

New Modular Building for
North Kitsap School District
Poulsbo, Washington

Code Compliance

Table with 2 columns: Label, Value. Rows include: Applicable Codes, Type of Construction, Description, Occupancy, Floor Area, Gross Wall Area, Occupant Load, Job Number, Energy Zone.

Project Information

Table with 2 columns: Label, Value. Rows include: Site Address, Dealer, Builder.

N.L.E.A.'s

- 1. Foundation plan review and inspection.
- 2. Air barrier test where required by the individual state.
- 3. An accessible route shall be provided to the building area as required in 2015 IBC section 1104.
- 4. Electrical connection to service.
- 5. On site electrical service grounding, electrode system and bonding.
- 6. Required arc flash labeling per NEC 110.16
- 7. Available fault current field markings per NEC 110.24.
- 8. Plumbing connection to service.
- 9. Installation of heat tape.
- 10. Water heater pressure relief valve and/or drain pan disposal terminates at building exterior.
- 11. Fire extinguisher installed near exterior door on site when required.
- 12. Fire alarm system review, testing and inspection.
- 13. Register airflow test and balancing of HVAC system to be performed by others on site when required by the state.
- 14. Ridge-venting, insulation, vapor barriers, air barriers and draftstopping at marriage line installed on site.
- 15. Mid-span floor support.
- 16. Site completion or installation of siding, roofing, exterior/interior trim, floor covering and any electrical, plumbing or mechanical crossover connections as they pertain to mod connections.
- 17. Site installed gutters & downspouts or roof drains as applicable.
- 18. Per WAC 296-150F Section 0500 Item No. 1: The installation of the interior equipment and appliances associated with the modular unit shall be completed under permit and inspection with the local building department.

Index to Drawing

Table with 2 columns: Label, Value. Rows include: T-1 Title Sheet, A-0.1 Door & Window Schedule, A-1 Floor Plan, A-2 Section, Material List & Fastening Schedule, A-3 Exterior Elevations, A-3.1 Interior Elevations, A-4 Details, A-4.1 Details, A-5 Reflected Ceiling Plan, Details, M-1 Mechanical Plan, M-2 Mechanical Schedules, P-1 Plumbing Schematics and Information, E-1 Electrical Power and Data, E-2 Electrical Lighting Plan, E-3 Electrical Schedules, S-1 Foundation Plan, S-2 Foundation Details.

General Notes

- The Structural Design Details Herein are Specific to the Building Size and Module Configuration Shown on the Floor Plan of These Drawings.
- No Authorization is Given or Implied for use of the Modules in the Initial or Subsequent Installation Which Results in a Building Size or Installed Module Configuration Different Than Shown on These Drawings.
- This Building will be sited a minimum of 10 feet from all Property Lines and 10 feet from any assumed Property Lines between existing structures on this site.
- Site contractor bears responsibility for providing handicap accessibility to this structure in conformance with appropriate codes.

Design Loads

Table with 2 columns: Label, Value. Rows include: Roof, Wind, Floor, Seismic, Risk Category II.

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Subject to Field Inspection

Hilder Pearson Elementary School



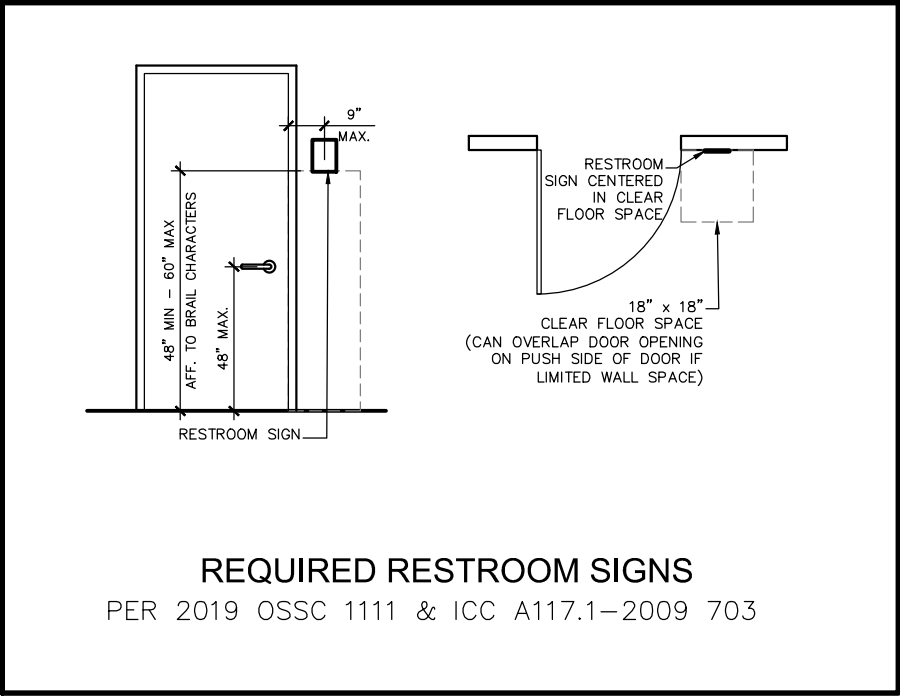
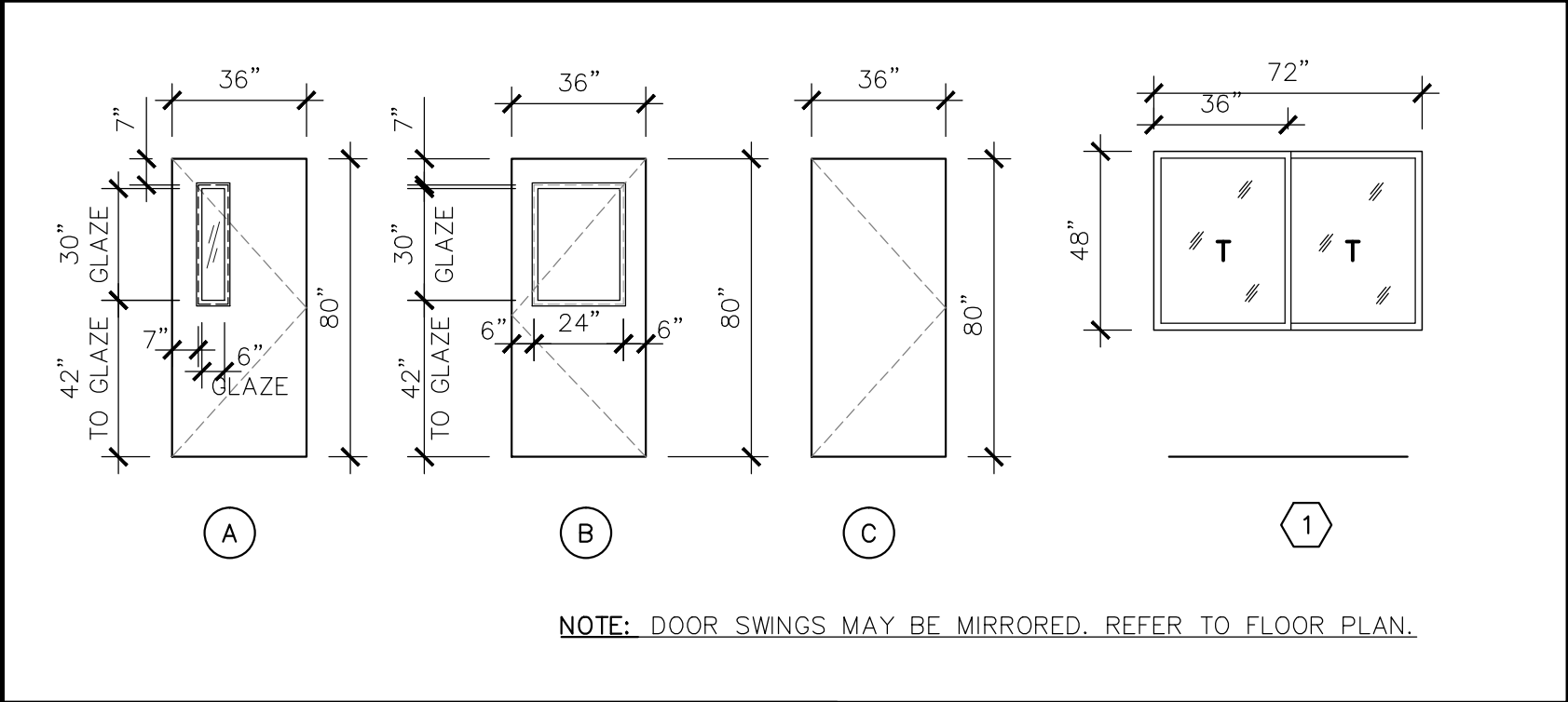
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	STYLE	QTY.	SIZE	DESCRIPTION	LOCK	REMARKS
DOORS	① A	2	3 ⁰ 6 ⁸	INSULATED GALV. STEEL w/ WELDED STEEL JAMB AND WEATHERSTRIPPING DEFAULT .37 U-FACTOR	CYLINDER	S.S. BBR'G NRP HINGES TEXTURED PAINT FINISH CLOSER PANIC DEVICE 8" x 32" LITE
	② B	2	3 ⁰ 6 ⁸	INSULATED GALV. STEEL w/ WELDED STEEL JAMB AND WEATHERSTRIPPING DEFAULT .37 U-FACTOR	CYLINDER	S.S. BBR'G NRP HINGES TEXTURED PAINT FINISH CLOSER PANIC DEVICE 24" x 30" LITE
	③ C	2	3 ⁰ 6 ⁸	SOLIDCORE VINYLWRAP w/ TIMELY FRAME	PRIVACY LEVER	STANDARD HINGES VW OAK FINISH

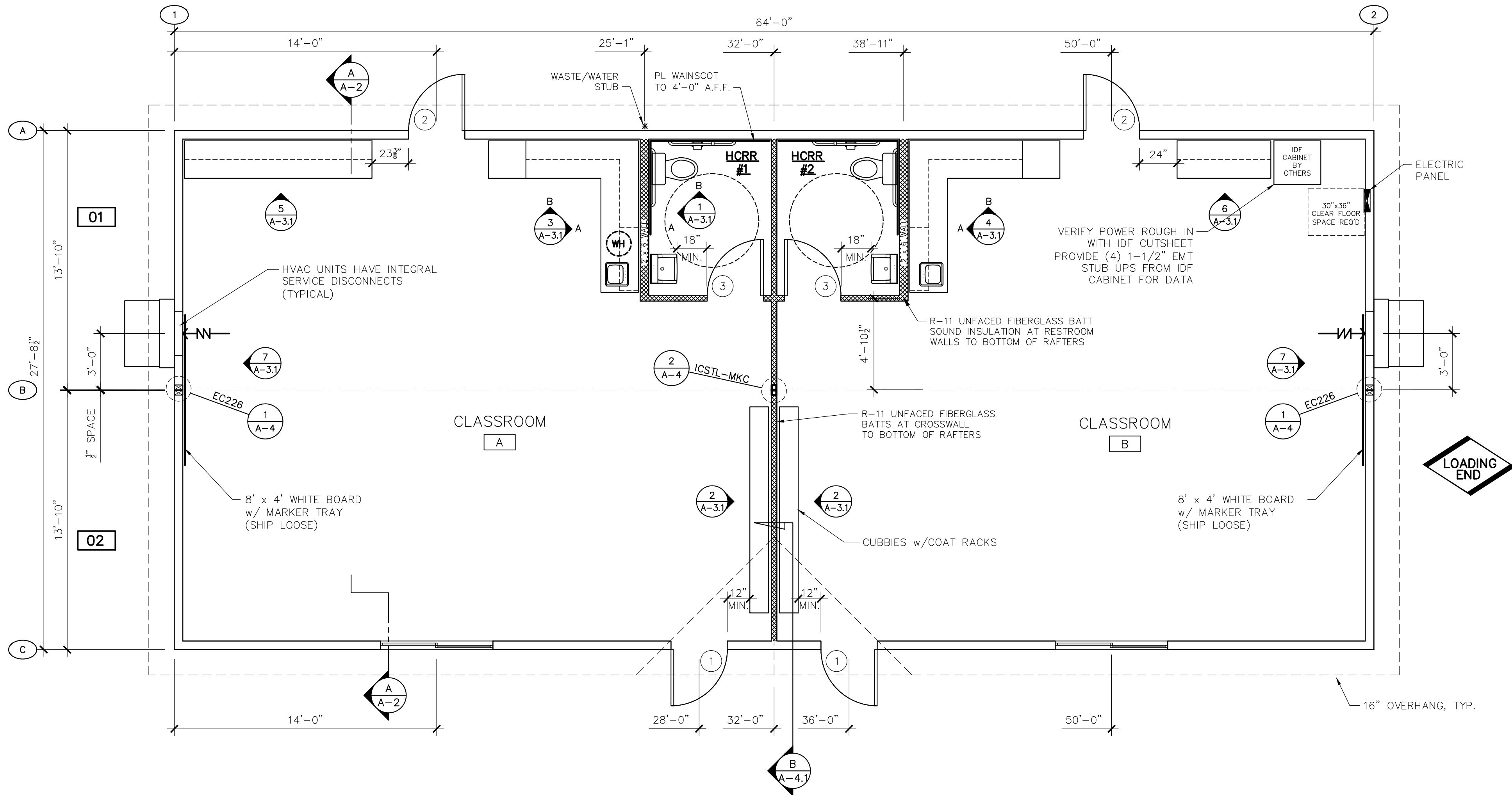
NOTE: DOOR HARDWARE SHALL BE COMPLIANT WITH ICC A117.1-2009 SECTION 404.2.6

WINDOWS	①	2	72 x 48	PRIME-- HORIZONTAL SLIDER - DUAL GLAZE - LOW "E" WHITE VINYL FINISH-ARGON-TEMPERED-MINI BLINDS NFRC 0.29 U-FACTOR, SHGC = 0.39, V.T.=0.56
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NOTES:
-GALVANIZED FLASHING INSTALLED UNDER EXTERIOR TRIM ABOVE WINDOWS
-INSTALL SELF-ADHESIVE FLASHING OVER EXTERIOR FLANGES PER
RECOMMENDED INSTALLATION PATTERN



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					WA GOLD		Drawn By: AJB	
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FLOOR PLAN

SCALE: 1/4" = 1'-0"

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NOTES:
-THE TOP PLATES OF THE INTERIOR WALLS CAN SPAN
A MAXIMUM OF 10'-0" BEFORE REQUIRING BRACING
TO THE ROOF STRUCTURE OR AN INTERSECTING WALL.



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FASTENING SCHEDULE

MATERIAL LIST

WALLS:	
PLATE-TO-STUD	MIN. OF 2- 0.121 x 3" NAILS
SHEETROCK-TO-STUD @ INTERIOR	0.091 x 1 ¹ / ₈ " SHEETROCK NAILS @ 16"oc EDGE AND CONSTRUCTION ADHESIVE IN FIELD
VW TACKBOARD-TO-STUD @ INTERIOR	16 ga. x 2" WIDECROWN STAPLES (SENCO P21) @ 6"oc TOP & BOTTOM AND GLUE IN FIELD
BOTTOM PLATE-TO-FLOOR	0.131 x 3" NAILS @ 8"oc (SENCO KC27 OR EQUAL)
EXT. GYPSUM SHEATING-TO-STUD @ EXTERIOR	6d COATED NAILS @ 7"oc EDGE AND 7"oc FIELD
7 ¹ / ₈ " SHEATHING-TO-STUD AT SIDEWALL	0.113x2 ³ / ₈ " NAILS @ 6"oc EDGE, 12"oc FIELD. ALL EDGES SUPPORTED BY FRAMING OR BLOCKING
7 ¹ / ₈ " SHEATHING-TO-STUD AT ENDWALL	SEE ENDWALL FASTENING NOTES ON ELEVATIONS
LAP SIDING-TO-STUD	PER MANUFACTURER'S RECOMMENDATION
THREE STUD CORNER CONNECTION	0.131 x 3" NAILS @ 12"oc (SENCO KC27 OR EQUAL)

AIR BARRIER NOTES:	
THESE KEY AREAS SHALL BE SEALED BY CAULKING, GASKETS, TAPE OR WEATHER-STRIPPING:	
-JOINTS AROUND FENESTRATION (WINDOWS AND DOOR FRAMES): USE APPROPRIATELY SIZED BACKER ROD WITH MINIMUM 2" LAP AT ENDS.	
-JUNCTIONS BETWEEN WALLS AT:	
-BUILDING CORNERS: USE CAULKING	
-STRUCTURAL FLOORS: USE SILL SEAL OR CAULKING	
-ROOFS (AT RIM): USE SILL SEAL OR CAULKING	
-PENETRATIONS OF UTILITY SERVICES THRU THE AIR BARRIER @ ROOFS, WALLS, AND FLOORS: USE CAULKING, SPRAY FOAM, OR AIR BARRIER TAPE.	
-BUILDING ASSEMBLIES USED AS DUCTS OR PLENUMS: USE BACKER ROD, CAULK, SPRAY FOAM OR AIR BARRIER TAPE.	
-JOINTS, SEAMS, AND PENETRATIONS OF VAPOR RETARDANTS: USE CAULK OR APPROVED TAPE.	
-RECESSED LIGHTING FIXTURES: USE CAULK OR SPRAY FOAM	

FLOOR:	
2 x 8 FLOOR JOIST-TO-RIM	MIN. OF 4- 0.131" x 3" NAILS (SENCO KC27 OR EQUAL)
CLASS "A" BOTTOM BOARD-TO-JOIST	16 GA. x 3/8" WIDE CROWN @ 12" MAX. EDGES ONLY
FLOOR DECKING-TO-2x JOIST	.113" x 2 3/8" RING SHANK @ 6"oc EDGE, 12"oc FIELD (SENCO GE-24). USE CONSTRUCTION ADHESIVE (AFG01) ON JOISTS
ROOF:	
FURRING-TO-RAFTERS	MIN. OF 4- M20 2" x 3" (MIN.) RATED EACH SIDE
RIM-TO-RAFTERS	MIN. OF 3- 0.131 x 3" NAILS (SENCO KC27 OR EQUAL)
ROOF RIM-TO-TOP PLATE	0.131" x 3" NAILS @ 8"oc (SENCO KC27 OR EQUAL)
LEDGER-TO-RIDGEBEAM	0.131" x 3" NAILS @ 3" oc & 3 @ BUTT JOINTS (SENCO KC27 OR EQUAL)
RAFTER-TO-RIDGEBEAM	4- 0.131" x 3" NAILS (SENCO KC27 OR EQUAL)
SHEATHING-TO-ROOF MEMBERS	16 GA. x 1 3/4" STAPLES @ 6"oc EDGE, 12"oc FIELD, AND 4"oc AT VENTED EAVES

NOTE: SHEATHING TO BE INSTALLED PERPENDICULAR TO THE RAFTERS. OFFSET SHEATHING 4 ft. BLOCK EDGES OF ANY PIECES LESS THAN 24"

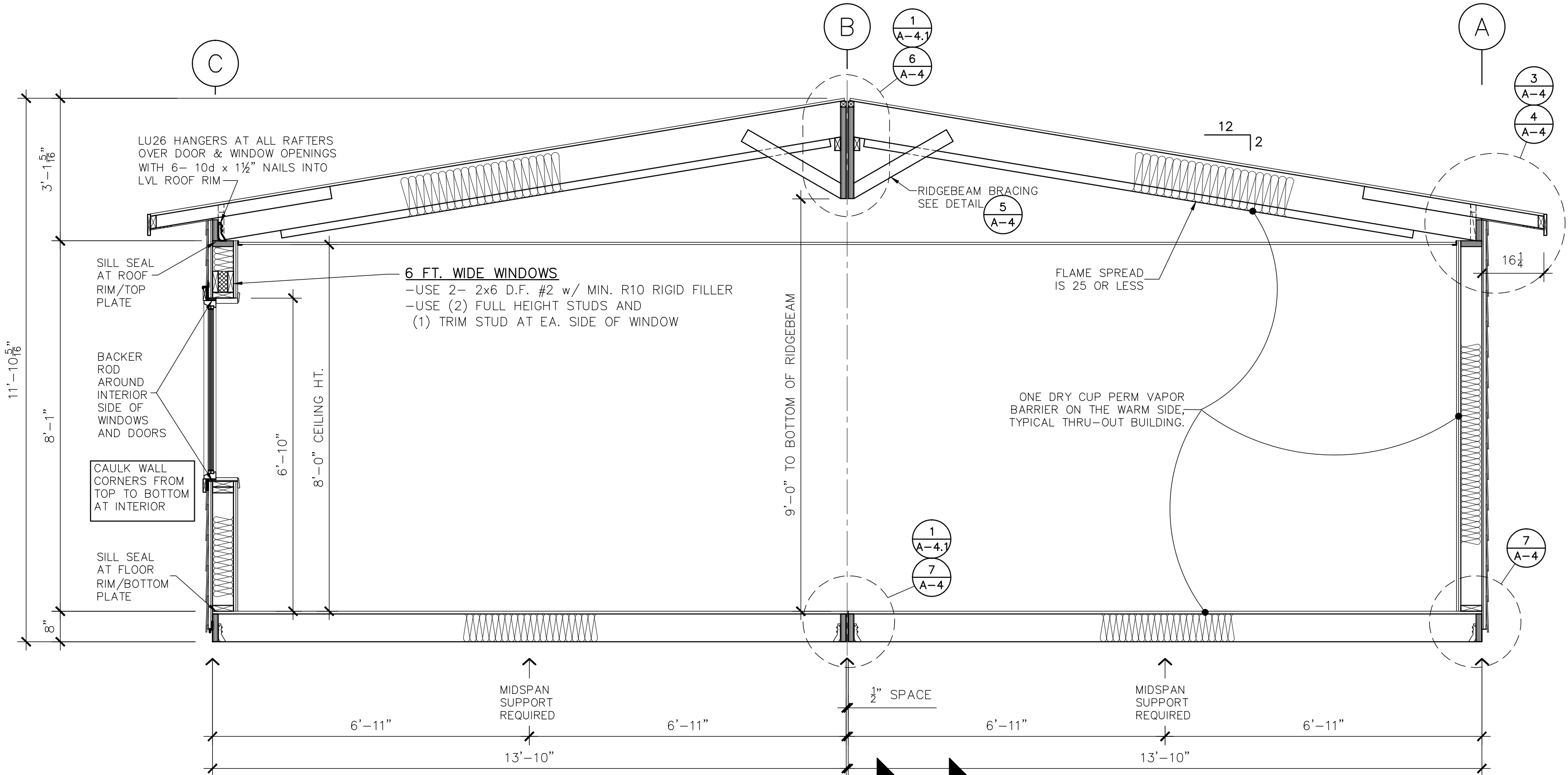
MODLINE CONNECTION:	NOTE: ALL MODLINES (DEFINED AS THE SPACE BETWEEN ADJOINING MODULES) MUST BE INSULATED AT THE ROOF, FLOOR <u>AND</u> WALLS <u>ON SITE</u> .
RIDGEBEAMS	1/2" BOLTS w/ 1 1/2" DIA. WASHERS @ 6'-0"oc AND 8" FROM EACH END (MINIMUM 2" EDGE DISTANCE)
RIM JOISTS	1/2" BOLTS w/ 1 1/2" DIA. WASHERS @ 4'-0"oc AND 8" FROM EACH END (MINIMUM 2" EDGE DISTANCE)

