = 2500 psi Reinforcing Steel Yield Strength: Fy = 60000 psiConcrete Reinforcement Cover: 3 in

FOOTING SIZE Width:

W = 3.5 ft Length: I = 3.5 ft Depth: Depth = 10 in Effective Depth to Top Layer of Steel: 6.25 in

COLUMN AND BASEPLATE SIZE

Column Type: Concrete Column Width: m = 6 inColumn Depth: n = 8 in

FOOTING CALCULATIONS

| Bearing | Calculations: |
|---------|----------------|
| | - aioaiationoi |

Ultimate Bearing Pressure: Qu = 2158 psf Effective Allowable Soil Bearing Pressure: Qe = 2375 psf Required Footing Area: Areq = 11.13 sf Area Provided: 12.25 sf A = **Baseplate Bearing:** 37511 lb Bearing Required: Bear =

Allowable Bearing: Beam Shear Calculations (One Way Shear):

Beam Shear: Vu1 = 10494 lb Allowable Beam Shear: Vc1 = 19688 lb

Bear-A =

132600 lb

Punching Shear Calculations (Two Way Shear):

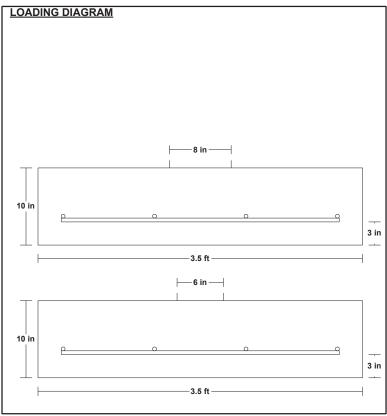
Bo = 53 in Critical Perimeter: Vu2 = 33799 lb Punching Shear: Allowable Punching Shear (ACI 11-35): vc2-a = 62109 lb Allowable Punching Shear (ACI 11-36): 83438 lb vc2-b =Allowable Punching Shear (ACI 11-37): vc2-c = 49688 lb Controlling Allowable Punching Shear: vc2 = 49688 lb **Bending Calculations:**

144686 in-lb **Factored Moment:** Mu = Nominal Moment Strength: Mn = 253752 in-lb **Reinforcement Calculations:**

Concrete Compressive Block Depth: 0.53 in Steel Required Based on Moment: As(1) =0.44 in2 Min. Code Req'd Reinf. Shrink./Temp. (ACI-10.5.4): As(2) = 0.76 in2 Controlling Reinforcing Steel: As-reqd = 0.76 in2 Selected Reinforcement: #4's @ 11.0 in. o.c. e/w (4) Min. Reinforcement Area Provided: 0.79 in2 As =

Development Length Calculations:

Development Length Required: Ld = 15 in Development Length Supplied: Ld-sup = 15 in



FOOTING LOADING

Live Load: $PI = 14470 \text{ lb}^3$ Dead Load: PD = 11966 lb * Total Load: PT = 26436 lb * Ultimate Factored Load: Pu = 37511 lb Footing plus soil above footing weight: Wt = 987 lb * Load obtained from Load Tracker. See Summary Report for details.

NOTES

Established Basic Permit #

Pacific Northwest Structural Group, LLC

| | Project: | Red Barn Lane - Duplex 1400 | By: | DLS |
|---|---------------------------------|--|--------------|---------|
| ı | Location: | NW Hogan Ln & Nels Nelson Rd NW, Bremerton, WA 98311 | Project No.: | 19-002c |
| ı | Client: Envision Northwest, LLC | | | odate: |
| | | 27-Apr-19 | | |

| Mark | Sheating Type, Nail Size, Panel Edges Fastener Spacing, & Capacity | Capacity (plf) |
|------------|---|----------------|
| A | 15/32" Sheathing W/ 8d @ 6" oc | 365 |
| ₿ | 15/32" Sheathing W/ 8d @ 4" oc | 533 |
| \Diamond | None | #N/A |

| Mark | Simpson Strong-Tie Holdowns | Capacity (lb) | Holdown Deflection at Highest Load (in) | |
|------|--------------------------------|------------------|--|-----------|
| 1 | HDU2-SDS2.5 W/ 3" Post | 3,075 | 0.088 | |
| 2 | HDU5-SDS2.5 W/ 3" Post | 5,645 | 0.115 | |
| 3 | HDU11-SDS2.5 W/ 5.5" Post | 9,535 | 0.137 | O SEISMIC |
| | None | N/A | N/A | WIND |
| | None | N/A | N/A | |
| | None | N/A | N/A | |
| | None | N/A | N/A | |
| | None | N/A | N/A | |
| | None | N/A | N/A | |
| | None | N/A | N/A | |
| | None | N/A | N/A | |
| | None | N/A | N/A | |

| Shear Wall Deflection | | | | |
|-----------------------|-----------|-----------------|--|--|
| G | 90,000 | psi | | |
| E | 1,200,000 | psi | | |
| Α | 8.25 | in ² | | |