ROOF:	
ROOFING.....	.24 GA. STANDING SEAM METAL 18" WIDE PANELS OVER "HIGH TEMP" SELF ADHERED ROOFING UNDERLAYMENT
SHEATHING.....	1 ⁵ / ₈ " APA RATED (32/16)(¹ / ₂ " PLYWOOD)
FRAMING.....	.2 x 10 DF #2 RAFTERS @ 24"oc w/ 2" FURRING ON BOTTOM FOR R-38
RIDGEBEAM.....	.1 1/2" x 24" CONT. LVL 2.0E
LEDGERS.....	.2 x 4 D.F. TAPER CUT
RIMS.....	.2 x 6 CONTINUOUS LVL 2.0E WITH 2 x 10 DF VENT BLOCKS
INSULATION.....	R-38 CELLULOSE BLOW-IN OVER CLASS 'A' MATERIAL (AIR BARRIER COMPONENT) NOTE: MIN. 1" AIR SPACE REQUIRED AT ROOF SHEATHING. USE BAFFLES IF REQUIRED FOR VENT CLEARANCE
CEILING.....	SUSPENDED T-BAR (PER IBC 808.1)
ARCHITECTURAL....	.16" OVERHANG
SOFFIT.....	1/4" FIBER CEMENT PANEL, PERFORATED FOR VENTING
VENTING.....	SOFFIT AND RIDGE
WALLS:	
SIDING.....	FIBER CEMENT LAP SIDING w/ 8" EXPOSURE. WRAP LOWER 12" OF BUILDING WITH MOIST-STOP. WRAP BUILDING WITH BUILDING WRAP
SHEATHING.....	7 ¹ / ₈ " APA RATED UNDER 5/8" EXTERIOR GYPSUM WITH TREATED CORE
FASCIA.....	1 x 6
TRIM.....	5/4 x 4 AT CORNERS, WINDOWS AND DOORS

NOTE: 2"x 2" GALV. FLASHING UNDER CORNER TRIM
5/4 x 6 AT MODLINES (SHIP LOOSE)

FRAMING.....	EXT: 2 x 6 D.F. #3 or BETTER STUDS @ 16"oc INT: 2 x 4 H.F. @ 16"oc PLUMBING WALLS TO BE 2 x 6 H.F. NOTE: CROSSWALL AND RESTROOM WALLS FRAMED FULL HEIGHT TO BOTTOM OF RAFTERS
TOP PLATE.....	.2 x 6 CONTINUOUS (DF#2 OR LVL 2.0E)
BOTTOM PLATE.....	.2 x 6 D.F.
INSULATION.....	EXT: R-21 FIBERGLASS BATTS INT: R-11 UNFACED FIBERGLASS INSULATION BATTS AT CROSSWALL AND RESTROOM WALLS TO BOTTOM OF RAFTERS
INTERIOR FINISH.....	1/2" VINYLWRAP TACKBOARD OVER 5/8" TYPE 'X' SHEETROCK, AND SHEETROCK ABOVE WALL FINISH AT GABLE ENDS (AIR BARRIER COMPONENT). PLASTIC LAMINATE PER CODE IN RESTROOMS

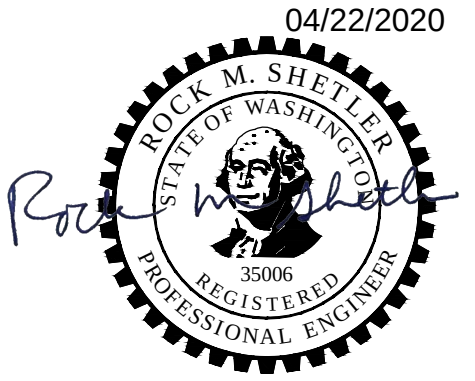
FLOOR:	
COVERING.....	RESTROOMS: SHEET VINYL ALL ELSE: ON SITE BY OTHERS
DECKING.....	1st: 2 ³ / ₈ " APA RATED T&G - GLUED AND NAILED (AIR BARRIER COMPONENT) 2nd: 1/4" ULTRAPLY XL IN RESTROOMS
FRAMING.....	.2 x 8 DF#2 JOISTS @ 16"oc
RIMS.....	.2 x 8 CONTINUOUS LVL 2.0E
JOIST HANGERS.....	AT ALL JOISTS
INSULATION.....	R-30 (USE TWO LAYERS OF R15 FIBERGLASS)
BOTTOM COVER.....	CLASS "A"



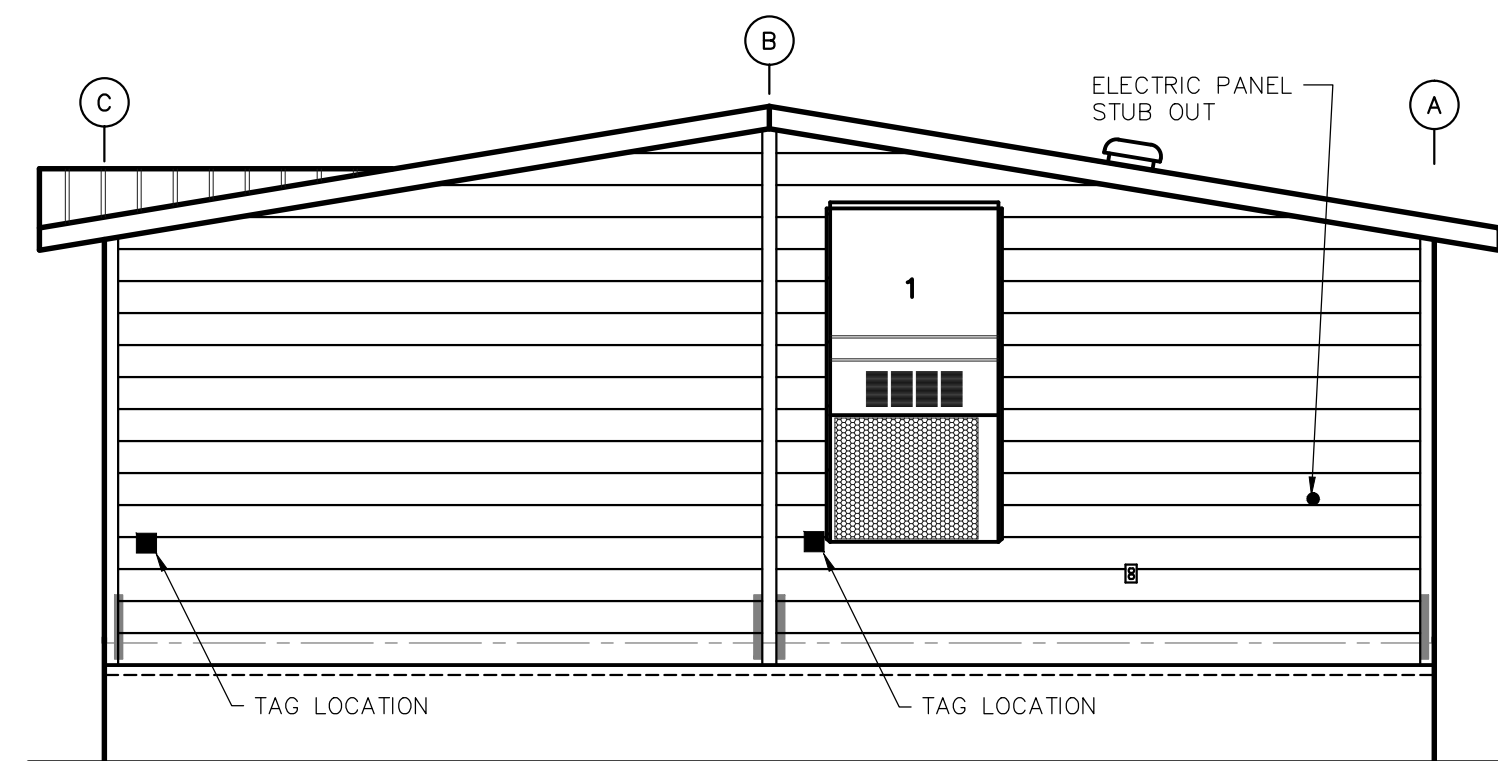
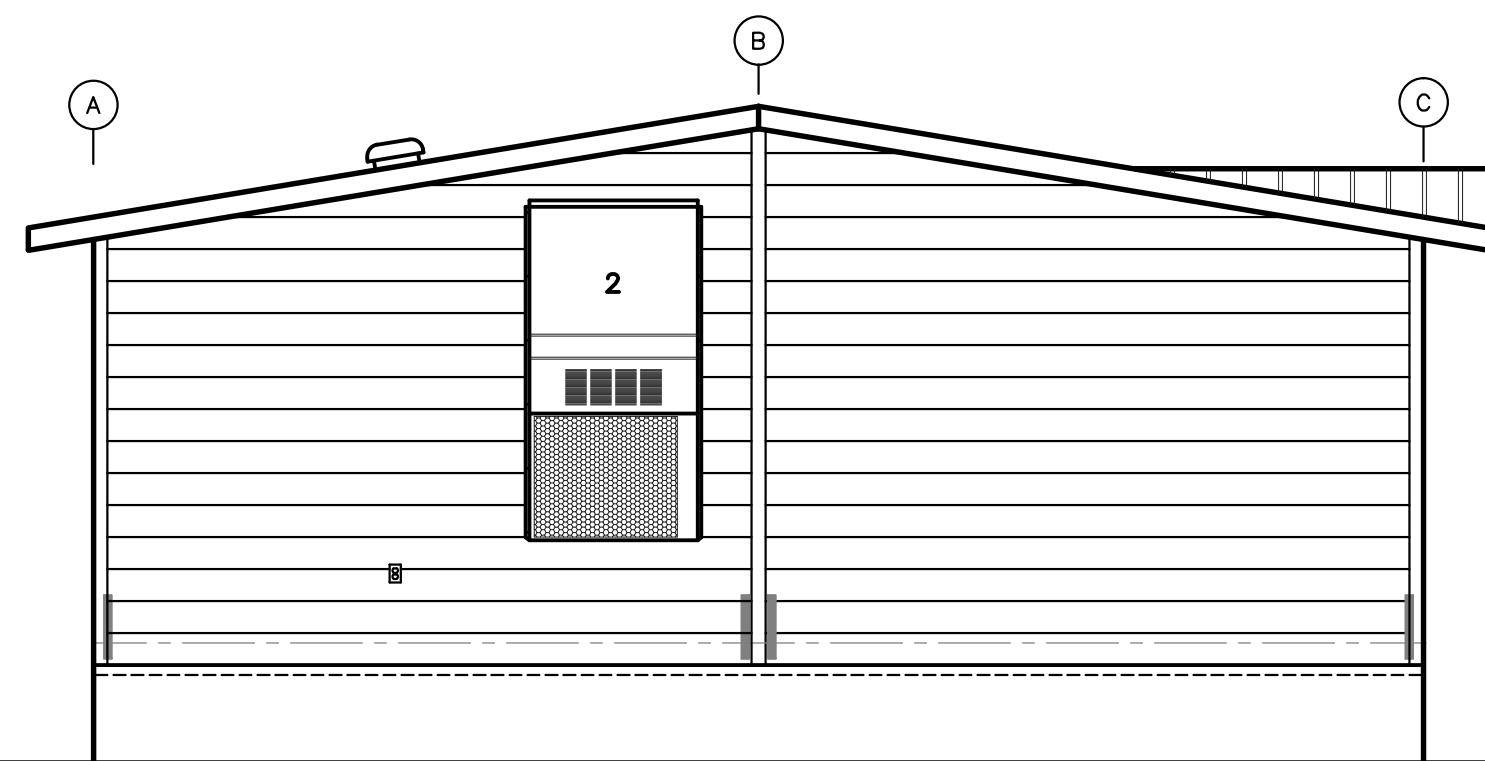
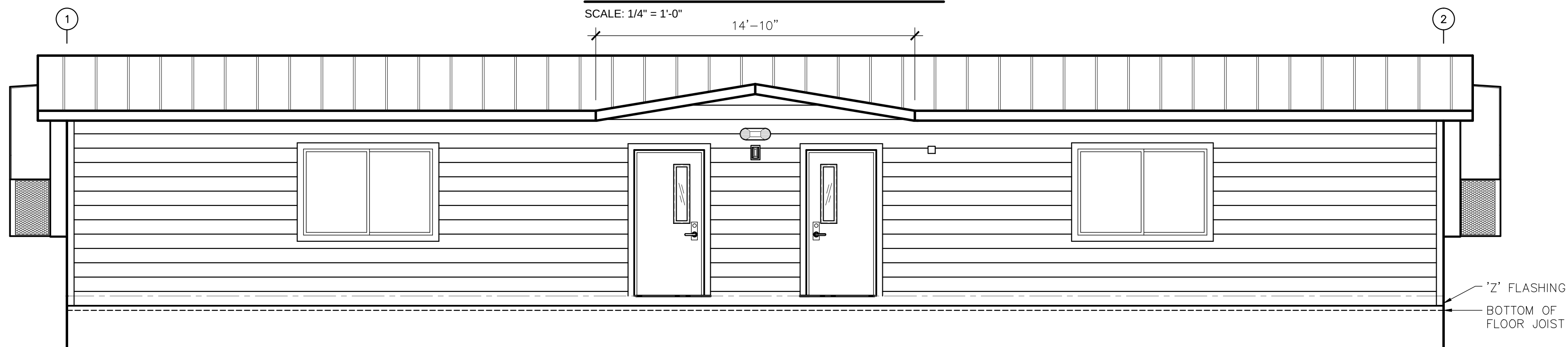
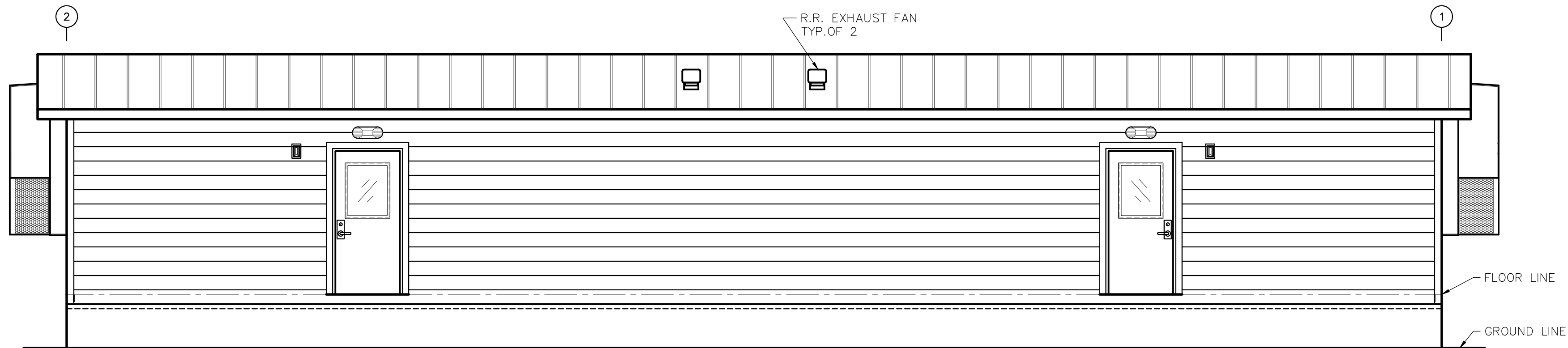
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SECTION - A-A

SCALE: 1/2" = 1'-0"



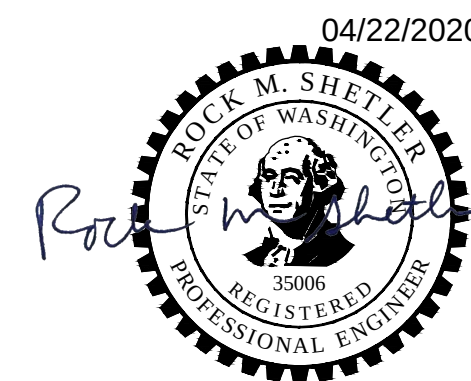
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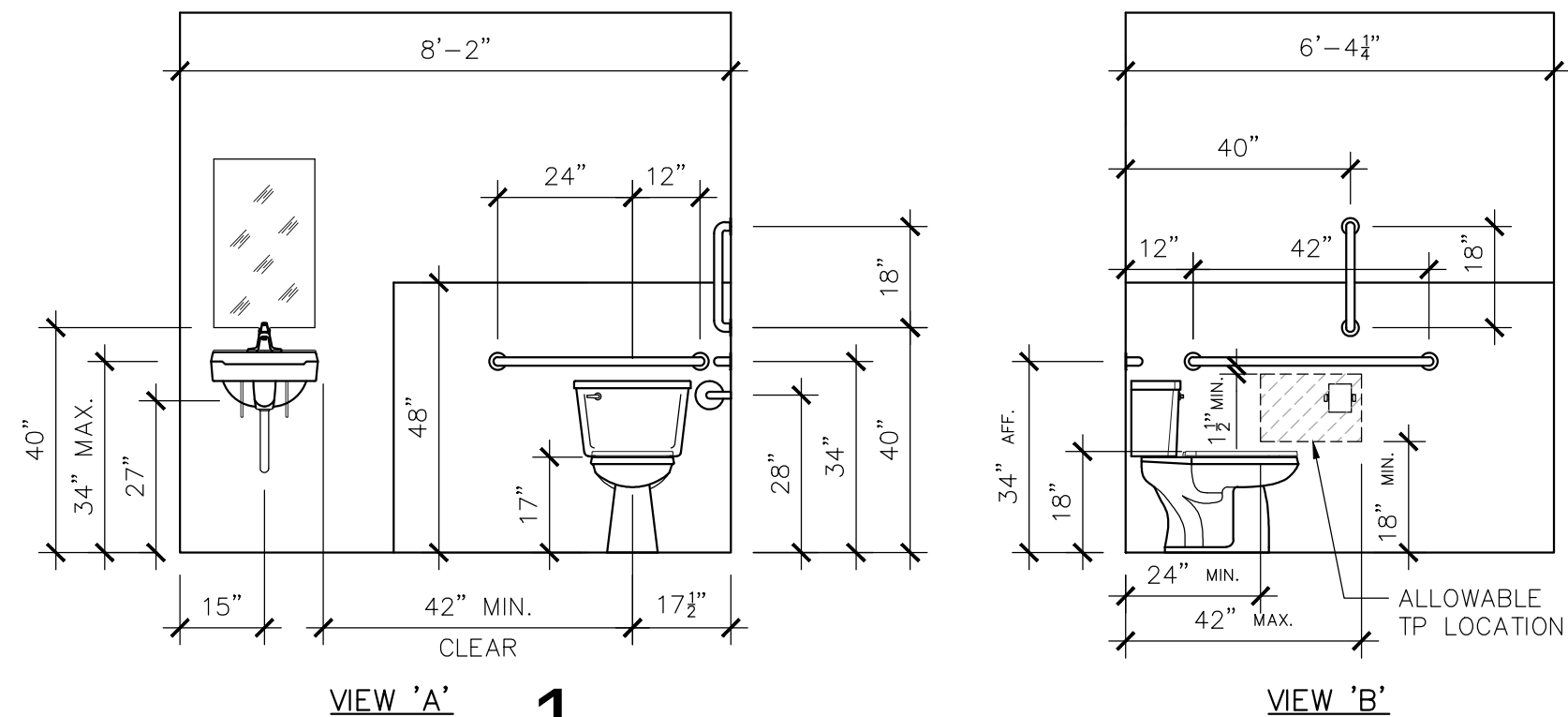
ENDWALL FASTENING:

1. INSTALL $\frac{7}{16}$ " RATED SHEATHING w/ ALL EDGES SUPPORTED. FASTEN w/ 0.113 x $2\frac{3}{8}$ " GALV. NAILS @ 6"oc EDGE, 12"oc FIELD
2. INSTALL ST2215 STRAPS WHERE SHOWN w/ 7- 10d x $1\frac{1}{2}$ " NAILS EACH END OF EACH STRAP

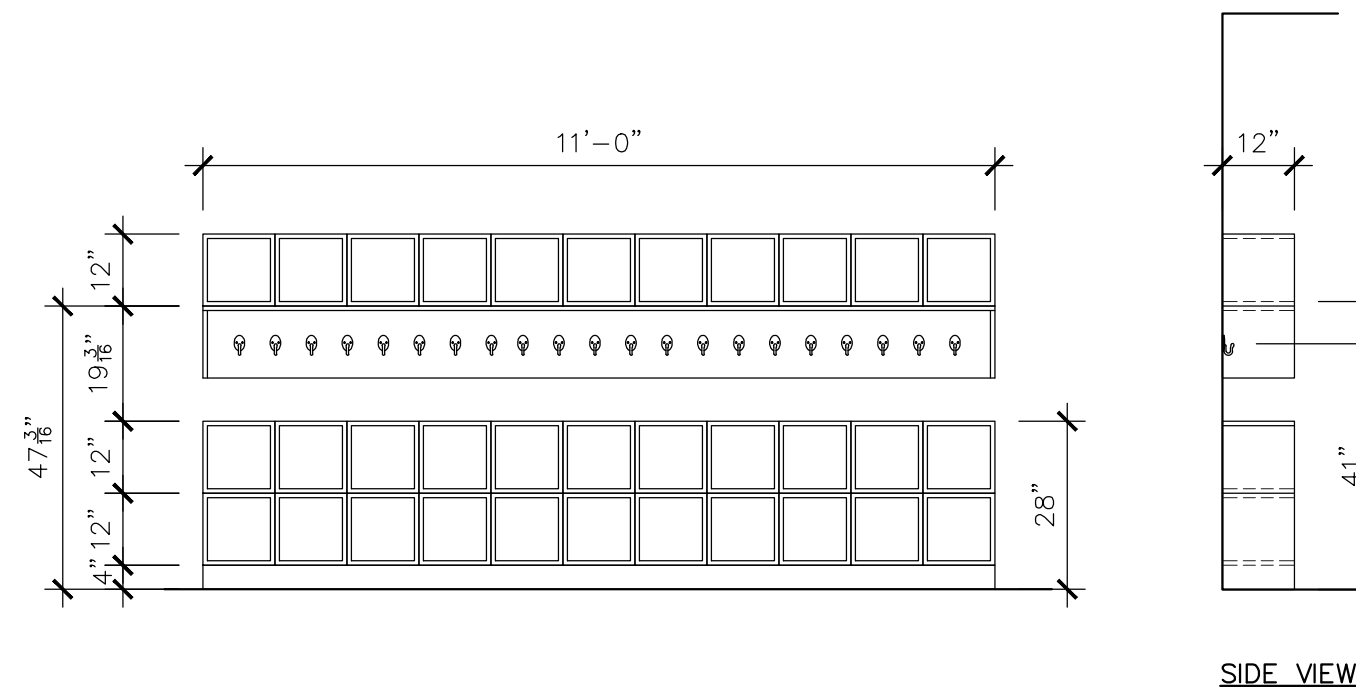
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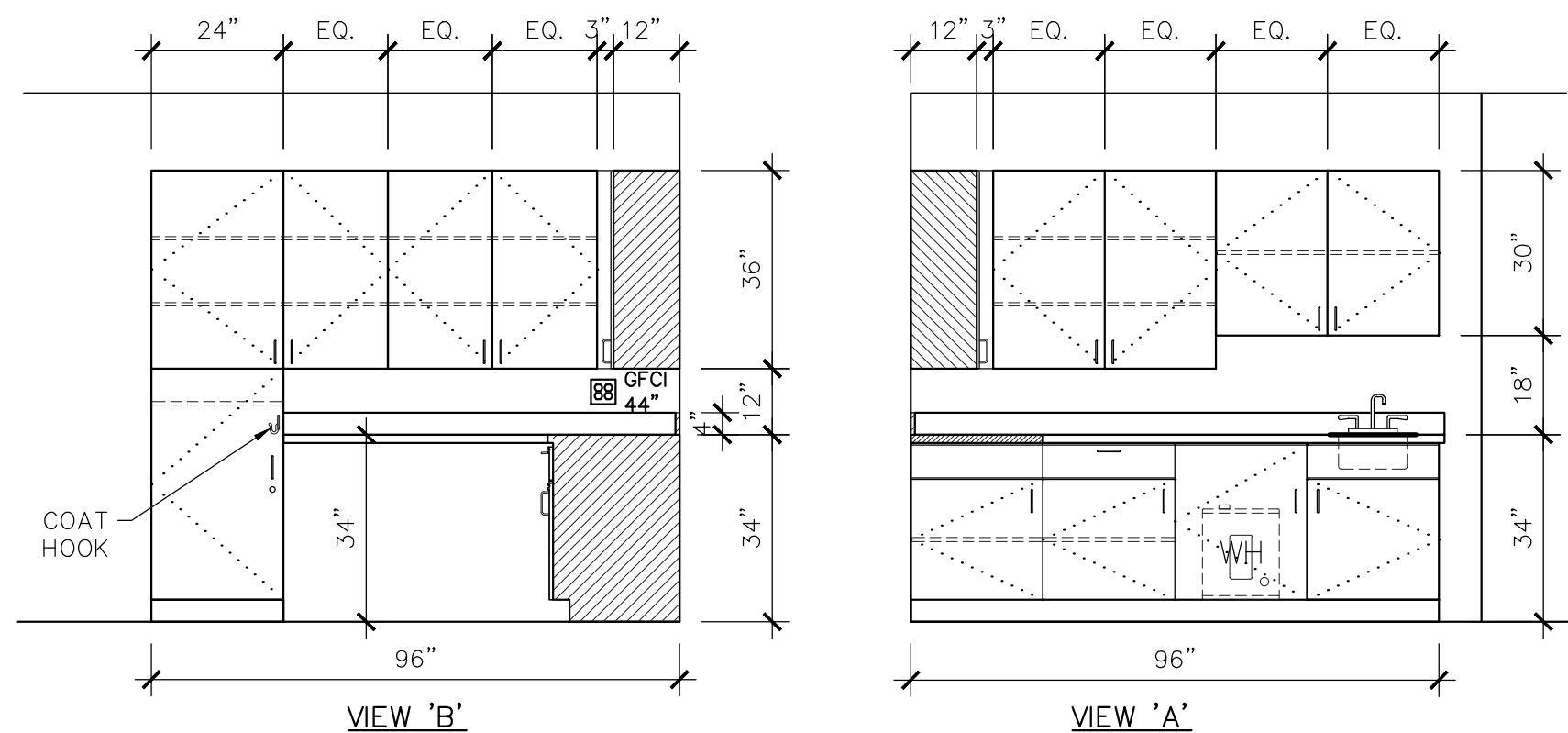


1 H.C.R.R. ELEVATIONS
3/8" = 1'-0"

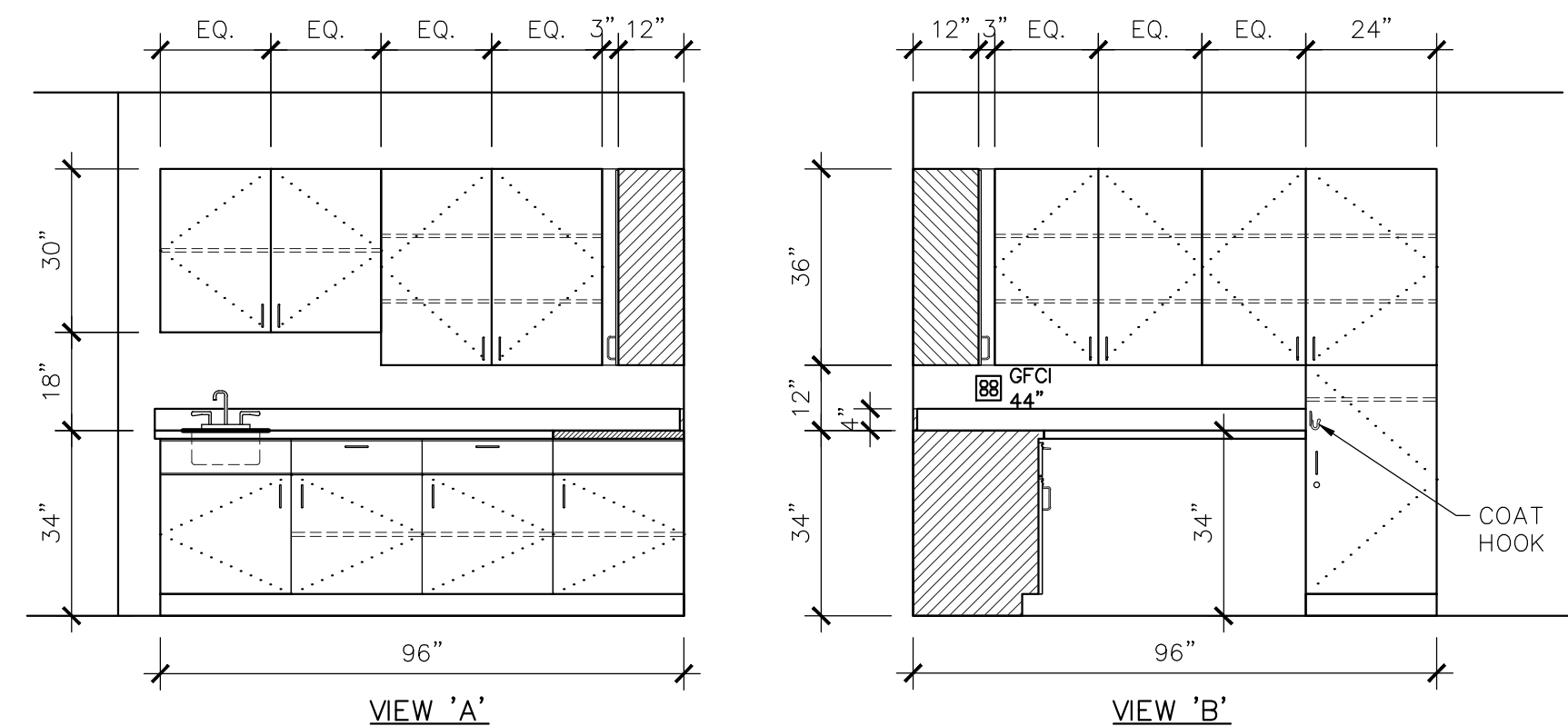


2 CUBBIES w/ COATRACK ELEVATION
3/8" = 1'-0"

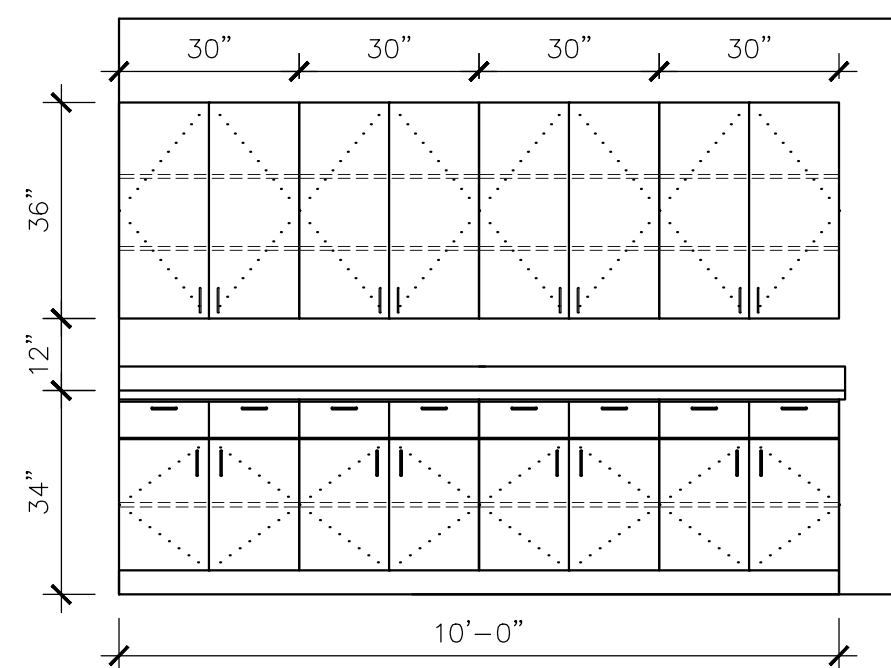
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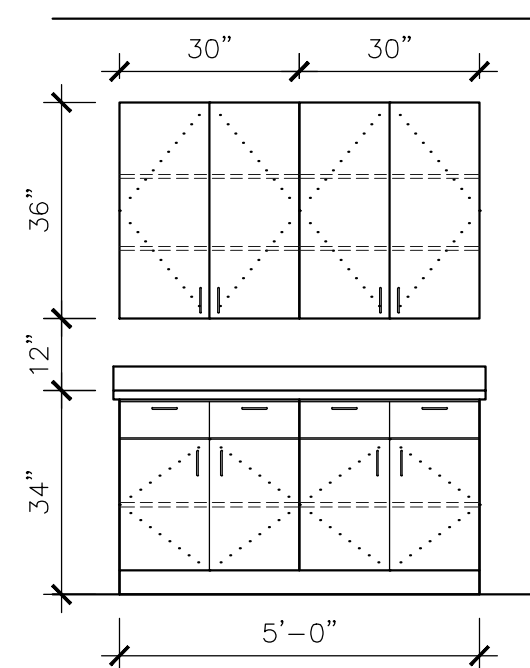
3 CABINET ELEVATIONS
3/8" = 1'-0"



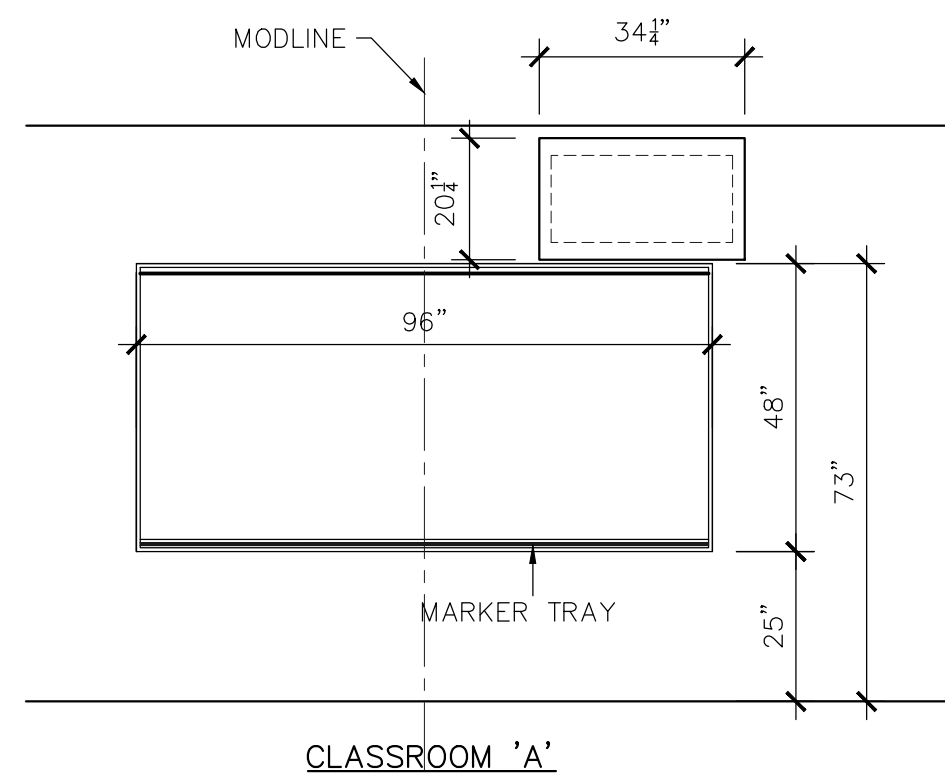
4 CABINET ELEVATIONS
3/8" = 1'-0"



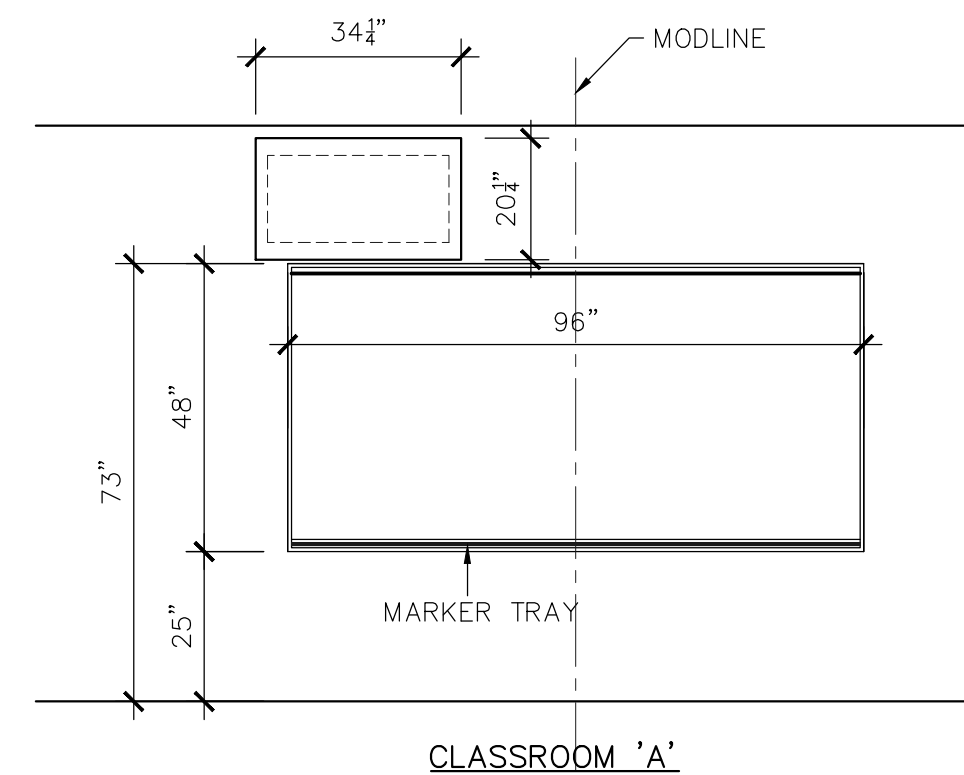
5 CABINET ELEVATION
3/8" = 1'-0"

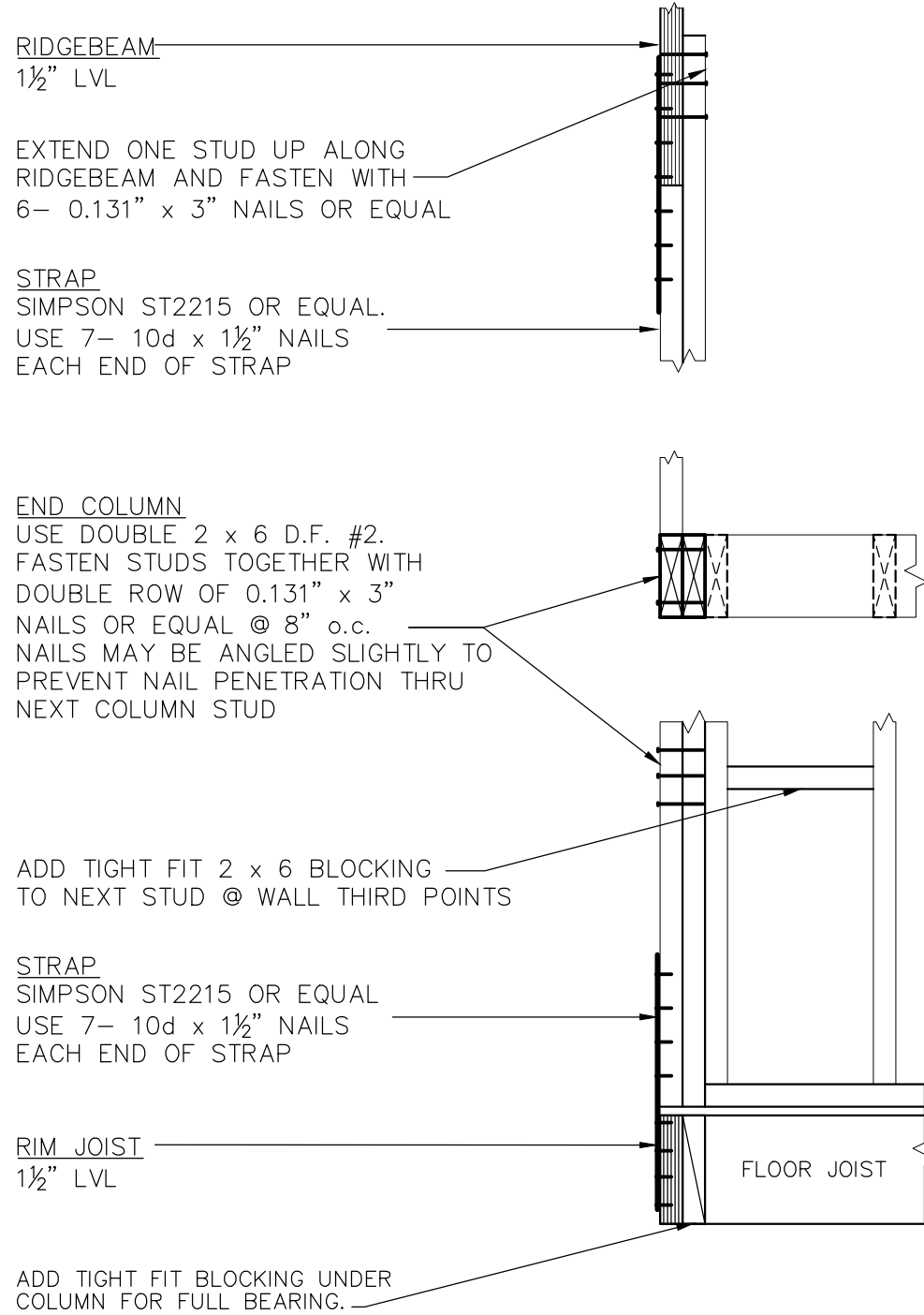


6 CABINET ELEVATION
3/8" = 1'-0"

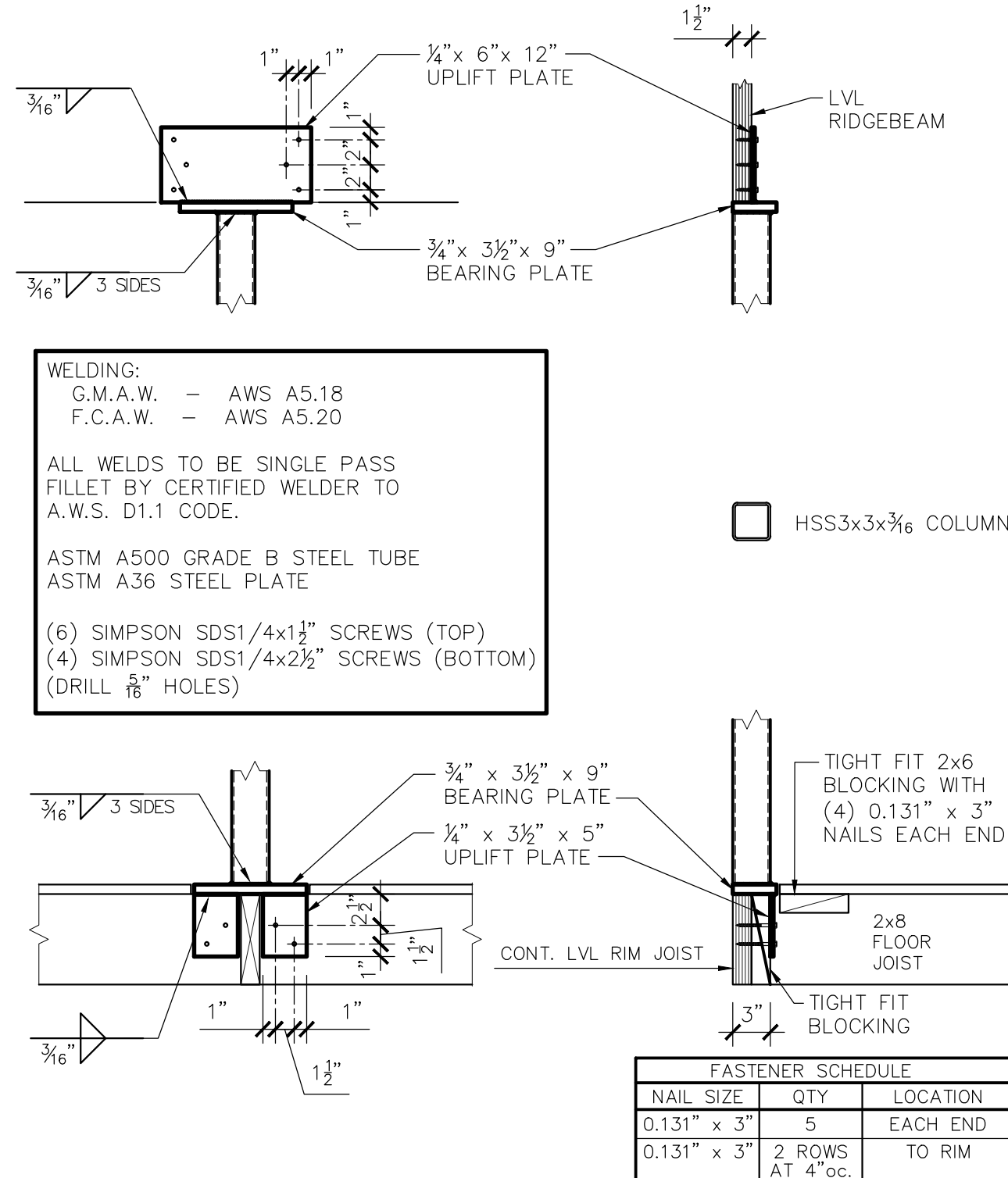


7 WHITEBOARD ELEVATIONS
3/8" = 1'-0" (SHIP LOOSE)

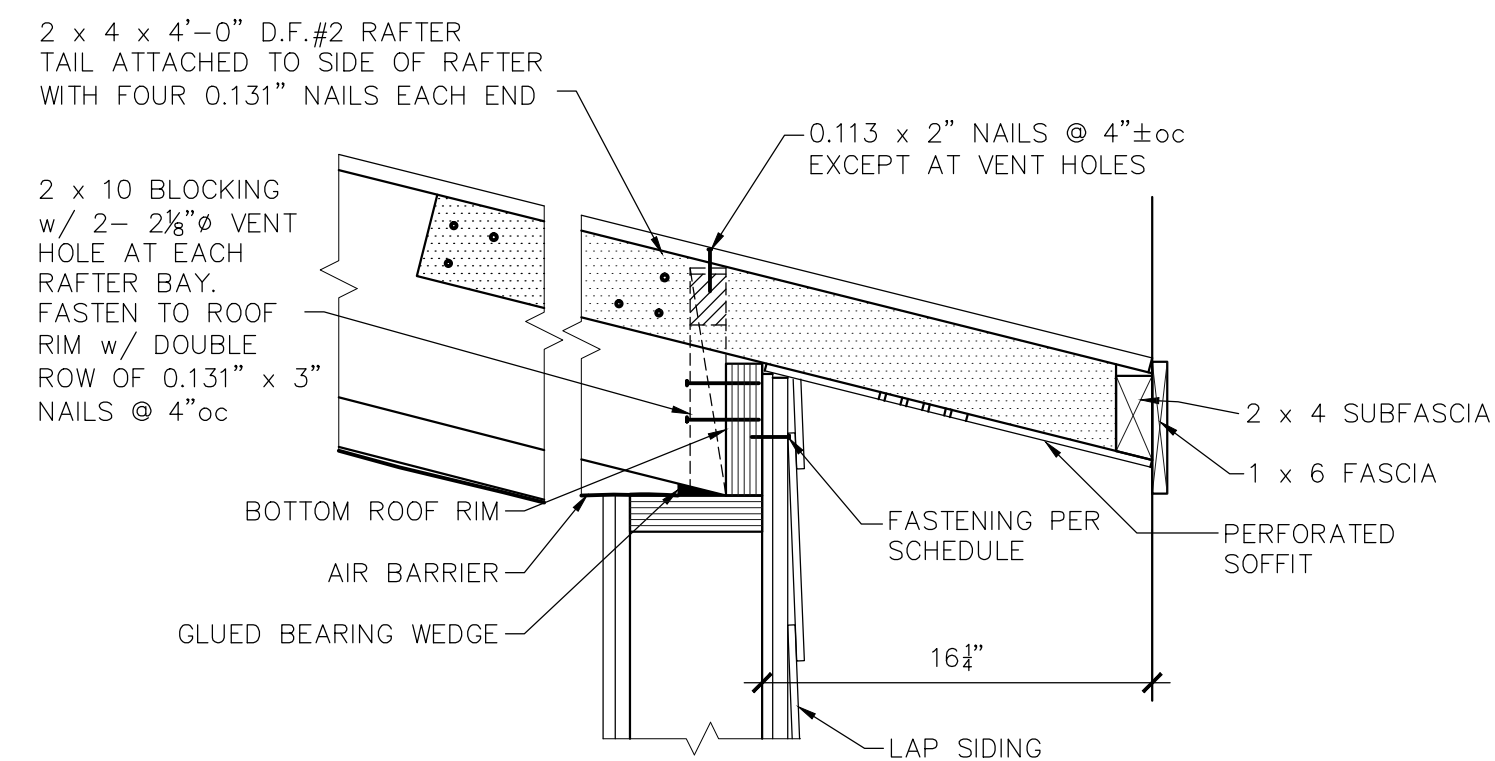




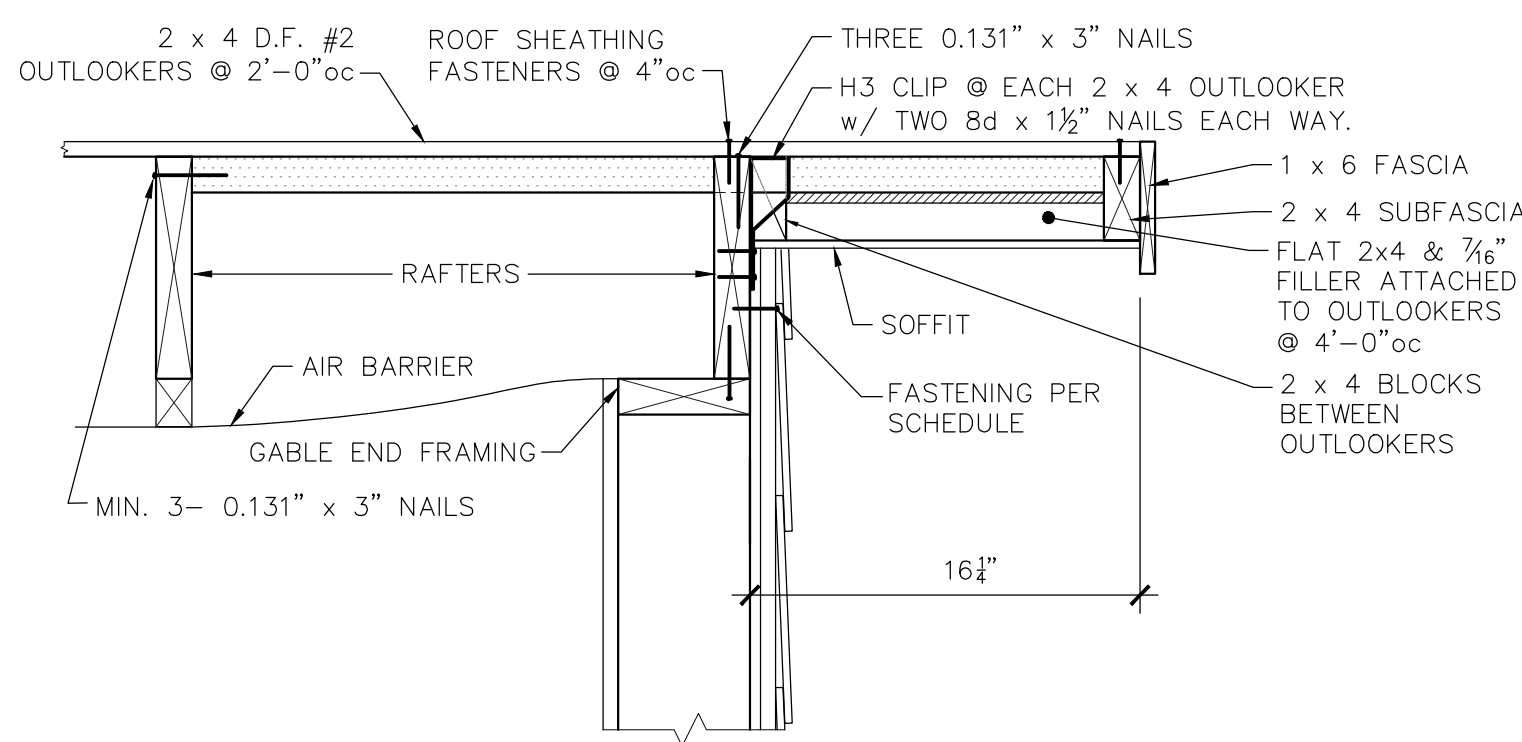
1 EC226:END COL. DETAIL - DBL 2 x 6
1" = 1'-0"



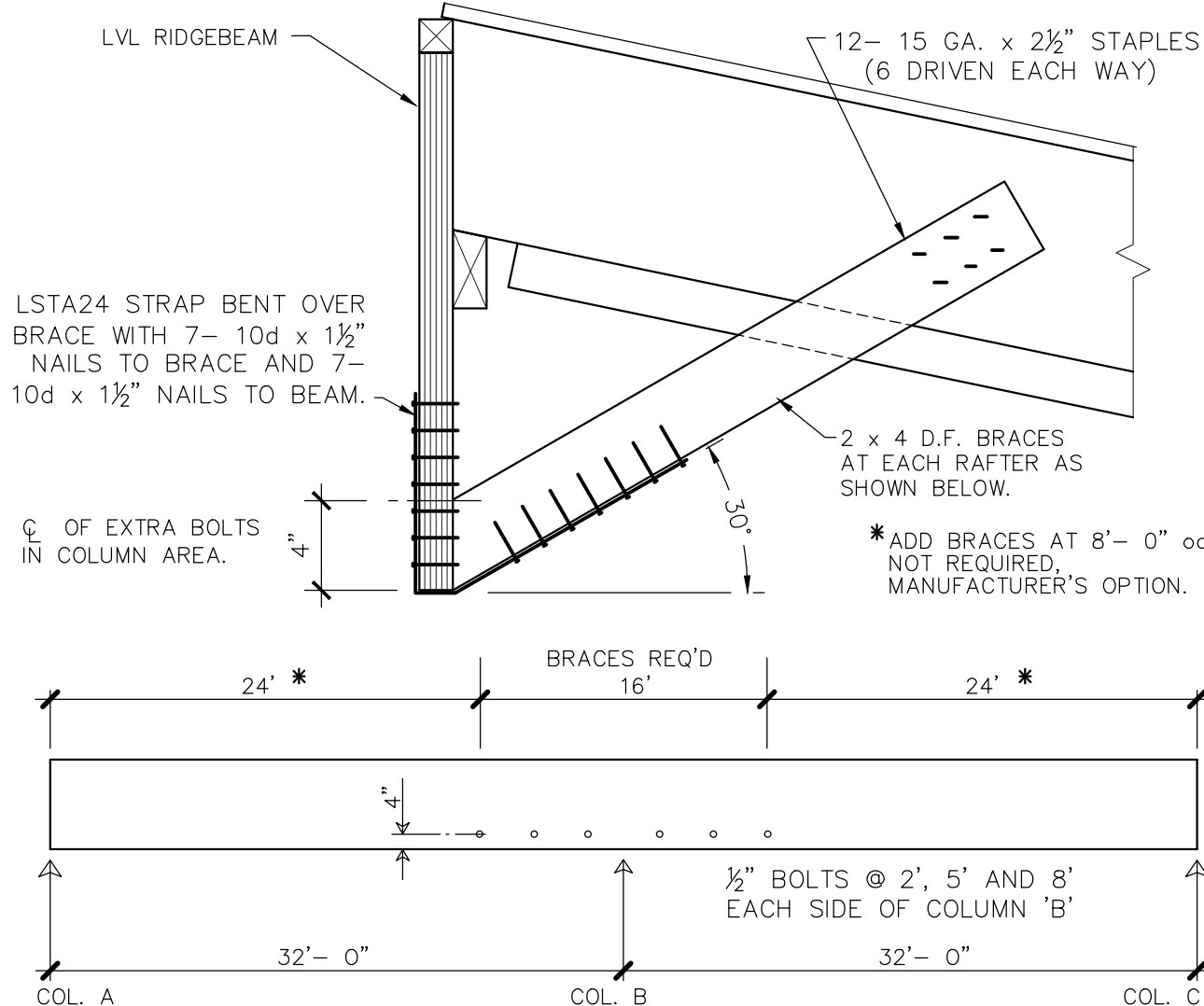
2 ICSTL-MKC: INTERIOR COLUMN DETAIL
1" = 1'-0"



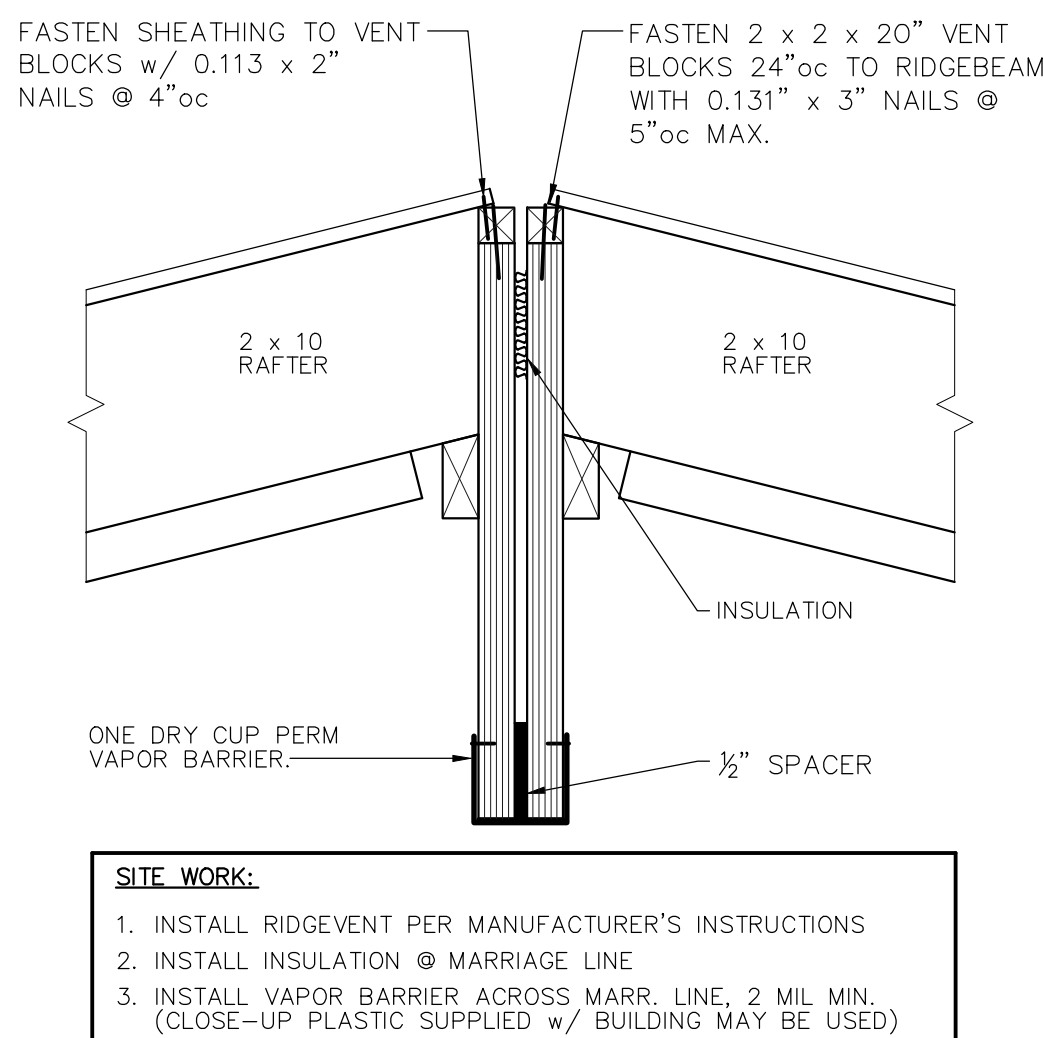
3 EAVE DETAIL
1 1/2" = 1'-0"