| | | 0.11 | | | | | 2nd Level | | | | | | | | | | l st Level | | | | | | | | | | |
|--|-----|--------|--------------|--------------|---------|---------------|-------------|----------------------|-----------------------------------|----------|---------|--------------|----------|---------|--------------|-----------|--------------------------------------|-------|--------|---------------------------------|----------|---------|---------|---------|--|--|--|
| | | | 3rd Lev | /el | | | | | | | | 2nd Le | /el | | | | | | | 1st Lev | el | | | | | | |
| Lateral Tnb. Width ft | | 9.3 | Shearw | all Type | | | | | al Trib. Width | ft | 9.3 | Shearw | all Type | | | | Lateral Tnb. Width | ft | 9.3 | Shearwa | all Type | | | | | | |
| V from above k Uniform v this level p | | 115.7 | | | | | | | m above rm v this level | k | 1.1 | | | | | | V from above Uniform v this level | k | 2.7 | | | | | | | | |
| Total Wall Length ft | | 31.00 | < | / | | | | | Wall Length | PIF | 26.00 | \ \ \ \ \ | | | | | Total Wall Length | PIT | 36.00 | \ \rightarrow \(\rightarrow \) | | | | | | | |
| V this level k | | 1.1 | ~ | γ | | | | | s level | It. | 1.7 | \ \' | γ | | | | V this level | It. | 1.7 | \ \tag{\chi} | <i>y</i> | | | | | | |
| V accum. k | | 1.1 | | | | | | Vaco | | k. | 2.7 | | | | | | V accum. | k. | 4.4 | | | | | | | | |
| Unit Wall Shear p | e e | 35 | | | | | | | Vall Shear | юlf | 105 | | | | | | Unit Wall Shear | n)H | 122 | | | | | | | | |
| Shear Wall Capcity p | e e | 365 | | | | | | | r Wall Capcity | рlf | 365 | | | | | | Shear Wall Capcity | plf | 365 | | | | | | | | |
| Demand vs. Capoity Rat | 10 | 0.09 | | | | | | Dema | ind vs. Capcity R | atio | 0.29 | | | | | | Demand vs. Capcity I | Ratio | 0.33 | | | | | | | | |
| Apparent Stiffness, Ga K | /In | 10.00 | | | | | | Appar | ent Stiffness, Ga | K/In | 10.00 | | | | | | Apparent Stiffness, Ga | K/In | 10.00 | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Overturning Moment Overturning Moment | | | | | | | | | | | | | | | | | Overturning Moment | | | | | | | | | | |
| | | Wall I | Wall 2 | Wall 3 | Wall 4 | Wall 5 | Wall 6 | | | la n | Wall I | Wall 2 | Wall 3 | Wall 4 | Wall 5 | Wall 6 | | I. n | Wall I | Wall 2 | Wall 3 | Wall 4 | Wall 5 | Wall 6 | | | |
| | -ft | 20.9 | 9.00 | 9.00 | 9.00 | | | | | k-ft | 3.1 | 1.4 | 1.4 | 2.8 | 9.00 | - | M _{OT} from above | k-ft | 5.8 | 4.0 | 4.0 | 14.7 | 2.3 | - | | | |
| Story Ht ft Length ft | | 8.08 | 8.08 5.00 | 8.08 5.00 | 8.08 | - | | Ston | / Ht | 31 | 8.08 | 8.08 | 8.08 | 8.08 | 8.08 2.75 | - | Story Ht Lenath | 15 | 9.58 | 9.58 | - | 9.58 | - | | | | |
| Diaphragm Ratio | | 0.73 | 1.62 | 1.62 | 0.81 | - | _ | | n Iraam Ratio | 31 | 2.49 | 2.69 | 2.69 | 0.58 | 2.75 | - | Diaphraam Ratio | TC . | 0.87 | 0.87 | - | 0.68 | - | | | | |
| Modified Capacity | | 365 | 365 | 365 | 365 | | | | fied Capacity | | 294 | 271 | 2.65 | 365 | 248 | | Modified Capacity | | 365 | 365 | | 365 | | | | | |
| | -ft | 3.1 | 1.4 | 1.4 | 2.8 | | | Mor | | k-ft | 2.8 | 2.5 | 2.5 | 11.9 | 2.3 | | M or | k-ft | 12.9 | 12.9 | | 16.4 | | | | | |
| | -ft | 3.1 | 1.4 | 1.4 | 2.8 | - | - | Mor a | accum | k-ft | 5.8 | 4.0 | 4.0 | 14.7 | 2.3 | - | M _{OT} accum | k-ft | 18.7 | 16.8 | 4.0 | 31.1 | 2.3 | - | | | |
| | | She | ear Wall Di | | | | | | | | | ear Wall D | efection | | | | | | | ear Wall De | efection | | | | | | |
| Δ_{B} | | 0.016 | 0.035 | 0.035 | 0.018 | | | Δ_{B} | | ın | 0.166 | 0.179 | 0.179 | 0.038 | 0.196 | | Δ_{B} | ın | 0.095 | 0.095 | - | 0.074 | - | - | | | |
| Δ_{ee} | | 0.246 | 0.246 | 0.246 | 0.246 | - | - | Δ_{\lor} | | ın | 0.246 | 0.246 | 0.246 | 0.246 | 0.246 | - | Δ_{\bigvee} | ın | 0.291 | 0.291 | - | 0.291 | - | - | | | |
| Δ_{HD} | | - | - | - | - | | - | Δ_{MD} | | ın | | 0.237 | 0.237 | - | 0.259 | - | Δ_{HD} | ın | 0.077 | 0.077 | - | - | - | - | | | |
| Δ_{SW} | | 0.262 | 0.281 | 0.281 | 0.264 | - | - | Δ_{SW} | | m | 0.411 | 0.662 | 0.662 | 0.284 | 0.700 | - | $\Delta_{\sf SW}$ | ın | 0.463 | 0.463 | - | 0.366 | - | | | | |
| | | Re | esisting N | loment | | | | Resisting Moment | | | | | | | | R | esisting M | oment | | | | | | | | | |
| | -ft | - | - | - | - | - | - | M _R fr | om above | k-ft | 12.0 | 3.2 | 3.2 | 10.1 | - | - | M _R from above | k-ft | 13.6 | 4.6 | 4.6 | 28.6 | 1.3 | - | | | |
| DIDE WELL P | sf | 10.0 | 10.0 | 10.0 | 10.0 | - | - | Distr | Wall Wt | psf | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | - | Distr Wall Wt | psf | 10.0 | 10.0 | - | 10.0 | - | - | | | |
| Tnb above ft | | 6.0 | 6.0 | 6.0 | 6.0 | - | - | 1 | Trib above | ft | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | - | Tnb above | ft | 6.0 | 6.0 | - | 6.0 | - | - | | | |
| | sf | 12.0 | 12.0 | 12.0 | 12.0 | - | - | Wts. | Wt above | psf | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 | - | Wts. Wt above | psf | 12.0 | 12.0 | - | 12.0 | - | - | | | |
| End Hdr. Tnb ft | | - | - | - | | - | - | End | Hdr. Tnb tnb to hdr | 1E 44 | - | - | - | - | | - | End Hdr. Tnb tnb to hdr | 15 | - | - | - | - | - | | | | |
| | c f | | | | | | | Wts. | Wt to hdr | nei | | | | | | | Wts. Wt to hdr | net | | | | | | | | | |
| Disk to wall fit | | 11.00 | 5.00 | 5.00 | 10.00 | | | | Dist to wall | ft | 3.25 | 3.00 | 3.00 | 14.00 | 2.75 | | Diet to wall | ft | 11.00 | 11.00 | | 14.00 | - | | | | |
| resp. | , | 250 | 250 | 250 | 250 | - | - | Perp. | Wt of wall | lЬ | 250 | 250 | 250 | 250 | 250 | - | rerp. | lЬ | 500 | 500 | - | 500 | - | - | | | |
| Wall Dist to wall ft | | - | - | - | - | - | - | Wall Wts. | Dist to wall | ft | - | - | - | - | - | - | Wall Wts. Dist to wall | ft | - | - | - | - | - | - | | | |
| Wt of wall | , | - | - | - | - | - | - | | Wt of wall | lb | - | - | - | - | - | - | Wt of wall | lЬ | - | - | - | - | - | - | | | |
| | -ft | 11.99 | 3.16 | 3.16 | 10.14 | - | - | | ns level | k-ft | 1.62 | 1.44 | 1.44 | 18.47 | 1.27 | - | M _R this level | k-ft | 15.65 | 15.65 | | 23.44 | - | - | | | |
| M _R accum k | -ft | 11.99 | 3.16 | 3.16 | 10.14 | - | - | M _R as | ocum | k-ft | 13.61 | 4.60 | 4.60 | 28.61 | 1.27 | - | M _R accum | k-ft | 29.27 | 20.25 | 4.60 | 52.06 | 1.27 | - | | | |
| | | | old Down | | | | | | | | | old Down | | | | | | | | old Down I | | | | | | | |
| Wt. Reduction | | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | | Leduction | | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | Wt. Reduction | | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | | | |
| T _R accum HD Offset | - | 1.09 | 0.63 | 0.63 | 1.01 | - | - | | T _R accum HD Offset | | 4.19 | 1.53 | 1.53 | 2.04 | 0.46 | - | T _R accum HD Offset | k | 2.66 | 1.84 | - | 3.72 | - | - | | | |
| HD Force | | - | - | - | - | - | - | | HD Force | | - | 0.40 | 0.40 | 4.00 | 0.57 | - | HD Force | | 0.10 | 0.42 | - | - | - | - | | | |
| HD Capacity | - 1 | - | - | | - | | | | HD Capacity | | - | 3.08 | 3.08 | | 3.08 | - | HD Capacity | k | 3.08 | 3.08 | - | | - | | | | |
| Hold Down Type | | 0 | <u></u> | <u></u> | <u></u> | 0 | <u></u> | | told Down Typ | e | <u></u> | 1 | 1 | <u></u> | 1 | <u></u> | Hold Down Ty | ре | 1 | 1 | <u></u> | <u></u> | <u></u> | <u></u> | | | |
| | | | | Project: | Red B | iarn Lane - I | Duplex 1400 | | | | | | | | | | By: | | | DLS | | | | | | | |
| | | | | Location: | TF-1 | | | | | | | | | | | | Job No.: | | | 19-002c | | | | | | | |
| Cont. Envison Northwest, LLC | | | | | | | | | | | | Last Update: | | | | 27-Apr-20 | | | | | | | | | | | |
| Walter Walter | | | | | | | | | | | | | | | , | | | | 4 | | | | | | | | |
| Wood Shear Wall Design Aid Comments: See Perforated Shear Calculations | | | | | | | | | | | | | | | | | | | | | | | | | | | |