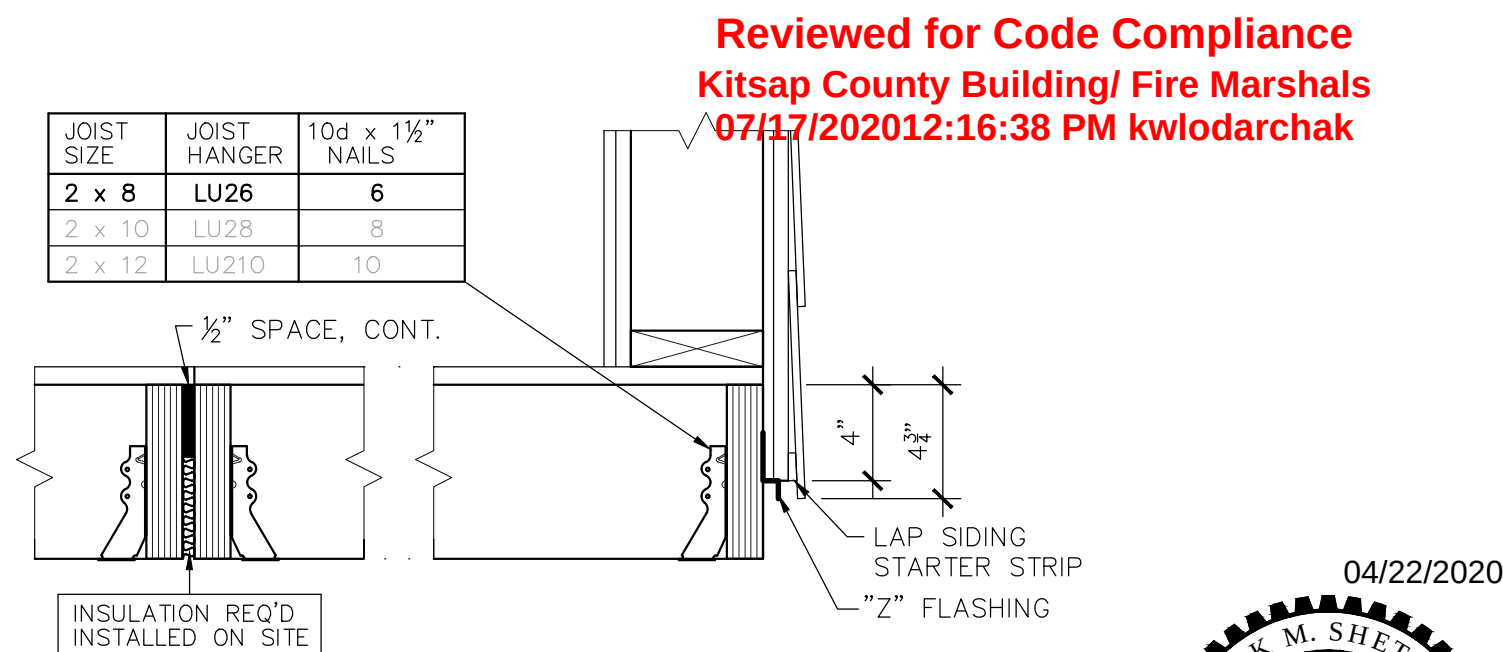
4 ENDWALL ROOF OVERHANG DETAIL
1 1/2" = 1'-0"



5 RIDGEBEAM BRACING DETAIL
1 1/2" = 1'-0"

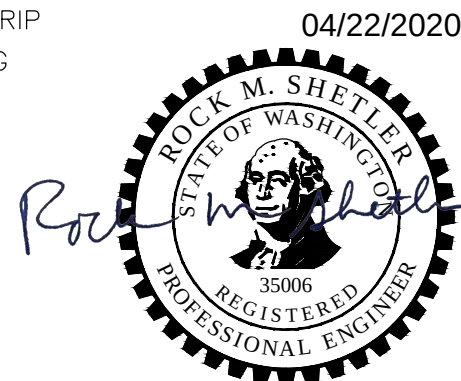


6 RIDGE DETAIL
1 1/2" = 1'-0"



7 FLOOR DETAIL
1 1/2" = 1'-0"

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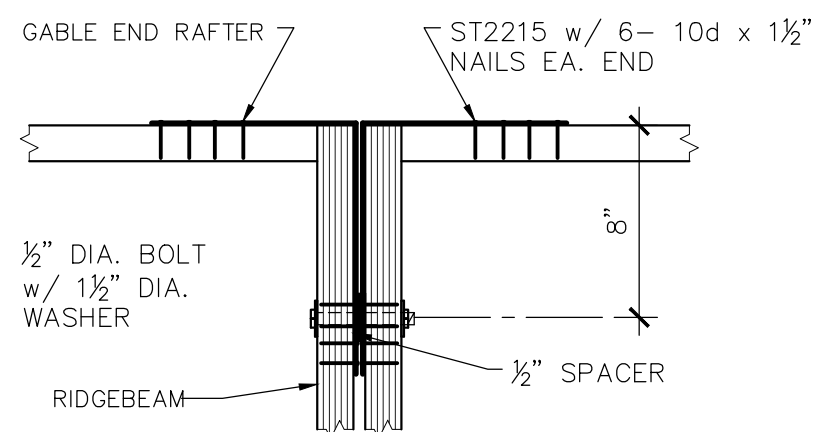
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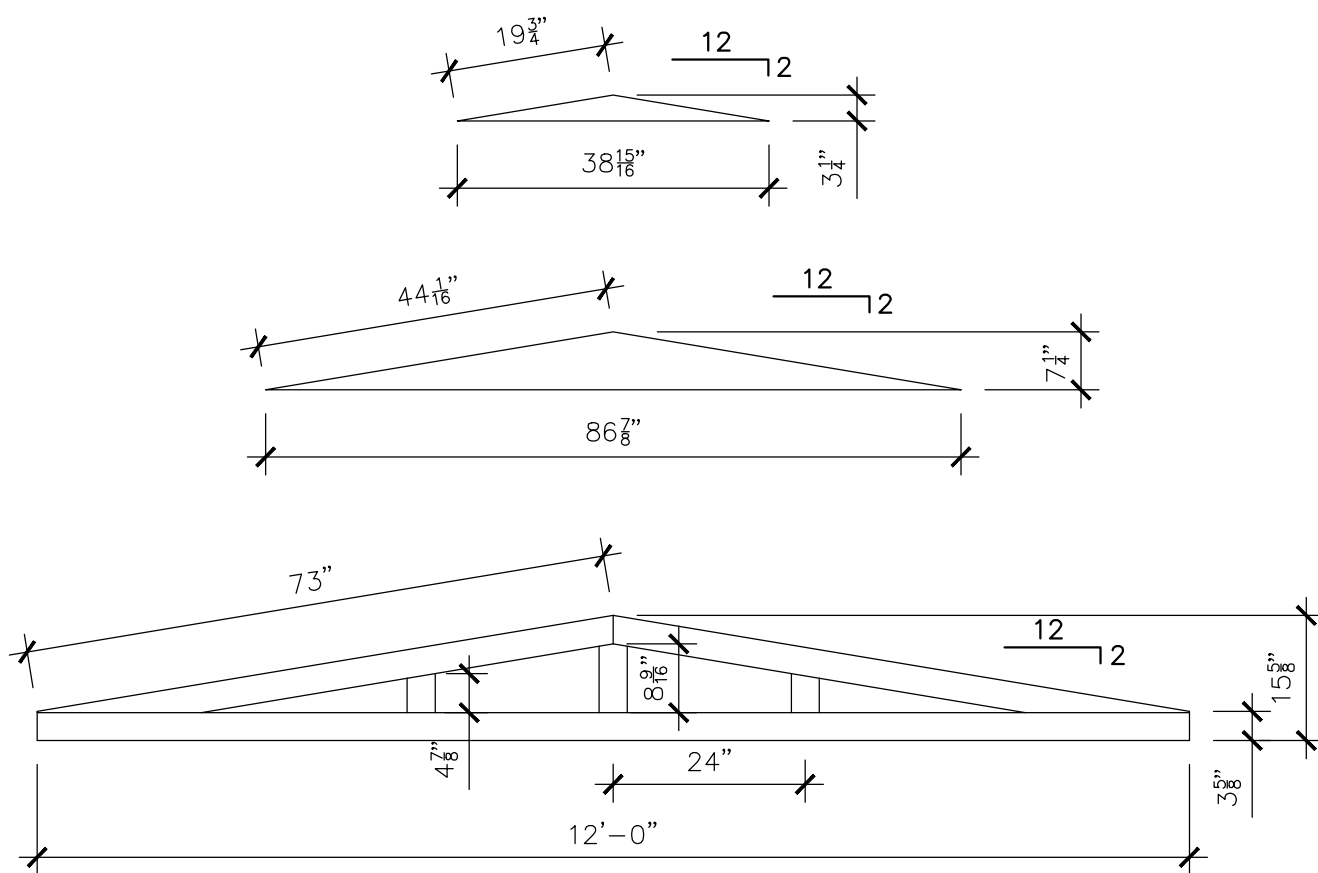
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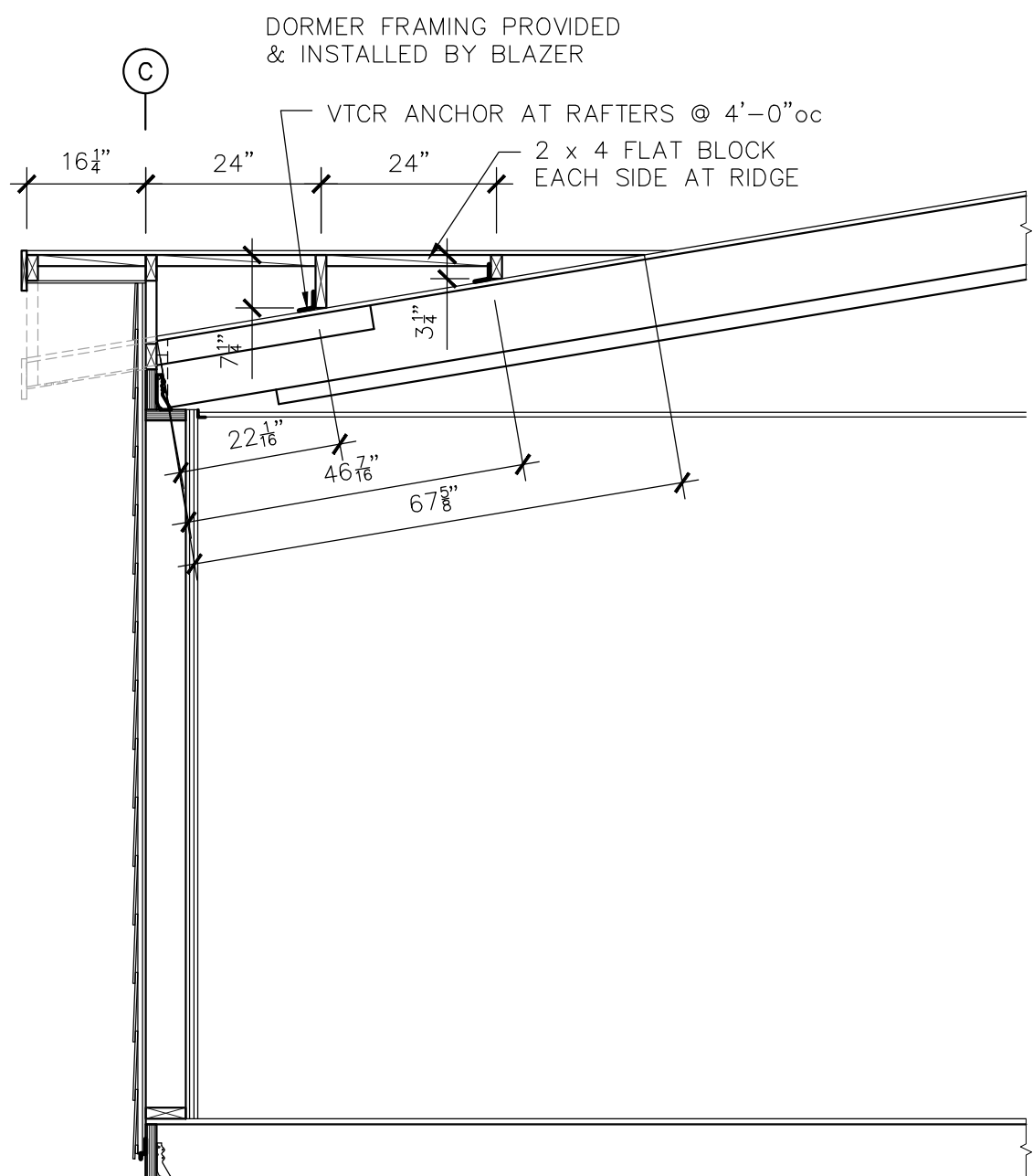
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1 CHORD SPLICE DETAIL
1 1/2" = 1'-0" SIMILAR AT FLOOR



2 DORMER FRAMES
1/2" = 1'-0"



SECTION - B
SCALE: 1/2" = 1'-0"



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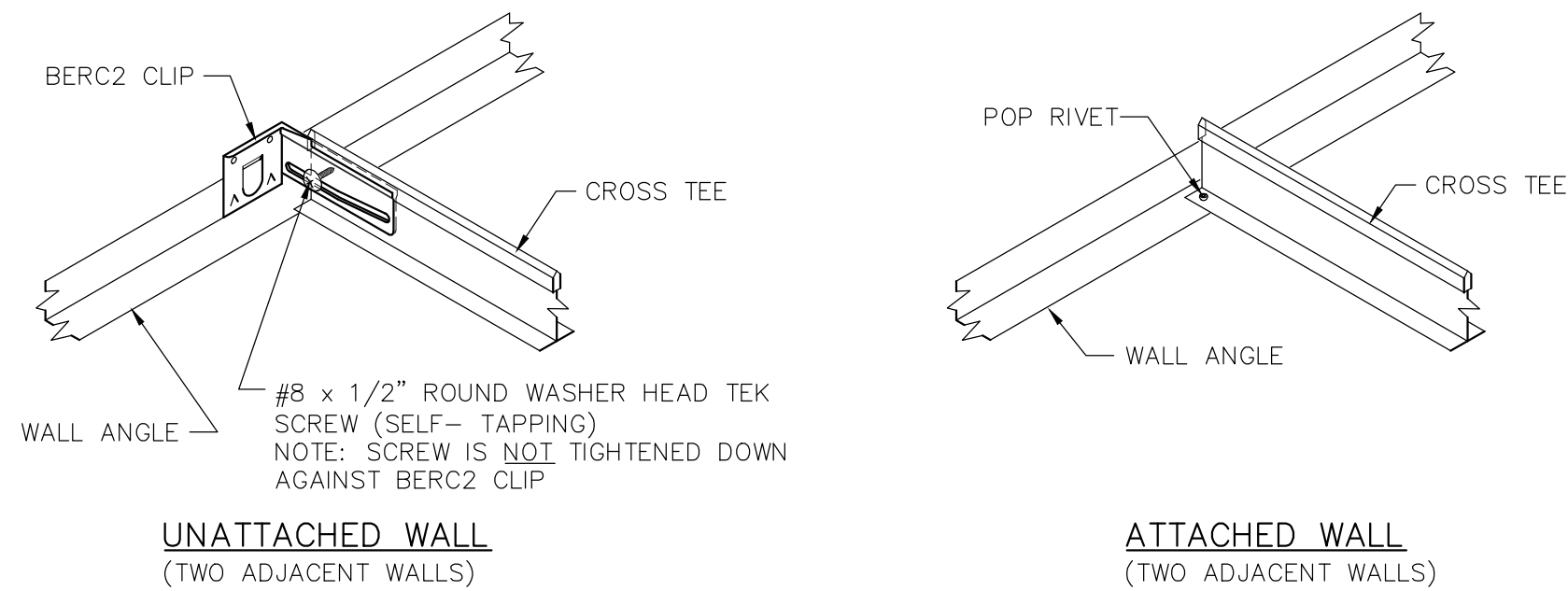


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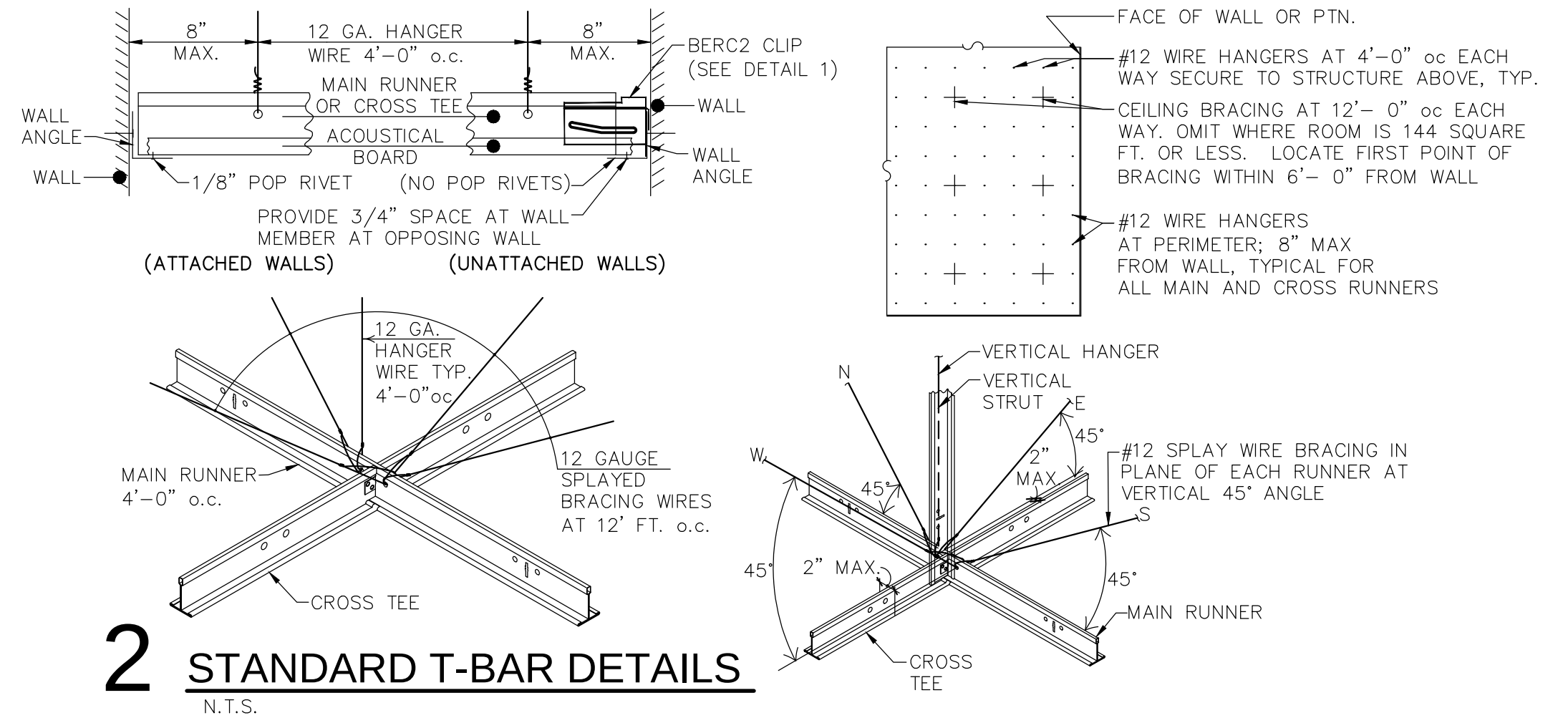
Job No: 19668
A-4.1



1 SEISMIC ATTACHMENT AT WALLS

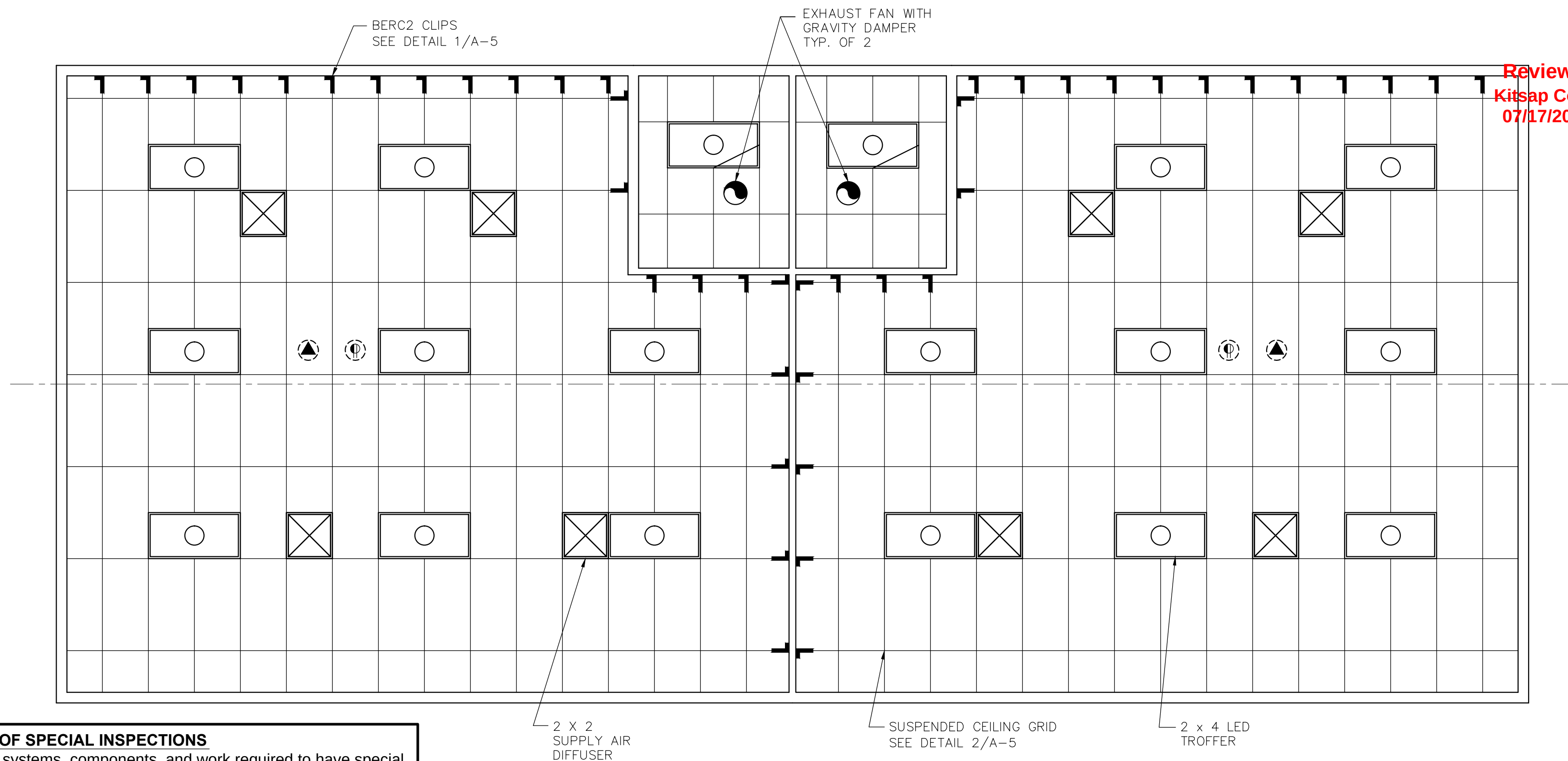
N.T.S. [ARMSTRONG SEISMIC 'Rx' SUSPENSION SYSTEM (ESR 1308)]

SEISMIC BERC2 CLIP
 -FACTORY INSTALLED AT TWO ADJACENT WALLS.
 -SCREW TIGHTENED FOR SHIPPING IN ROOMS WHERE
 CEILING CROSSES MOD LINE, LOOSEN SCREW ON SITE
 BY SET UP CREW



2 STANDARD T-BAR DETAILS

N.T.S.