Established Basic Permit #

19-03646

| | | | 3rd Lev | vel | | | | | | | 2nd Le | vel | | | | | | | 1st Lev | el | | | |
|---|----------------|----------------------------|-------------|-----------|---------|---------------|-------------|---|----------------|------------------------------|----------------|----------|--------------|---------|------------|---|----------------|------------------------------|-------------|----------|---------|---------|---------|
| Lateral Trib. Width V from above Uniform v this level Total Wall Length | ft k plf | 9.3 - 115.7 16.50 | Shearw | all Type | | | | Lateral Trib. Width V from above Uniform v this level Total Wall Lenath | ft k plf | 9.3 1.1 178.7 16.50 | Shearw | all Type | | | | Lateral Trib, Width V from above Uniform v this level Total Wall Length | ft k plf | 9.3 2.7 178.7 20.50 | Shearw | | | | |
| V this level V accum. Unit Wall Shear | k k plf | 1.1 1.1 65 | | <i>y</i> | | | | V this level V accum. Unit Wall Shear | k k pH | 1.7 2.7 166 | | <i>y</i> | | | | V this level V accum. Unit Wall Shear | k k plf | 1.7 4.4 214 | | <i></i> | | | |
| Shear Wall Capcity Demand vs. Capcity Apparent Stiffness, Ga | | 365 0.18 10.00 | • | | | | | Shear Wall Capcity Demand vs. Capcity Apparent Stiffness, Ga | | 365 0.45 10.00 | | | | | | Shear Wall Capcity Demand vs. Capcity R Apparent Stiffness, Ga | | 365 0.59 10.00 | | | | | |
| | | Ov | erturning l | Moment | | | | | | Ov | erturning | Moment | | | | | | Ove | erturning l | Moment | | | |
| | | Wall I | Wall 2 | Wall 3 | Wall 4 | Wall 5 | Wall 6 | | | Wall I | Wall 2 | Wall 3 | Wall 4 | Wall 5 | Wall 6 | | | Wall I | Wall 2 | Wall 3 | Wall 4 | Wall 5 | Wall 6 |
| M _{OT} from above | k-ft | 0.00 | | | | | | M _{OT} from above | k-ft | 2.8 | 5.9 | - | - | - | | M _{OT} from above | k-ft | 9.8 | 21.0 | - | - | - | - |
| Story Ht | ft. | 8.08 | 8.08 | - | | - | - | Story Ht | ft. | 8.08 | 8.08 | - | | | - | Story Ht | 1t | 9.58 | 9.58 | - | - | - | - |
| Length Diaphragm Ratio | TE | 5.25 | 0.72 | - | | - | - | Length Diaphragm Ratio | TE. | 5.25 | 0.72 | - | - | - | - | Length Diaphragm Ratio | 10 | 9.25 | 0.85 | - | | | |
| Modified Capacity | | 365 | 365 | | | | | Modified Capacity | | 365 | 365 | | | | | Modified Capacity | | 365 | 365 | | | | |
| M ot | k-ft | 2.8 | 5.9 | - | - | - | - | M _{OT} | k-ft | 7.0 | 15.1 | - | - | - | - | M ot | k-ft | 19.0 | 23.1 | - | - | | - |
| M _{OT} accum | k-ft | 2.8 | 5.9 | - | - | - | - | M _{OT} accum | k-ft | 9.8 | 21.0 | - | - | - | - | M _{OT} accum | k-ft | 28.8 | 44.1 | - | - | - | - |
| | | She | ear Wall D | efection | | | | | | Sh | ear Wall D | efection | | | | | | She | ear Wall Di | efection | | | |
| Δ_{B} | ın | 0.063 | 0.030 | - | - | - | - | Δ_{B} | ın | 0.162 | 0.075 | - | - | - | - | Δ_{B} | ın | 0.198 | 0.162 | - | - | - | - |
| Δ_{\bigvee} | ırı | 0.246 | 0.246 | - | | - | - | Δ_{\lor} | ın | 0.246 | 0.246 | - | - | - | - | Δ_{\lor} | ırı | 0.291 | 0.291 | | | - | |
| Δ_{HD} | ın | - | - | - | - | - | - | Δ_{HD} | ın | 0.135 | 0.063 | - | - | - | - | Δ_{HD} | ın | 0.091 | 0.075 | - | - | - | - |
| $\Delta_{\sf SW}$ | ırı | 0.309 | 0.275 | - | | - | - | Δ_{SW} | ın | 0.543 | 0.384 | - | - | | - | $\Delta_{\sf SW}$ | ırı | 0.580 | 0.529 | | | - | - |
| | | R | esisting N | 1oment | | | | | | R | esisting N | 1oment | | | | | | R | esisting N | loment | | | |
| M _R from above | k-ft | - | - | - | - | - | - | M _R from above | k-ft | 4.9 | 10.9 | - | - | - | - | M _R from above | k-ft | 8.3 | 25.5 | - | - | - | - |
| Distr Wall Wt | psf | 10.0 | 10.0 | - | - | - | - | Distr Wall Wt | psf | 10.0 | 10.0 | - | - | - | - | Distr Wall Wt | psf | 10.0 | 10.0 | - | - | | - |
| Tnb above | ft | 6.0 | 6.0 | - | - | - | - | Trib above | ft | 6.0 | 8.8 | - | - | - | - | Tnb above | ft | 6.0 | 6.0 | - | - | - | - |
| Wts. Wt above | psf | 12.0 | 12.0 | - | - | - | - | Wts. Wt above | psf | 12.0 | 12.0 | - | - | - | - | Wts. Wt above | psf | 12.0 | 12.0 | - | - | - | - |
| End Hdr. Tnb | ft. | | - | - | | - | | End Hdr. Tnb | 7E | - | - | - | | | - | End Hdr. Tnb | ft- | | - | | - | - | |
| Wts. Wt to hdr | psf | | - | | - | | - | Wts. Wt to hdr | psf | | - | | | - | | Wts. Wt to hdr | psf | - | | - | | - | |
| Poor Dist to wall | ft | 11.00 | 5.00 | - | - | - | - | Poss Dist to wall | ft | 5.25 | 11.25 | - | - | - | - | Poor Dist to wall | ft | 9.25 | 11.25 | - | - | - | - |
| Wt of wall | lb | 250 | 250 | - | - | - | - | We of wall | lb | 250 | 250 | - | - | - | - | Wt of wall | lЬ | 250 | 250 | - | - | - | - |
| We Dist to wall | ft | - | - | - | - | - | - | W/sc Dist to wall | ft | - | - | - | - | - | - | Who Dist to wall | ft | - | - | - | - | - | - |
| Wt of wall | lb. | 4.86 | | - | - | - | - | Wt of wall | lb. | 3.42 | | - | - | - | - | Wt of wall | lb fr | - 0.45 | 10.47 | - | - | - | - |
| M _R this level M _R accum | k-ft k-ft | 4.86 | 10.92 | | | | - | M _R this level M _e accum | k-ft k-ft | 8.27 | 14.57 25.49 | | - | | - | M _R this level M _P accum | k-ft k-ft | 9.49 | 13.43 | | | - | |
| WK accom | K-10 | | old Down | Forces | | | | my accom | KHIL | | old Down | Forces | | | | IVIK SCCOIII | A-10 | | old Down | Forces | | | |
| Wt. Reduction | | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | Wt. Reduction | | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | Wt. Reduction | - | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 |
| T _P accum | 1 | 0.60 | 0.60 | 0.60 | - 0.60 | 0.60 | -0.00 | T _P accum | | 1.58 | 2.27 | 0.60 | 0.60 | - 0.60 | 0.60 | T _p accum | | 1.92 | 3.46 | 0.60 | 0.60 | - 0.60 | 0.60 |
| HD Offset | - | - 0.02 | | - | - | - | - | HD Offset | | - | - | - | - | - | | HD Offset | | - | - | - | - | - | - |
| HD Force | , i | - | - | - | - | - | - | HD Force | | 0.92 | 0.51 | - | - | - | - | HD Force | k | 1.96 | 1.84 | - | - | - | - |
| HD Capacity | ķ | - | | - | - | - | - | HD Capacity | | 3.08 | 3.08 | - | - | - | - | HD Capacity | k | 3.08 | 3.08 | - | - | | - |
| Hold Down Ty | уре | 0 | <u></u> | 0 | <u></u> | 0 | <u></u> | Hold Down Ty | ре | 1 | 1 | <u></u> | <u></u> | <u></u> | <u></u> | Hold Down Typ | pe | 1 | 1 | <u></u> | <u></u> | <u></u> | <u></u> |
| | | | | Project: | Red E | Barn Lane - I | Duplex 1400 | | | | | | | | | By: | ly: DLS | | | | | | |
| | | | | Location: | TF-2 | | | | | | | | | | | Job No.: | | | | 19-002 | 20 | | |
| | | Clent: | on Northwes | t IIC | | | | | | | | | Last Undate: | | | | 27-Apr-20 | | | | | | |
| | | | Coent: | | | - | | | | | | | | | ian opone: | | | | 27-Apr-20 | | | | |
| 1 | | | | | wood Sh | ear Wall Des | ign Ald | Comments: | | | | | | | | | | | | | | | |

| | | | 3rd Lev | rel | | | | | | | | 2nd Le | vel | | | | | | | 1st Lev | el | | | |
|-----------------------------|-------------|--------------|-------------|-----------|-----------------|--|-------------|----------------------|---------------------------|--------|--------|------------|-------------|--------|--------|--------|----------------------------|------------|--------|-------------|-------------|--------|--------|---------|
| Lateral Tnb. Width f | ft | 18.5 | Shearw | all Type | | | | | al Trib. Width | ft | 18.5 | Shearw | all Type | | | | Lateral Trib. Width | ft | 18.5 | Shearwa | all Type | | | |
| V from above k | k | - | | 71 | | | | | m above | k | 1.6 | | 71 | | | | V from above | k | 3.4 | | 71 | | | |
| Uniform v this level p | plf r | 88.3 7.84 | < | | | | | | rm v this level | plf | 96.0 | < | <i>></i> | | | | Uniform v this level | plf | 101.6 | < P | | | | |
| Total Wall Length f | ft . | | | ' | | | | | Wall Length | 杜 | | | ~ | | | | Total Wall Length | řt. | | \ \' | <i>></i> | | | |
| V this level k V accum. k | k | 1.6 | | | | | | V the | s level | k | 1.8 | | | | | | V this level V accum. | k | 1.9 | | | | | |
| Unit Wall Shear p | K will | 208 | | | | | | | Wall Shear | K will | 261 | | | | | | Unit Wall Shear | K | 351 | | | | | |
| Shear Wall Capcity p | pii niii | 365 | | | | | | | ir Wall Capcity | рlf | 365 | | | | | | Shear Wall Capcity | pli pli | 365 | | | | | |
| Demand vs. Capcity Rat | r= | 0.57 | | | | | | | and vs. Capcity R | F | 0.71 | | | | | | Demand vs. Capcity | Rotio | 0.96 | | | | | |
| Apparent Stiffness, Ga K | КЛп | 10.00 | | | | | | | rent Stiffness, Ga | | 10.00 | | | | | | Apparent Stiffness, Ga | | 10.00 | | | | | |
| | | | | | | | | | | | | | | | | | 7, | | | | | | | |
| | | Ove | erturning l | Moment | | | | | | | Ov | erturning | Moment | | | | | | Ove | erturning N | Moment | | | |
| | | Wall I | Wall 2 | Wall 3 | Wall 4 | Wall 5 | Wall 6 | | | | Wall I | Wall 2 | Wall 3 | Wall 4 | Wall 5 | Wall 6 | | | Wall I | Wall 2 | Wall 3 | Wall 4 | Wall 5 | Wall 6 |
| | k-ft | | | | | | | | from above | k-ft | 4.1 | 5.1 | 4.1 | - | - | - | M _{OT} from above | k-ft | 9.3 | 13.6 | 9.3 | 4.2 | 4.2 | - |
| Story Ht f | ft | 8.08 | 8.08 | 8.08 | - | - | - | Ston | y Ht | ft | 8.08 | 8.08 | 8.08 | 8.08 | 8.08 | - | Story Ht | ft | 9.58 | 9.58 | 9.58 | 9.58 | 9.58 | - |
| Length f | ft | 2.42 | 3.00 | 2.42 | - | - | - | Leng | | ft | 2.50 | 4.08 | 2.50 | 2.00 | 2.00 | - | Length | ft | 1.75 | 7.58 | 1.75 | 2.00 | 2.00 | - |
| Diaphragm Ratio | | 3.34 | 2.69 | 3.34 | - | - | - | | nragm Ratio | | 3.23 | 1.98 | 3.23 | 4.04 | 4.04 | - | Diaphragm Ratio | | 5.47 | 1.26 | 5.47 | 4.79 | 4.79 | - |
| Modified Capacity | | 219 | 271 | 219 | - | - | - | Mod | ified Capacity | | 226 | 365 | 226 | N/A | N/A | - | Modified Capacity | | N/A | 365 | N/A | N/A | N/A | - |
| | k-ft | 4.1 | 5.1 | 4.1 | - | - | - | M ot | | k-ft | 5.3 | 8.6 | 5.3 | 4.2 | 4.2 | - | M _{OT} | k-ft | 5.9 | 25.5 | 5.9 | 6.7 | 6.7 | - |
| M _{OT} accum | k-ft | 4.1 | 5.1 | 4.1 | - | - | - | M _{OT} : | accum | k-ft | 9.3 | 13.6 | 9.3 | 4.2 | 4.2 | - | M _{OT} accum | k-ft | 15.2 | 39.1 | 15.2 | 10.9 | 10.9 | - |
| | | She | ear Wall D | efection | | | | | | | Sh | ear Wall D | efection | | | | | | She | ear Wall De | efection | | | |
| Δ _B | ın | 0.440 | 0.355 | 0.440 | | - | - | Δ_{B} | | ın | 0.533 | 0.327 | 0.533 | 0.667 | 0.667 | - | Δ_{B} | ın | 1.709 | 0.395 | 1.709 | 1.495 | 1.495 | - |
| Δ_{V} | ın | 0.246 | 0.246 | 0.246 | - | - | - | $\Delta_{\lor/}$ | | ın | 0.246 | 0.246 | 0.246 | 0.246 | 0.246 | - | Δ_{\bigvee} | ın | 0.291 | 0.291 | 0.291 | 0.291 | 0.291 | - |
| Δ _{HD} | ırı | 0.294 | 0.237 | 0.294 | | - | - | Δ_{HD} | | ın | 0.372 | 0.174 | 0.372 | 0.356 | 0.356 | - | Δ_{HD} | ın | 0.750 | 0.145 | 0.750 | 0.551 | 0.551 | - |