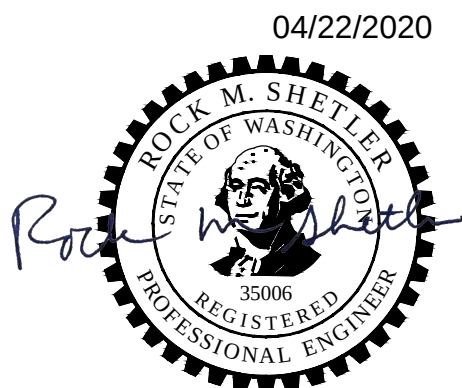
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STATEMENT OF SPECIAL INSPECTIONS
 The materials, systems, components, and work required to have special inspections are listed below. Inspections will be completed by the engineer of record.

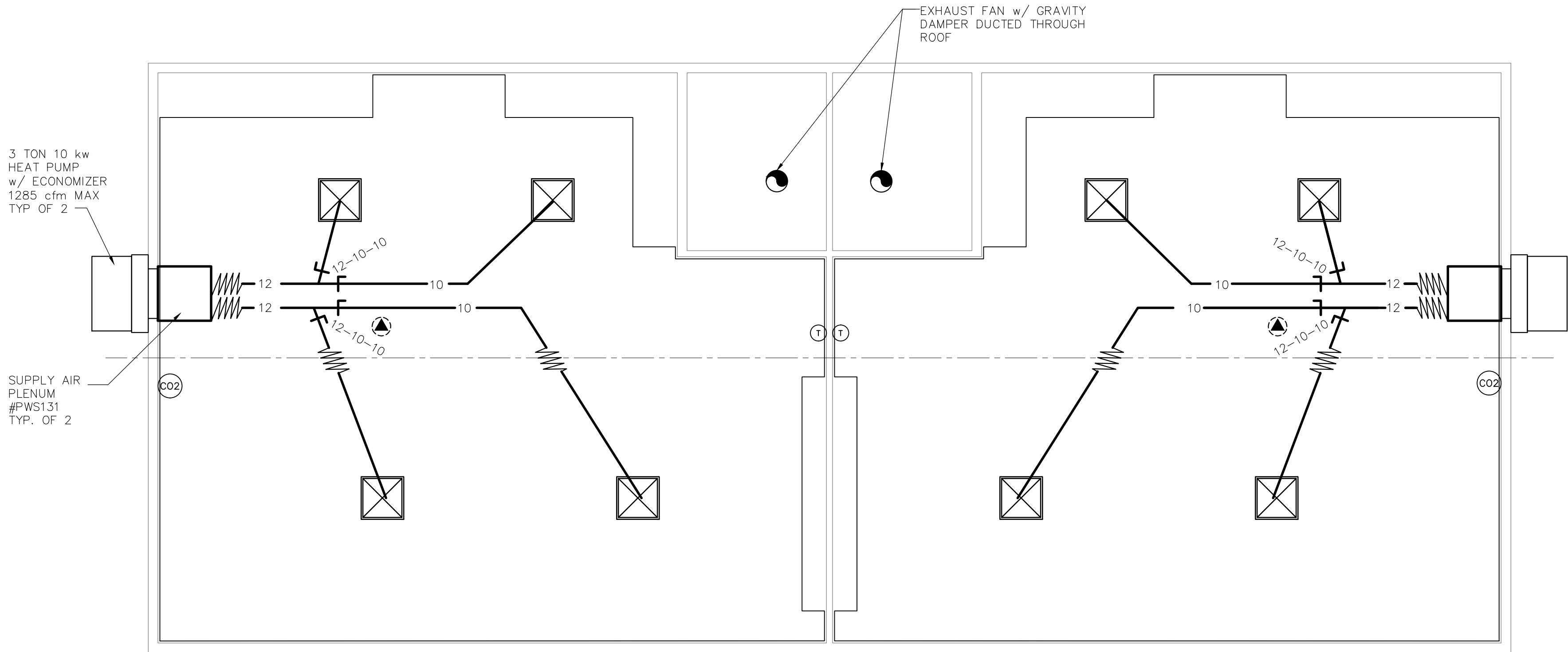
Special inspection for suspended ceiling system:
 Periodic inspection of the suspended ceiling system to verify that it complies with ESR-1308.

REFLECTED CEILING PLAN

SCALE: 1/4" = 1'-0"



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MECHANICAL PLAN

SCALE: 1/4" = 1'-0"

MECHANICAL NOTES:

- DUCT MATERIAL IS 26 GA. GALV. AND FLEX DUCT. DUCTWORK SHALL BE SUPPORTED PER 2015 IMC WAC CHAPTER 6. SECTION 603.
- MATERIAL IN DUCTS SHALL HAVE A FLAME SPREAD INDEX OF LESS THAN 25, SMOKE DEVELOPMENT OF 50 PER 2015 IMC WAC CHAPTER 6. SECTION 602.
- LOW PRESSURE DUCT SYSTEMS SHALL HAVE LONGITUDINAL AND TRANSVERSE JOINTS, SEAMS AND CONNECTIONS OF SUPPLY AND RETURN DUCTS AND PLENUMS SECURELY FASTENED AND SEALED WITH WELDS, GASKETS, MASTICS (ADHESIVES), MASTIC-PLUS EMBEDDED-FABRIC SYSTEMS OR APPROVED TAPES INSTALLED IN ACCORDANCE WITH 2015 IMC WAC CHAPTER 6 SECTION 603.9.
- WHEN ISOLATION SLEEVES ARE USED AT LINE CONNECTIONS TO PLENUMS, THEN THEY SHALL COMPLY WITH IMC CHAPTER 6.
- 10" DIFFUSERS WITH NO MANUAL DAMPERS. USE FLOW CONTROLS AT WYES, TYPICAL AS NOTED ON PLAN.
- MINIMUM OUTSIDE AIR VENTILATION PER 2015 IMC WAC CHAPTER 4, TABLE 403.3.1.1.
- OUTSIDE AIR DAMPERS SHALL COMPLY WITH 2015 WSEC, SECTION C403.2.4.3.
- ALL NEW SYSTEMS HAVING A TOTAL COOLING CAPACITY OF GREATER THAN 20,000 Btu/h REQUIRE ECONOMIZERS PER WSEC 403.3 EXCEPT AS PERMITTED BY C403.3 EXCEPTION 1
- THIS BUILDING IS EQUIPPED WITH A DOAS PER 2015 WSEC SECTION C 403.6.

	QTY.	SIZE	DESCRIPTION
HVAC	2	3 TON	10 KW BARD WALL HUNG HEAT PUMP w/ ERV – 11 EER
INT. THERMOSTAT	2		BARD #8403-060 w/ MICROPROCESSOR– 7 DAY PROGRAMMABLE AUTOMATIC SETBACK– DEADBAND CONTROL
CO2 SENSOR	2		BARD #8403-067
EXHAUST FAN	2	80 cfm	SWITCHED WITH LIGHTS IN RESTROOMS

MECHANICAL NOTES: (cont.)

MECHANICAL EQUIPMENT INSTALLATION IN OR ON THIS BUILDING SHALL BE IN ACCORDANCE WITH THE REQUIREMENTS OF THE 2015 IMC WAC CHAPTER 6.

ROUND FLEX DUCT SHALL BE U.L. LISTED CLASS 1, STANDARD 181 - FACTORY MADE AIR DUCTS AND AIR CONNECTORS. MEASURED IN ACCORDANCE TO ASTM C 518 OR ASTM C 177 AT 75DEG F MEAN TEMPERATURE. INSTALLATION SHALL BE IN ACCORDANCE WITH MANUFACTURERS INSTALLATION INSTRUCTIONS.

MECHANICAL DRAWINGS SHOW DUCTWORK SIZES TO BE CLEAR INSIDE DIMENSION.

DUCT INSULATION SHALL COMPLY WITH 2015 IMC WAC CHAPTER 6, SEC 604.

ELECTRICIAN MUST VERIFY ALL ELECTRICAL REQUIREMENTS AND LOCATIONS.

THERMOSTAT SCHEDULING TO BE PERFORMED ON SITE BY OTHERS.

ALL HVAC EQUIPMENT LEAVES FACTORY WIRED FOR 240 VOLT OPERATION
THE ACCEPTABLE OPERATING RANGE FOR THE 240V & 208V TAPS ARE:

TAP	RANGE
240	253 -216
208	220-187

SITE MECHANICAL CONTRACTOR IS RESPONSIBLE FOR MAKING SURE THE RIGHT TAP IS CONNECTED FOR THE APPLIED SITE VOLTAGE.

AIR FILTERS IN HVAC UNITS OR SYSTEMS ARE TO BE CHANGED EVERY 30 DAYS BY OTHERS ON SITE.

REGISTER AIR FLOW TEST AND BALANCE OF HVAC SYSTEM TO BE PROVIDED AND PERFORMED BY OTHERS ON SITE.

HVAC SITE CONTRACTOR IS RESPONSIBLE FOR BALANCING THE SYSTEM. (2015 IMC WAC 403.3.1.5)

MECHANICAL SYMBOLS

SYMBOL	DESCRIPTION
	2'x2' SUPPLY AIR DIFFUSER
	FLEX DUCT
	SUPPLY DUCT w/DIAMETER INDICATOR
	DAMPER IN SUPPLY DUCT AT WYE
	SUPPLY WYE w/ DUCT CONNECTION SIZES INDICATED
	THERMOSTAT
	CO2 SENSOR
	EXHAUST FAN

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DATE	REVISION	BY								

PACKAGE *SPVU* HIGH EFFICIENCY WALL MOUNT HEAT PUMP – SCHEDULE																																																																													
								DOAS/ERV/ELECTRICAL ①				DOAS/ERV/ELECTRICAL ②				COOLING CAPACITY ③								HEATING CAPACITY ④				DOAS ENERGY RECOVERY				UNIT ELECT. INFORM.				HEAT STRIPS ELECT. INFORM.						ADDITIONAL REMARKS																																			
TAG	QTY	BARD MODEL #	TONS	COMP TYPE SCROLL	TOTAL CFM NOM. PART/FULL	BLR. TYPE.	ECON. 100% FREEFLOW	DOAS ERV OSA VENTIL.	LOW VENTILATION MODE			FULL VENTILATION MODE			OUTSIDE DB	ENT DB	ENT WB	EER	IPLV	COOL CAP. BTUH PART LOAD	SENS. CAP. BTUH PART LOAD	COOL CAP. BTUH FULL LOAD	SENS. CAP. BTUH FULL LOAD	OUTSIDE DB	COP	HTG CAP. BTUH PART/LOAD	HTG CAP. BTUH FULL/LOAD	SUMMER EFFICIENT	OUTDOOR DB/WB DEG'S	HRS BTUH	HRL BTUH	WINTER EFFICIENT	INDOOR DB	MOP	V–PH	MCA	MOP	CKT	V–PH	MCA	WHR BTUH		CKT	ELEC. HEAT KW	ELEC. HEAT BTUH	OPER. WGT. LBS.																															
									V–PH	ERV	ECM BLOWER MOTOR	V–PH	ERV	ECM BLOWER MOTOR																																																															
HP–1	2	C36HA–A10ZP4XXR	3	2–STAGE	750 1100	ECM	NO	388 450	230/1	AMPS–1.3 WATTS–296	AMPS–.87 WATTS–95	230/1	AMPS–2.2 WATTS–497	AMPS–1.74 WATTS–192	95	80	67	11.0	14.5	23.4K	18.5K	35K	26.3K	47	3.3	22.7K	31K	65%	95/70	6,318	1,711	80%	1,711	23,328	230/1	27	40	A	240/1	52	60	B	10	34,130	678	1, 2, 3, 4, 5, 6, 7, 8																															
ADDITIONAL REMARKS: 1 – ENERGY MODEL PLAN APPROVAL #15FBS1700193 2 – INCLUDE BARD WALL CURB #TCURBF3642A–4. 3 – THERMOSTAT, BARD #8403–060, 7–DAY PROGRAMMABLE. 4 – WALL CO2 SENSOR. #8403–067 5 – OCCUPANCY SENSOR, (SUPPLIED BY BLAZER) 6 – GPS (FIELD INSTALLED CONTROL KIT). 7 – 2" FILTER. 8 – ERV (DOAS) ENERGY RECOVERY. 9 – UNIT COLOR IS *BUCKEYE GRAY* 10 – PRE INSTALLED OUTDOOR THERMOSTAT, SET AT 40DEG'S. ** M.C. TO REFER TO INSTALLATION INSTRUCTIONS FOR START UP AND EQUIPMENT SET. ** M.C. TO CHECK SITE VOLTAGE AND SET CORRECT TAP ON TRANSFORMER. ** M.C. TO SET AND PROGRAM THERMOSTAT PER CUSTOMERS REQUIREMENTS.										C36H1 <table><tr><td>ERV Watts – Low</td><td>296 Watts</td><td>Blower Full Load</td><td>192 Watts</td></tr><tr><td>ERV Amps – Low</td><td>1.3 Amps</td><td>Blower Full Load</td><td>1.74 Amps</td></tr><tr><td>ERV CFM – Low</td><td>300 CFM</td><td>Blower Part Load</td><td>95 Watts</td></tr><tr><td>ERV Watts – Med</td><td>415 Watts</td><td>Blower Part Load</td><td>0.87 Amps</td></tr><tr><td>ERV Amps – Med</td><td>1.8 Amps</td><td></td><td></td></tr><tr><td>ERV CFM – Med</td><td>375 CFM</td><td>Compressor Full</td><td>2588 Watts</td></tr><tr><td>ERV Watts – Hi</td><td>497 Watts</td><td>Compressor Full</td><td>11.46 Amps</td></tr><tr><td>ERV Amps – Hi</td><td>2.2 Amps</td><td>Compressor Part</td><td>1734 Watts</td></tr><tr><td>ERV CFM – Hi</td><td>450 CFM</td><td>Compressor Port</td><td>7.99 Amps</td></tr><tr><td></td><td></td><td></td><td></td></tr><tr><td></td><td></td><td>Outdoor Fan</td><td>380 Watts</td></tr><tr><td></td><td></td><td>Outdoor Fan</td><td>1.67 Amps</td></tr></table>										ERV Watts – Low	296 Watts	Blower Full Load	192 Watts	ERV Amps – Low	1.3 Amps	Blower Full Load	1.74 Amps	ERV CFM – Low	300 CFM	Blower Part Load	95 Watts	ERV Watts – Med	415 Watts	Blower Part Load	0.87 Amps	ERV Amps – Med	1.8 Amps			ERV CFM – Med	375 CFM	Compressor Full	2588 Watts	ERV Watts – Hi	497 Watts	Compressor Full	11.46 Amps	ERV Amps – Hi	2.2 Amps	Compressor Part	1734 Watts	ERV CFM – Hi	450 CFM	Compressor Port	7.99 Amps							Outdoor Fan	380 Watts			Outdoor Fan	1.67 Amps	The sequence of operation for the Integrated DOAS system. 1. Upon a call from the occupancy sensor the (DOAS) ERV and the indoor (ECM) motor will start in low vent mode and ventilate the space continuously as occupied. Note: 1 on the HVAC Schedule. 2. Upon a call from the CO2 sensor the (DOAS) ERV and the indoor (ECM) motor will change to full vent mode and ventilate the space until the CO2 sensor is satisfied and then revert back to the low vent mode during the occupied time. Note: 2 on the HVAC Schedule. 3. The Heating and Cooling section will only work if there is a Heating or Cooling call from the thermostat. This action works entirely independent of the DOAS ventilation portion. Note: 3 & 4 on the HVAC Schedule. 4. This action will keep repeating itself as required by the occupancy sensor, CO2 sensor and Room Thermostat.									
ERV Watts – Low	296 Watts	Blower Full Load	192 Watts																																																																										
ERV Amps – Low	1.3 Amps	Blower Full Load	1.74 Amps																																																																										
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MINIMUM VENTILATION RATES PER IMC SECTION 403									
room #	name	Az (sf)	sf/1000	Occ. Dens	Pz (calc)	Pz (used)	Rp (cfm/person)	Ra (cfm/sf)	Vbz (cfm)
1	Classroom A	770	0.77	35	27	27	10	0.12	362
2	Classroom B	770	0.77	35	27	27	10	0.12	362
3	Restroom #1	52	0.052	n/a	n/a	n/a	5	0.06	n/a
4	Restroom #2	52	0.052	n/a	n/a	n/a	5	0.06	n/a
									725 cfm

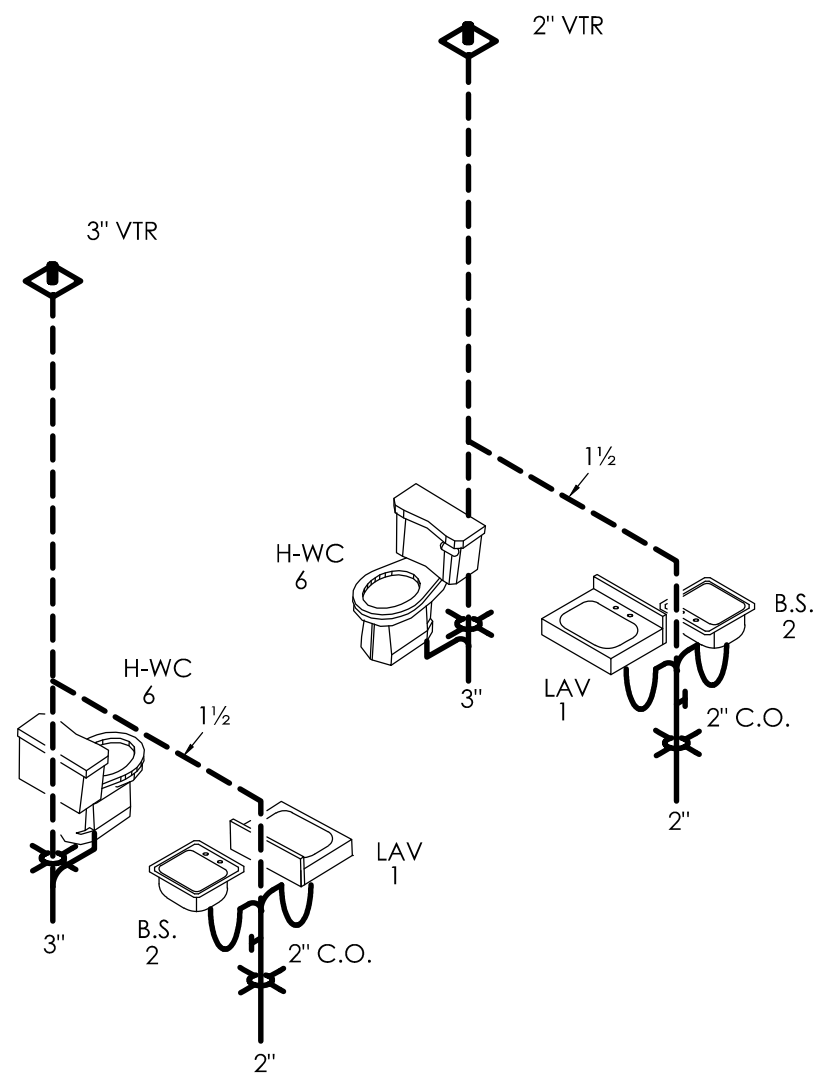
Az = room area (sf)
Occ. Dens = occupant density (from Table 403.3)
Pz (calc) = zone population or occupant quantity (calculated)
Pz (used) = zone population or occupant quantity (user can override the calculation-increase only)
Rp = people outdoor airflow rate in breathing zone (cfm/person)
Ra = area outdoor airflow rate in breathing zone (cfm/sf)
Vbz = Breathing zone outdoor air flow rate per eq. 4-1 (Rp*Pz+Ra*Az)

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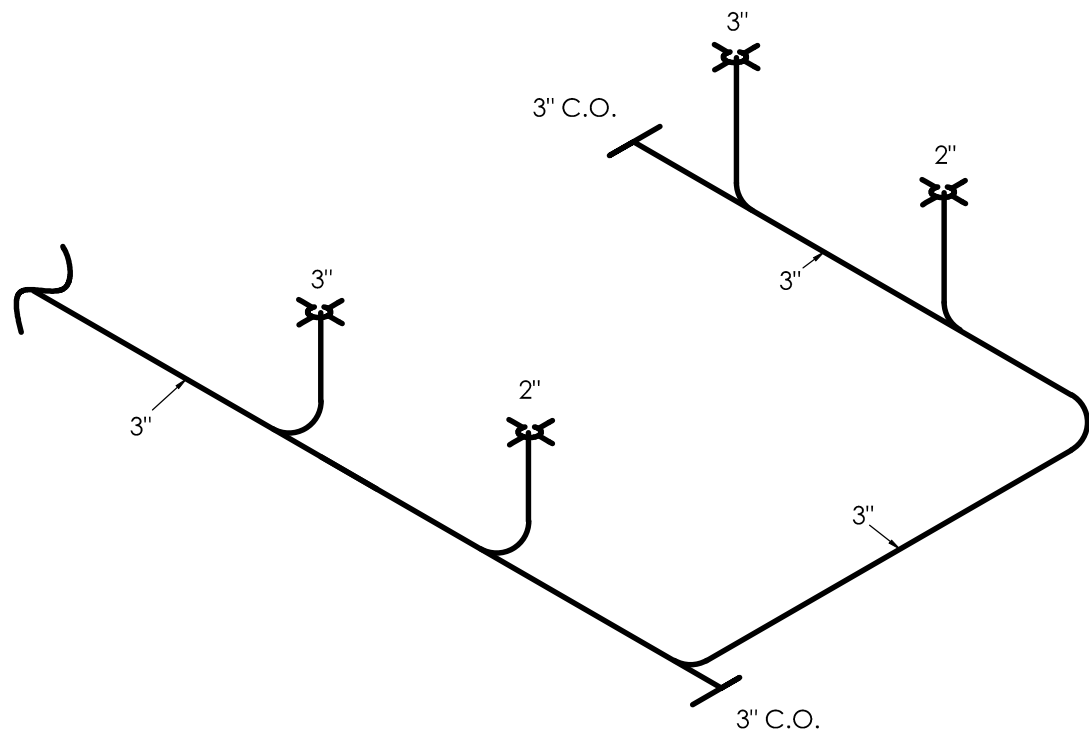
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M-2

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PLUMBING BELOW FLOOR JOIST NOT INCLUDED.



DRAINAGE AND VENT PIPING:

- FIXTURE UNITS _____ 18
- SIZE OF BUILDING DRAIN _____ 3"
- AGGREGATE AREA _____ 10.21

GENERAL NOTES:

- WASHINGTON: SIZED TO UPC 2015.
- D.W.V. MATERIAL - P.V.C.
- PER 2009 ANSI A117.1 SECTION 606.6. P-TRAPS ON ACCESSIBLE FIXTURES INSULATED.
- CONTINUATION OF WASTE LINE DONE ON SITE BY OTHERS.
- PLUMBING APPLIANCE -
- VENT STUB 10' OFF OF PEAK OF ROOF.

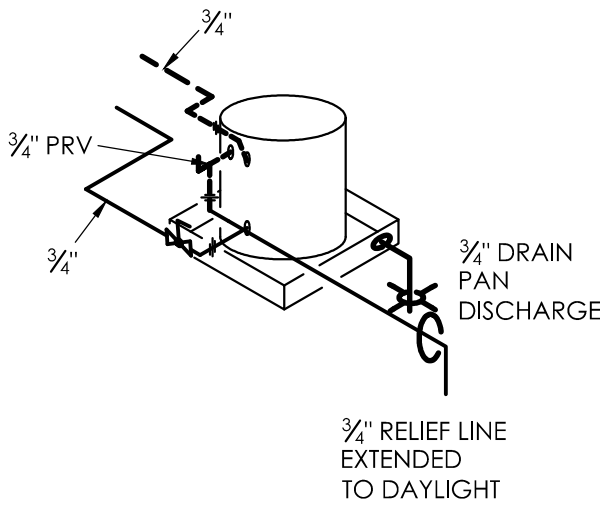
GENERAL NOTES:

- SIZED TO 2015 UPC WAC.
- POTABLE WATER MATERIAL - COPPER AND AQUAPEX.
- CONTINUATION OF WATER MAIN PROVIDED AND INSTALLED ON SITE BY OTHERS.
- HEAT TAPE PROVIDED AND INSTALLED ON SITE BY OTHERS.
- HAMMER ARRESTORS INSTALLED PER 2015 UPC 609.10.
- 2015 UPC WAC PEX TUBING SHALL NOT BE INSTALLED WITHIN THE FIRST 18" OF PIPE CONNECTED TO THE WATER HEATER.
- 2015 UPC 608.3 THERMAL EXPANSION DEVICE IS TO BE PROVIDED AND INSTALLED ON SITE BY OTHERS WHEN REQUIRED.
- 2015 UPC 507.2. WATER HEATERS SHALL BE ANCHORED OR STRAPPED.
- 2015 UPC 407.3 PUBLIC LAVATORIES SHALL HAVE TEMPERING VALVES MEETING ASSE 1070.
- 2015 WSEC C404.2 WATER HEATER SHALL MEET THE REQUIREMENTS OF TABLE 404.2.
- 2015 WSEC C404.6 WATER PIPING SHALL BE INSULATED FROM THE WATER HEATER TO THE TERMINATION OF THE HEATED WATER FIXTURE SUPPLY PIPE IN ACCORDANCE WITH TABLE 403.2.9. PER THIS TABLE ALL PIPING LESS THAN 1" NOMINAL SHALL BE INSULATED WITH 1" INSULATION.
- 2009 ANSI/ASHRAE A117.1 606.6 EXPOSED PIPES AND SURFACES. WATER SUPPLY AND DRAIN PIPES UNDER LAVATORIES AND SINKS SHALL BE INSULATED OR OTHERWISE CONFIGURED TO PROTECT AGAINST CONTACT. THERE SHALL BE NO SHARP OR ABRASIVE SURFACES UNDER LAVATORIES AND SINKS.
- PUBLIC USE TOILET SEATS SHALL COMPLY WITH 2015 UPC 411.3 AND PLASTIC SEATS WITH IAPMO Z124.5.
- PUBLIC USE WATER CLOSETS SHALL BE ELONGATED AND COMPLY WITH 2015 UPC 411.1.

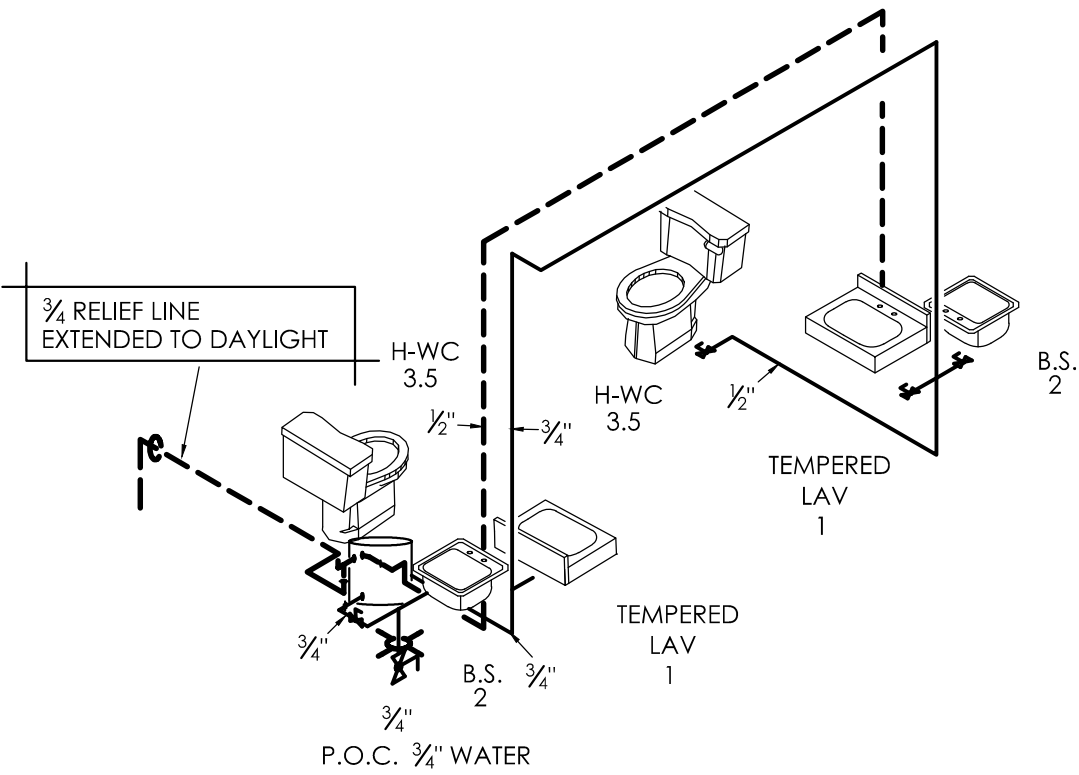
PLUMBING FIXTURE SCHEDULE		
QTY	FIXTURE	DESCRIPTION
1	HC-PATT FLUSH-Right	GERBER 21-318-R 1.6 GPF Elongated
1	HC-PATT FLUSH-Left	GERBER 21-318 1.6 GPF Elongated
2	LAVATORY SINK-wall	GERBER 12-314 W/ OFF SET GRID DRAIN
2	BAR SINK 15 x 15	PROFLO PFSR151562A
2	FAUCET- H-Lav	A/S 7385.004.002 2.2 GPM
2	FAUCET- H-bar	A/S 7500.170.002 2.2 GPM
1	WATER HEATER - 6 GALLON	AO SMITH EJC-6 1650 WATT
2	TEMPERING VALVE	WATTS LFUSG-B-M2

PLUMBING SCHEMATICS & DATA

Job: 19664 Drawn by Paul: 3-18-2020



WATER HEATER PAN DETAIL

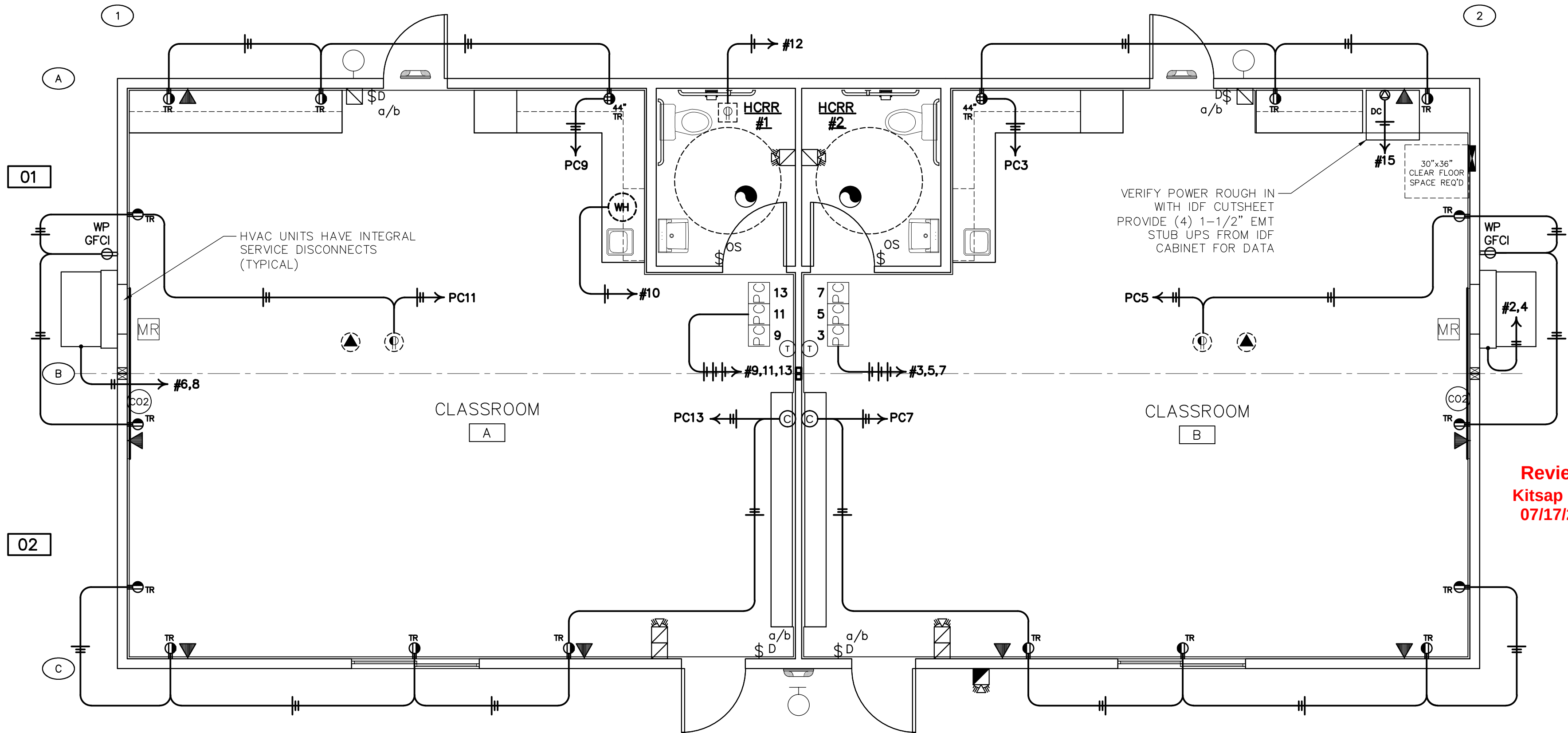


WATER PIPING:

- FIXTURE UNITS _____ 13
- DEVELOPED LENGTH _____ 40'
- ELEVATION DIFFERENCE _____ X
- STREET PRESSURE _____ 46 to 60
- METER SIZE _____ 3/4"
- BUILDING SUPPLY SIZE _____ 3/4"

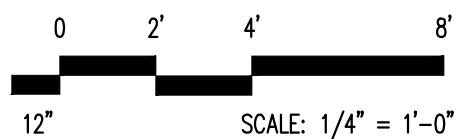
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							Issue Date: 3-24-20	

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ELECTRICAL POWER PLAN

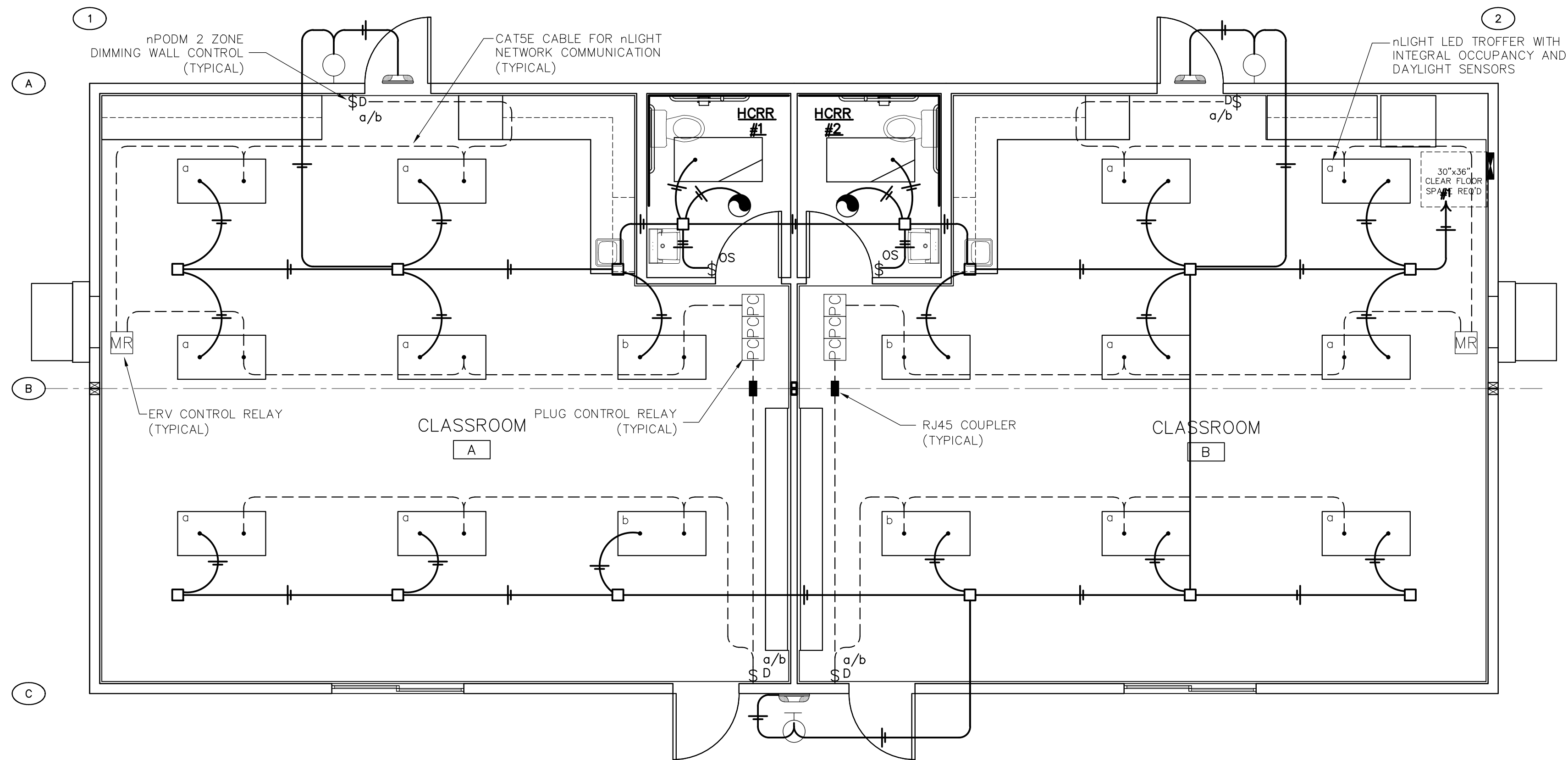


JF 3/19/20

	QTY.	SIZE	DESCRIPTION
ELECTRIC PANEL	1	200 AMP	120/240V - SINGLE PHASE - STUB THRU- METALLIC RACEWAY SYSTEM
HVAC	2	3 TON	10 KW BARD WALL HUNG HEAT PUMP w/ERV - 11 EER
THERMOSTAT	2		BARD #8403-060 w/ MICROPROCESSOR- 7 DAY PROGRAMMABLE AUTOMATIC SETBACK- DEADBAND CONTROL
CO2 SENSOR	2		BARD #8403-067
LIGHTING	16	2 x 4	LED VOLUMETRIC TROFFER- nLIGHT ENABLED- 6000 LUMEN- 48 WATTS- 4000K- LITHONIA - 2BLT4 60L ADPT EZ1 LP840 N100 NES7ADCX PWS1836
	2	2 x 4	LED VOLUMETRIC TROFFER - 6000 LUMEN - 48 WATTS - 4000K- LITHONIA - 2BLT4 60L ADPT EZ1 LP840 PWS1836
	3	18 WATT	LED WALL PACK w/ INTEGRAL PHOTOCCELL RAB SLIM18/PC
EXHAUST FAN	2	80 cfm	CONTROLLED WITH LIGHTS IN RESTROOMS
WATER HEATER	1	6 GAL	IN CABINET - 120V - 1650W - PROVIDE BREAKER LOCK OUT DEVICE