| Δ_{SW} | m | 0.980 | 0.838 | 0.980 | - | - | - | Δ_{SW} | | ırı | 1.151 | 0.747 | 1.151 | 1.268 | 1.268 | - | Δ_{SW} | ın | 2.750 | 0.831 | 2.750 | 2.337 | 2.337 | - |
| | | R | esisting N | loment | | | | | | | R | esisting N | Noment | | | | | | R | esisting M | oment | | | |
| M _R from above k | k-ft | - | - | - | - | - | - | M _R fr | om above | k-ft | 0.8 | 1.2 | 0.8 | - | - | - | M _R from above | k-ft | 1.3 | 2.5 | 1.3 | 0.3 | 0.3 | - |
| Distr Wall Wt p | psf | 10.0 | 10.0 | 10.0 | - | - | - | Distr | Wall Wt | psf | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | - | Distr Wall Wt | psf | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | - |
| . Tnb above f | ft | 16.3 | 16.3 | 16.3 | - | - | - | | Trib above | ft | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | - | - Trib above | ft | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | - |
| | psf | 12.0 | 12.0 | 12.0 | - | - | - | Wts. | Wt above | psf | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 | - | Wts. Wt above | psf | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 | - |
| End Hdr. Tnb f | ft | - | - | - | - | - | - | End | Hdr. Tnb | ft | - | - | - | - | - | - | End Hdr. Tnb | ft | - | - | - | - | - | - |
| Wts. tnb to hdr f | tt nef | - | - | - | - | - | - | Wts. | tnb to hdr | łt, | - | - | - | - | - | - | Wts. tnb to hdr | ft, | - | - | - | - | - | - |
| Wt to hdr p | pst tr | - | - | | - | - | | | Wt to hdr Dist to wall | psf | - | - | - | - | - | | Wt to hdr Dist to wall | pst | - | - | - | - | - | - |
| rerp. | lh | | - | | | | | Perp. | Wt of wall | lh | - | | | | | | resp. We of wall | lb. | | - | - | | | |
| Wall Dick to wall 6 | f+ | | | | | | | Wall | Dist to wall | f+ | | | | | | | Wall Dick to wall | f+ | | | | | | |
| Wts. Wt of wall | lb | | | | | | | Wts. | Wt of wall | lb | | | | | | | Wts. Wt of wall | lb | | | | | | |
| | k-ft | 0.81 | 1.24 | 0.81 | - | | - | Mo ti | his level | k-ft | 0.48 | 1.27 | 0.48 | 0.31 | 0.31 | | Me this level | k-ft | 0.26 | 4.82 | 0.26 | 0.34 | 0.34 | - |
| M _R accum k | k-ft | 0.81 | 1.24 | 0.81 | - | - | - | | ccum | k-ft | 1.29 | 2.51 | 1.29 | 0.31 | 0.31 | - | M _p accum | k-ft | 1.54 | 7.33 | 1.54 | 0.64 | 0.64 | - |
| | | Ho | old Down | Forces | | | | | | | н | old Down | Forces | | | | | | Ho | old Down I | Forces | | | |
| Wt. Reduction | | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | Wt. F | Reduction | | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | Wt. Reduction | | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 |
| T _R accum | į, | 0.33 | 0.41 | 0.33 | - | - | - | | T _R accum | | 0.51 | 0.62 | 0.51 | 0.15 | 0.15 | - | T _R accum | k | 0.88 | 0.97 | 0.88 | 0.32 | 0.32 | - |
| HD Offset | f | - | - | - | - | - | - | | HD Offset | | - | - | - | - | - | - | HD Offset | f | - | - | - | - | - | - |
| HD Force | ķ | 1.48 | 1.44 | 1.48 | - | - | - | | HD Force | | 3.43 | 2.97 | 3.43 | 2.01 | 2.01 | - | HD Force | k | 8.17 | 4.58 | 8.17 | 5.27 | 5.27 | - |
| HD Capacity | ķ | 3.08 | 3.08 | 3.08 | - | - | - | | HD Capacity | | 5.65 | 3.08 | 5.65 | 3.08 | 3.08 | - | HD Capacity | k | 9.54 | 5.65 | 9.54 | 5.65 | 5.65 | - |
| | | \bigcirc | \odot | 0 | <u></u> | 0 | 0 | 1 | Hold Down Typ | e e | 2 | () | 2 | 1 | 1 | 0 | Hold Down Ty | pe | 3 | 2 | 3 | 2 | 2 | <u></u> |
| Hold Down Type | _ | _ | | | | | | 1400 | | | | | | | | By: | | DLS | | | | | | |
| Hold Down Type | | | | Project: | Red E | Barn Lane - I | Duplex 1400 | | | | | | | | | | | | | | DLS | | | |
| Hold Down Type | | | | Project: | | Barn Lane - I | Duplex 1400 | 0 | | | | | | | | | - | | | | | 'c | | |
| Hold Down Type | | | | Location: | LF-1 | | | ט | | | | | | | | | Job No.: | | | | 19-002 | | | |
| Hold Down Type | | | | - | LF-1 Envisio | Barn Lane - I on Northwes ear Wall Des | t, LLC | 0 | | | | | | | | | - | | | | | | | |

Established Basic Permit #

19-03646

| | | 2nd Level | | | | | | | | | | lst Level | | | | | | | | | | | | |
|--|-----|--------------|-------------|----------------------|----------|--------------|-------------|-------------------|-----------------------------------|------|------------|---------------------|-------------|-------------|----------|----------|---|--------------|----------------|-------------|---------------------|-------------|----------|---------|
| | | | 3rd Lev | /el | | | | | | | | 2nd Le | /el | | | | | | | 1st Lev | rel | | | |
| Lateral Tnb. Width ft | | 18.5 | Shearwa | all Type | | | | | al Trib. Width | ft | 18.5 | Shearw | all Type | | | | Lateral Trib. Width | ft | 20.0 | Shearw | all Type | | | |
| V from above k | | - | | 71 | | | | | m above | k | 1.6 | | 71 | | | | V from above | k | 3.4 | | 71 | | | |
| Uniform v this level pli Total Wall Length ft | | 88.3 | | | | | | | rm v this level | PIF | 96.0 | \ \ \ \ \ | | | | | Uniform v this level Total Wall Length | PIT | 101.6 30.08 | <i> </i> | | | | |
| V this level k | | 1.6 | ~ | \sim | | | | | Wall Length | 31 | 1.8 | / | γ | | | | V this level | 15 | 2.0 | \ \' | γ | | | |
| V triis ievei k | | 1.6 | | | | | | V acc | | K. | 3.4 | | | | | | V accum. | K L | 5.4 | | | | | |
| Unit Wall Shear pl | | 77 | | | | | | | Vall Shear | nlf | 108 | | | | | | Unit Wall Shear | nH | 181 | | | | | |
| Shear Wall Capcity pl | | 365 | | | | | | | r Wall Capcity | рlf | 365 | | | | | | Shear Wall Capcity | plf | 365 | | | | | |
| Demand vs. Capcity Ratio | 2 | 0.21 | | | | | | | ind vs. Capcity R | atio | 0.30 | | | | | | Demand vs. Capcity | Ratio | 0.50 | | | | | |
| Apparent Stiffness, Ga KJ | | 10.00 | | | | | | | ent Stiffness, Ga | | 10.00 | | | | | | Apparent Stiffness, Ga | | 10.00 | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | |
| | | Ove | erturning l | Moment | | | | | | | Ov | erturning | Moment | | | | | | Ove | erturning l | Moment | | | |
| | | Wall I | Wall 2 | Wall 3 | Wall 4 | Wall 5 | Wall 6 | | | | Wall I | Wall 2 | Wall 3 | Wall 4 | Wall 5 | Wall 6 | | | Wall I | Wall 2 | Wall 3 | Wall 4 | Wall 5 | Wall 6 |
| M _{OT} from above k- | ft | | | | | | | | | k-ft | 2.0 | 2.0 | 1.6 | 1.9 | - | - | M _{OT} from above | k-ft | 5.3 | 5.3 | 3.7 | 14.2 | - | - |
| Story Ht ft | | 8.08 | 8.08 | 8.08 | 8.08 | - | - | | / Ht | ft | 8.08 | 8.08 | 8.08 | 8.08 | - | - | Story Ht | ft | 9.58 | - | - | 9.58 | - | - |
| Length ft | | 3.25 | 3.25 | 2.50 | 3.08 | - | - | Lengt | | ft | 3.75 | 3.75 | 2.50 | 14.08 | - | - | Length | ft | 11.50 | - | - | 7.08 | - | - |
| Diaphragm Ratio | | 2.49 | 2.49 | 3.23 | 2.62 | - | - | | iragm Ratio | | 2.15 | 2.15 | 3.23 | 0.57 | - | - | Diaphragm Ratio | | 0.83 | - | - | 1.35 | - | - |
| Modified Capacity | Ea. | 294 | 294 | 226 | 278 | - | - | Modi | fied Capacity | 1 6 | 339 | 339 | 226 | 365 | - | - | Modified Capacity | k-ft | 365 | - | - | 365 | - | - |
| M ot k- | | 2.0 | 2.0 | 1.6 | 1.9 | | - | M OT | | k-ft | 3.3 | 3.3 5.3 | 2.2 3.7 | 12.3 | - | - | M OT | k-ft k-ft | 19.9 | | 3.7 | 12.3 | - | |
| M _{OT} accum k- | it | | | 1.6 | 1.9 | - | - | IVIOT 2 | accum | k-ft | 5.3 | | | 14.2 | - | - | M _{OT} accum | K-ft | 25.2 | 5.3 | | 26.5 | - | |
| Δ _B | Ŧ, | 5he 0.122 | o.122 | 0.159 | 0.129 | | | $\Delta_{\rm Pl}$ | | | 0.147 | ear Wall D 0.147 | 0.221 | 0.039 | | | $\Delta_{P_{I}}$ | L | 0.134 | ear Wall D | etection | 0.218 | | |
| Δ _V | | 0.122 | 0.122 | 0.159 | 0.129 | - | | Δ_{V} | | ın | 0.147 | 0.147 | 0.221 | 0.039 | | - | Δ_{\vee} | ın | 0.134 | | | 0.218 | - | |
| Δ _{HD} in | | 0.219 | 0.219 | 0.284 | 0.2.10 | | | Δ_{HD} | | ın | 0.190 | 0.190 | 0.284 | 0.051 | | | Δ_{HD} | ın | 0.073 | | - | 0.119 | | |
| Δ _{SW} | | | | | | | | Δ_{SW} | | | | | | | | | Δ_{SW} | | | | | | | |
| in in | - | 0.587 | 0.587 | 0.689 | 0.374 | - | - | -45W | | ırı | 0.583 | 0.583 | 0.751 | 0.335 | - | - | M⊃W . | ın | 0.499 | | - | 0.628 | - | - |
| | | Ke | esisting M | loment | | | | | | | | esisting N | | | | | | | | esisting N | | | | |
| M _R from above k- | | - | - | - | - | - | - | | om above | k-ft | 1.6 | 1.6 | 1.5 | 2.8 | - | - | M _R from above | k-ft | 2.7 | 2.7 | 2.0 | 18.0 | - | - |
| Distr Wall Wt ps | ið | 10.0 | 10.0 | 10.0 | 10.0 | - | - | Distr | Wall Wt | psf | 10.0 | 10.0 | 10.0 | 10.0 | - | - | Distr Wall Wt | psf | 10.0 | - | - | 10.0 | - | |
| . This above ft Wts. Wt above ps | | 12.0 | 6.0 12.0 | 16.3 | 16.3 | - | - | Wts. | Trib above Wt above | nef | 12.0 | 12.0 | 6.0 12.0 | 6.0 12.0 | | - | Trib above Wts. Wt above | nsf psf | 6.0 12.0 | - | | 6.0 12.0 | | |
| Hale Tolo 68 | 20 | 12.0 | 12.0 | 12.0 | 12.0 | | _ | | Hdr. Tnb | Sh. | 12.0 | 12.0 | 12.0 | 12.0 | | _ | Hule Tele | EP. | 12.0 | | | 12.0 | | |
| End to hote ft | | | | | - | | | End | tnb to hdr | ft. | | | | | | | End to har | ft | | | | | | |
| Wts. Wt to hdr ps | d . | - | - | - | - | - | - | Wts. | Wt to hdr | psf | - | - | - | - | - | - | Wts. Wt to hdr | psf | - | - | - | - | - | - |
| Dist to wall fit | | 3.25 | 3.25 | 2.50 | 3.08 | - | - | D | Dist to wall | ft | - | - | - | - | - | - | Diet to wall | ft | - | - | - | - | - | - |
| Perp. Wt of wall Ib | | 250 | 250 | 250 | 500 | - | - | Perp. Wall | Wt of wall | lb | - | - | - | - | - | - | Perp. Wall Wt of wall | lЬ | - | - | - | - | - | - |
| Wts. Dist to wall ft | | - | - | - | - | - | - | Wts. | Dist to wall | ft | - | - | - | - | - | - | Wts. Dist to wall | ft | - | - | - | - | - | - |
| Wt of wall Ib | | - | - | - | - | - | - | | Wt of wall | lb | - | - | - | - | - | - | Wt of wall | lb | - | - | | - | - | - |
| M _R this level k- | ft | 1.62 | 1.62 | 1.49 | 2.85 | - | - | | ns level | k-ft | 1.07 | 1.07 | 0.48 | 15.15 | - | - | M _R this level | k-ft | 11.10 | - | - | 4.21 | - | - |
| M _R accum k- | it | 1.62 | 1.62 | 1.49 | 2.85 | - | - | M _R as | ocum | k-ft | 2.69 | 2.69 | 1.96 | 17.99 | - | - | M _R accum | k-ft | 13.79 | 2.69 | 1.96 | 22.20 | - | - |
| | | | ld Down I | | | | | | | | | old Down | | | | | | | | old Down | | | | |
| Wt. Reduction | | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | | Leduction | | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | Wt. Reduction | _ | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 |
| T _R accum HD Offset | - 1 | 0.50 | 0.50 | 0.59 | 0.92 | - | - | | T _R accum HD Offset | | 0.72 | 0.72 | 0.79 | 1.28 | - | - | T _R accum HD Offset | k | 1.20 | - | - | 3.14 | - | |
| HD Offset | - | - | - | - 0.07 | - | - | - | | HD Force | | - | - | - | 7.00 | - | - | HD Force | - 1 | - 1.40 | - | - | - | - | - |
| HD Capacity | - | 0.33 | 0.33 | 0.27 3.08 | - | - | - | | HD Capacity | | 0.98 | 0.98 | 1.03 | 0.48 | - | - | HD Capacity | k | 1.48 | - | - | 1.86 | - | - |
| Hold Down Type | , | 3.00 | 1 | 1 | <u>.</u> | <u>.</u> | <u>.</u> | | told Down Typ | e | 1 | 3.00 | 1 | 1 | <u>.</u> | <u>.</u> | Hold Down Ty | rpe . | 1 | <u>.</u> | <u>.</u> | 1 | <u>.</u> | <u></u> |
| | | | | Project: | Red B | arn Lane - I | Duplex 1400 |) | | | | | | | | | By: | | DLS | | | | | |
| | | | | | | | | | | | | | | | 19-002c | | | | | | | | | |
| | | | | Location: | LF-2 | | | | | | | | | | | | Job No.: | | | | 19-002 | !c | | |
| | | | | | | n Northwes | * IIC | | | | | | | | | | | | | | | | | - |
| | | | | Location: Client: | Envisio | on Northwes | | | Comments: | | See Perfor | | | | | | Job No.: Last Update: | | | | 19-002 27-Apr-20 | | | |

Established Basic Permit #

19-03646

| Project: | Red Barn Lane - Duplex 1400 | By: | DLS |
|-----------|--|---------------|-----------|
| Location: | NW Hogan Ln & Nels Nelson Rd NW, Bremerton, WA 983 | Project No.: | 19-002c |
| Client: | Envision Northwest, LLC | Last Update: | 27-Apr-19 |
| | PERFORATED SHEAR WALL EFFECTIVE SHEAR CA | APACITY RATIO | |

| Wall Line | Force to Wall [P] (K) | Total Length of Wall [L] (ft) | Length of Full Height Shearwall [A I +A3+A5] (ft) | Unit Shear in Wall (plf) | Percent Full Height Sheathing | Plate Height [H] (ft) | Unrestrain | ed Opening (B2+B3) | Effective Shear Capacity Ratio | Required Capacity (plf) | Shearwall Capacity (plf) | Ratio | Revised Shearwall Type | Combined Resisting Force (K) | Required Uplift Capacity (K) | Revised Holdown Type |
|------------------|--------------------------------|--|--|-----------------------------------|-------------------------------------|-----------------------------|------------|-----------------------|---|-------------------------------|--------------------------------|--------|------------------------------|---------------------------------------|---------------------------------------|----------------------------|
| TF-1-2-WL \$ 5 | 0.63 | 8.25 | 6.00 | 105 | 73% | 8 | 5 | 62% | 0.799 | 132 | 365 | 0.3608 | А | 4.19 | (3.12) | <u>-</u> |
| TF-1-2-WL 2 \$ 3 | 0.63 | 11.00 | 6.00 | 105 | 55% | 8 | 5 | 62% | 0.724 | 145 | 365 | 0.3979 | А | 1.53 | (0.36) | <u>-</u> |
| LF-1-2-WL \$ 4 | 1.17 | 13.00 | 4.50 | 261 | 35% | 8 | 5 | 62% | 0.650 | 401 | 532.5 | 0.7529 | В | 0.51 | 2.73 | |
| LF-2-3-WL \$ 2 | 0.50 | 11.50 | 6.50 | 77 | 57% | 8 | 5 | 62% | 0.732 | 106 | 365 | 0.2902 | Α | - | 0.86 | |
| LF-2-3-WL 3-5 | 0.63 | 14.08 | 8.08 | 77 | 57% | 8 | 5 | 62% | 0.735 | 105 | 365 | 0.289 | Α | 0.92 | (0.07) | <u>-</u> |
| | - | - | - | | | - | - | | | | | | | - | - | <u> </u> |
| | - | - | - | | | - | - | | | | | | | - | - | - |
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