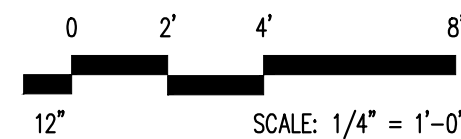
ELECTRICAL SYMBOLS							
SYMBOL	DESCRIPTION	AFF TO TOP	REMARKS	SYMBOL	DESCRIPTION	AFF TO TOP	REMARKS
	ELECTRIC PANEL	72"			WALL HUNG HVAC UNIT	AS REQUIRED	SEE MECH SCHEDULE AND CALCS
	DUPLEX RECEPTACLE TAMPER RES. - CONTROLLED	20"	180 VA EACH		THERMOSTAT	48"	4" SQ BOX SINGLE GANG MR WITH 1/2" CONDUIT STUB UP
	DUPLEX RECEPTACLE CEILING MOUNT- CONTROLLED	CEILING	180 VA EACH		CO2 SENSOR	48"	4" SQ BOX SINGLE GANG MR WITH 1/2" CONDUIT STUB UP
	SINGLE CLOCK HANGER RECEPTACLE	84"	180 VA EACH		80 CFM EXHAUST FAN	CEILING	25 VA EACH
	QUADPLEX RECEPTACLE- TAMPER RES. - CONTROLLED	20"	360 VA EACH		6 GALLON WATER HEATER	AS REQUIRED	1650 VA EACH PROVIDE BREAKER LOCK OUT DEVICE
	WEATHERPROOF GFCI RECEPTACLE	AS NOTED	180 VA EACH		nLIGHT ENABLED LED TROFFER w/ INTEGRAL SENSORS	CEILING	48 VA EACH
	DEDICATED WP RECEPTACLE FOR HEAT TRACE	UNDER FLOOR	500 VA EACH -GROUND FAULT EQUIPMENT PROTECTION DEVICE		LED TROFFER	CEILING	48 VA EACH
	nLIGHT DIMMING CONTROL SWITCH CAT5E CONNECTED	48"	DIMMING CONTROL. LOWER CASE LETTERS DESIGNATE ZONING		LED WALL PACK WITH INTEGRAL PHOTOCCELL	84"	20 VA EACH
	WALL MOUNT OCCUPANCY SENSOR	48"	AUTOMATIC ON / OFF CONTROL		EXT. EMERGENCY LIGHT	ABOVE DOOR	WITH 90 MINUTE BATTERY BACK UP
	nLIGHT nAR40 ERV CONTROL RELAY	ABOVE CEILING	CONTROLLED BY nLIGHT ENABLED FIXTURE OCCUPANCY SENSORS		FIRE ALARM EXTERIOR HORN/STROBE SHEET E-4	84"	3/4" RACEWAY ONLY STUB UP AND DOWN. PAINT RACEWAY AND BACK BOX SUBSTANTIALLY RED IN COLOR
	nLIGHT nPP20PL BP PLUG LOAD CONTROL RELAY	ABOVE CEILING	CONTROLLED BY nLIGHT ENABLED FIXTURE OCCUPANCY SENSORS		PULL STATION	48"	
	PHONE/DATA ROUGH IN 4" SQ BOX w/ SINGLE GANG MR	20"	3/4" FLEX STUBBED UP AND DOWN		FIRE ALARM INTERIOR HORN/STROBE SHEET E-4	84"	
	DATA BOX IN CEILING	CEILING	4" SQ BOX SINGLE GANG MR - NO CONDUIT PROVISIONS BY BLAZER				

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3-23-20	ENGINEERING REVIEW	HEM			28x64		File Copy:		
4-6-20	ADDED IDF CABINET	ARS			WA GOLD		Drawn By:	AJB	
DATE	REVISION	BY					Issue Date:	3-24-20	



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ELECTRICAL LIGHTING PLAN



JF 3/19/20

	QTY.	SIZE	DESCRIPTION
ELECTRIC PANEL	1	200 AMP	120/240V - SINGLE PHASE - STUB THRU- METALLIC RACEWAY SYSTEM
HVAC	2	3 TON	10 KW BARD WALL HUNG HEAT PUMP w/ERV - 11 EER
THERMOSTAT	2		BARD #8403-060 w/ MICROPROCESSOR- 7 DAY PROGRAMMABLE AUTOMATIC SETBACK- DEADBAND CONTROL
CO2 SENSOR	2		BARD #8403-067
LIGHTING	16	2 x 4	LED VOLUMETRIC TROFFER- nLIGHT ENABLED- 6000 LUMEN- 48 WATTS- 4000K- LITHONIA - 2BLT4 60L ADPT EZ1 LP840 N100 NES7ADCX PWS1836
	2	2 x 4	LED VOLUMETRIC TROFFER - 6000 LUMEN - 48 WATTS - 4000K- LITHONIA - 2BLT4 60L ADPT EZ1 LP840 PWS1836
	3	18 WATT	LED WALL PACK w/ INTEGRAL PHOTOCCELL RAB SLIM18/PC
EXHAUST FAN	2	80 cfm	CONTROLLED WITH LIGHTS IN RESTROOMS
WATER HEATER	1	6 GAL	IN CABINET - 120V - 1650W - PROVIDE BREAKER LOCK OUT DEVICE

ELECTRICAL SYMBOLS

SYMBOL	DESCRIPTION	AFF TO TOP	REMARKS	SYMBOL	DESCRIPTION	AFF TO TOP	REMARKS
	ELECTRIC PANEL	72"			WALL HUNG HVAC UNIT	AS REQUIRED	SEE MECH SCHEDULE AND CALCS
	DUPLX RECEPTACLE TAMPER RES. - CONTROLLED	20"	180 VA EACH		THERMOSTAT	48"	4" SQ BOX SINGLE GANG MR WITH 1/2" CONDUIT STUB UP
	DUPLX RECEPTACLE CEILING MOUNT- CONTROLLED	CEILING	180 VA EACH		CO2 SENSOR	48"	4" SQ BOX SINGLE GANG MR WITH 1/2" CONDUIT STUB UP
	SINGLE CLOCK HANGER RECEPTACLE	84"	180 VA EACH		80 CFM EXHAUST FAN	CEILING	25 VA EACH
	QUADPLEX RECEPTACLE- TAMPER RES. - CONTROLLED	20"	360 VA EACH		6 GALLON WATER HEATER	AS REQUIRED	1650 VA EACH PROVIDE BREAKER LOCK OUT DEVICE
	WEATHERPROOF GFCI RECEPTACLE	AS NOTED	180 VA EACH		nLIGHT ENABLED LED TROFFER w/ INTEGRAL SENSORS	CEILING	48 VA EACH
	DEDICATED WP RECEPTACLE FOR HEAT TRACE	UNDER FLOOR	500 VA EACH -GROUND FAULT EQUIPMENT PROTECTION DEVICE		LED TROFFER	CEILING	48 VA EACH
	nLIGHT DIMMING CONTROL SWITCH CAT5E CONNECTED	48"	DIMMING CONTROL. LOWER CASE LETTERS DESIGNATE ZONING		LED WALL PACK WITH INTEGRAL PHOTOCCELL	84"	20 VA EACH
	WALL MOUNT OCCUPANCY SENSOR	48"	AUTOMATIC ON / OFF CONTROL		EXT. EMERGENCY LIGHT	ABOVE DOOR	WITH 90 MINUTE BATTERY BACK UP
	nLIGHT nAR40 ERV CONTROL RELAY	ABOVE CEILING	CONTROLLED BY nLIGHT ENABLED FIXTURE OCCUPANCY SENSORS		FIRE ALARM EXTERIOR HORN-STROBE SHEET E-4	84"	3/4" RACEWAY ONLY STUB UP AND DOWN. PAINT RACEWAY AND BACK BOX SUBSTANTIALLY RED IN COLOR
	nLIGHT nPP20PL BP PLUG LOAD CONTROL RELAY	ABOVE CEILING	CONTROLLED BY nLIGHT ENABLED FIXTURE OCCUPANCY SENSORS		PULL STATION	48"	
	PHONE/DATA ROUGH IN 4" SQ BOX w/ SINGLE GANG MR	20"	3/4" FLEX STUBBED UP AND DOWN		FIRE ALARM INTERIOR HORN-STROBE SHEET E-4	84"	
	DATA BOX IN CEILING	CEILING	4" SQ BOX SINGLE GANG MR - NO CONDUIT PROVISIONS BY BLAZER				

3-19-20	ELECTRICAL ENGINEERING	JF	COPYRIGHT 2020, BLAZER INDUSTRIES, INC. THIS MATERIAL IS THE EXCLUSIVE PROPERTY OF BLAZER INDUSTRIES, INC. AND SHALL NOT BE REPRODUCED, USED, OR DISCLOSED TO OTHERS EXCEPT AS AUTHORIZED BY THE WRITTEN PERMISSION OF BLAZER INDUSTRIES.		MODULAR	Classroom w/ HCRR for: North Kitsap School District Pacific Mobile	Approved for Const:	Job No:	19668
3-23-20	ENGINEERING REVIEW	HEM			28x64		File Copy:		
DATE	REVISION	BY			WA GOLD		Drawn By:	AJB	
							Issue Date:	3-24-20	

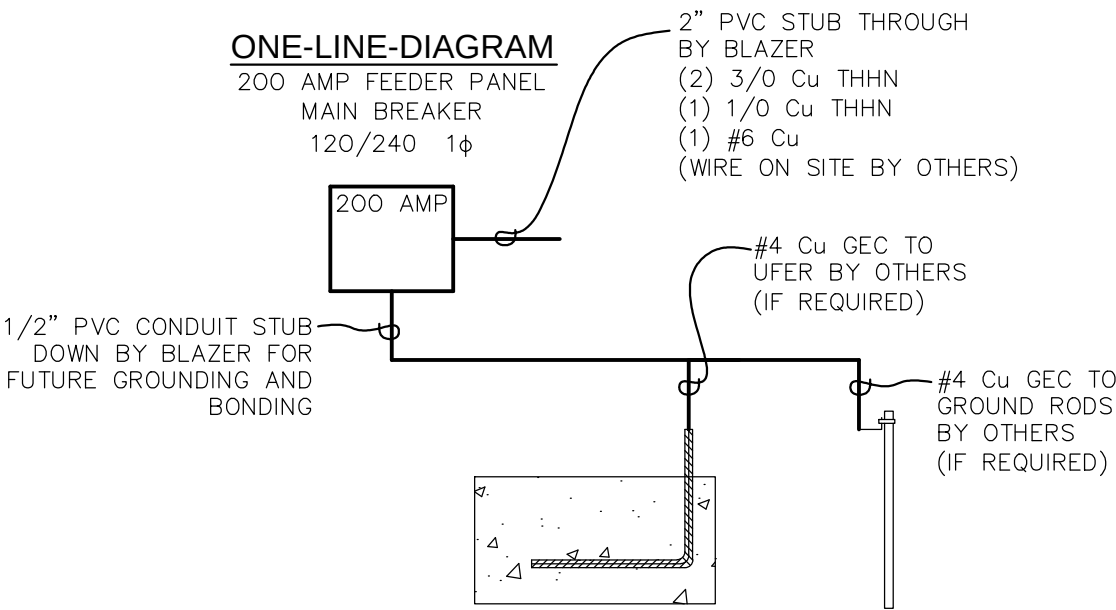
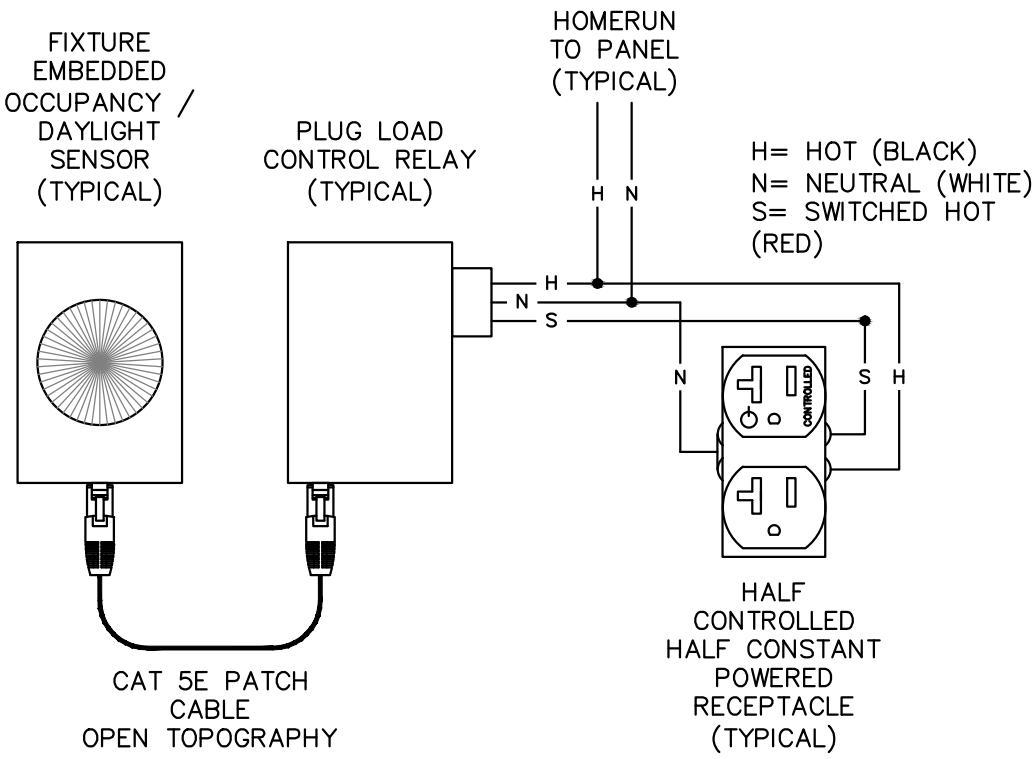
PANEL SCHEDULE											
PANEL DESIGNATION		PANEL A		VOLTS		120/240		AIC RATING: 22,000			
MOUNTING		FLUSH		PHASE		1		BUSS RATING: 200 AMP			
ENCLOSURE TYPE		NEMA 1						MCB RATING: 200 AMP			
* PROVIDE BREAKER LOCK OUT DEVICE											
** PROVIDE GFEPD CIRCUIT BREAKER											
CKT	CIRCUIT DESCRIPTION	TRIP	WIRE SIZE	CONNECTED LOAD (VA)				WIRE SIZE	TRIP	DESCRIPTION	CKT
				A		B					
1	LIGHTING	20	12	974	7052			4	80	HVAC	2
3	RECEPTACLES	20	12			720	7052	/	/	/	4
5	RECEPTACLES	20	12	720	7052			4	80	HVAC	6
7	RECEPTACLES	20	12			900	7052	/	/	/	8
9	RECEPTACLES	20	12	720	1650			12	20	WATER HEATER*	10
11	RECEPTACLES	20	12			720	500	12	20	HEAT TRACE**	12
13	RECEPTACLES	20	12	900							14
15	IDF CABINET	20	12			1500					16
17											18
19											20
CONNECTED LOAD		TOTAL LOAD:		19068.0		18444.0					
		TOTAL AMPS:		158.9		153.7					

ELECTRICAL PLAN REVIEW LOAD CALCULATION					CALC BY: JOEL FRESHOUR					
PROJECT INFO: 19668 KCDA NORTH KITSAP					DATE: 3/19/2020					
PANEL: PANEL A			VOLTAGE: 120/240		PHASE: 1		AMPACITY: 200			
FED FROM: EXISTING SERVICE							AIC RATING: 22,000			
DESCRIPTION	VA LOAD	DEMAND FACTOR	PHASE A	PHASE B		NEUTRAL A	NEUTRAL B		NOTES	
LIGHTING										
EXTERIOR LIGHTING	60	1.25	75			75				
INTERIOR LIGHTING	864	1.25	1080			1080				
EXHAUST FANS	50	1.25	63			63				
RECEPTACLES										
TOTAL	4680	1.00	2340	2340		2340	2340			
HVAC (MOTORS)										
TOTAL	8208	1.00	4104	4104						
LARGEST	2832	0.25	354	354						
HEATING	20000	1.00	10000	10000						
WATER HEATER	1650	1.00	1650			1650				
HEAT TRACE	500	1.00		500			500			
TOTALS			PHASE A	PHASE B		NEUTRAL A	NEUTRAL B			
VA			19666.0	17298.0		5208.0	2840.0			
AMPS			163.9	144.2		43.4	23.7			
LARGEST POWER PHASE 19666.0 VA 163.9 AMPS				LARGEST NEUTRAL PHASE 5208.0 VA 43.4 AMPS						
NOTES:										

BARD 3 TON - 10KW - 11EER CH UNIT

(TYPICAL OF 2)

H V A C (MOTOR, COMPRESSOR, HEATER SIZES)		
OPERATION VOLTAGE	197 MIN.	253 MAX.
COMPRESSOR	11.8 RLA	83 LRA
OUTDOOR FAN	2.5 FLA	1/3 HP
INDOOR BLOWER FAN	2.8 FLA	1/2 HP
HEAT STRIP	10 KVA	240 VOLT
MINIMUM CIRCUIT AMPS		79 AMPS
MAXIMUM OVERCURRENT PROTECTION		80 AMPS
OVERCURRENT PROTECTION SHALL BE DUAL ELEMENT TIME DELAY FUSE OR HACR CIRCUIT BREAKER		
INTERNAL SERVICE DISCONNECTS PROVIDED.		



GENERAL NOTES:

- WHEN STRANDED WIRE IS USED, ALL TERMINATIONS ARE MADE BY A PRESSURE TERMINAL, BY TAILING OFF WITH SOLID CONDUCTORS OR OTHER APPROVED MEANS OF TERMINATION.
- ALL CONDUCTORS ARE COPPER; TYPE THHN / THWN
- RATING OF STANDARD PANEL IS 22,000 A.I.C.
- WIRING METHOD IN METALLIC CONDUIT OR M.C. CABLE.
- HVAC DISCONNECTS SHALL BE LABELED WITH AN IDENTIFICATION PLATE SHOWING CIRCUIT NUMBER AND EQUIPMENT SERVED. WAC 296-46B-110 022
- EXTERIOR WEATHER PROOF GFCI SHALL HAVE A "HEAVY DUTY" WEATHER PROOF "IN USE" COVER. 2017 NEC 406.9(B)(1)
- CONTROLLED RECEPTACLES SHALL BE LABELED PER 2017 NEC 406.3(E) WITH THE TEXT "CONTROLLED" AND THIS SYMBOL
- WATER HEATER BRANCH CIRCUIT BREAKER SHALL BE CAPABLE OF BEING LOCKED OUT IN THE "OFF" POSITION OR HAVE A LOCAL DISCONNECT. 2017 NEC 422.31(B)
- HEAT TRACE RECEPTACLE SHALL BE PROTECTED BY A GROUND FAULT EQUIPMENT PROTECTION DEVICE SENSING LEAKAGE CURRENT FROM 6mA TO 50mA. 2017 NEC 427.22
- HVAC UNITS HAVE AN INTEGRAL SERVICE DISCONNECT.
- THIS PLAN IS NOT AN "AS-BUILT" CIRCUITS MAY BE RUN DIFFERENT THAN SHOWN BASED ON OBSTACLES ENCOUNTERED.

51-11C WAC 2015 WSEC CHAPTER 4 NOTES:

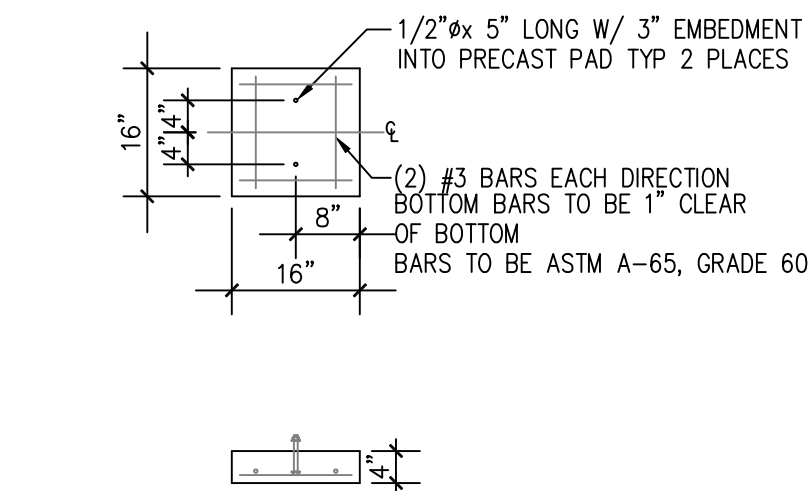
- ALL LIGHTING SHALL CONFORM TO SECTION C405
- A MINIMUM OF 90% OF LIGHTING FIXTURES HAVE EMBEDDED OCCUPANCY AND DAYLIGHT SENSORS FOR INCREASED ENERGY SAVINGS, AND ARE INDIVIDUALLY ADDRESSABLE. (C406.4)
- A MINIMUM OF 90% OF LIGHTING IS SET FOR CONTINUOUS DIMMING AND IS ADJUSTABLE BY OCCUPANTS, FOR OCCUPANT COMFORT, VIA WALL PODS. (C406.4)
- 50% OF RECEPTACLES IN CLASSROOMS, PRIVATE OFFICES, OPEN OFFICES, CONFERENCE ROOMS, COPY ROOMS, AND INDIVIDUAL WORKSTATIONS, ARE CONTROLLED BY LOCAL OCCUPANCY SENSORS (C405.10)

SPACE BY SPACE LIGHTING POWER DENSITY PER 2015 WSEC C405.4.2.1					
SPACE DESIGNATION	SQ. FT.	SPACE TYPE	WATTS SQ. FT.	BASE *	ADDITIONAL REDUCTION **
Classroom A	770	CLASSROOM	1	770	578
Classroom B	770	CLASSROOM	1	770	578
Restroom #1	52	RESTROOM	0.5	26	20
Restroom #2	52	RESTROOM	0.5	26	20
TOTAL SQ. FT.	1644		TOTAL ALLOWED		1194 W
			TOTAL INSTALLED		864 W
* BASE = SQ. FT. x ALLOWED WATTS PER SQ. FT. - TABLE C405.4.2(2)					
** ADDITIONAL REDUCTION = BASE x .75 - (C406.3.1)					

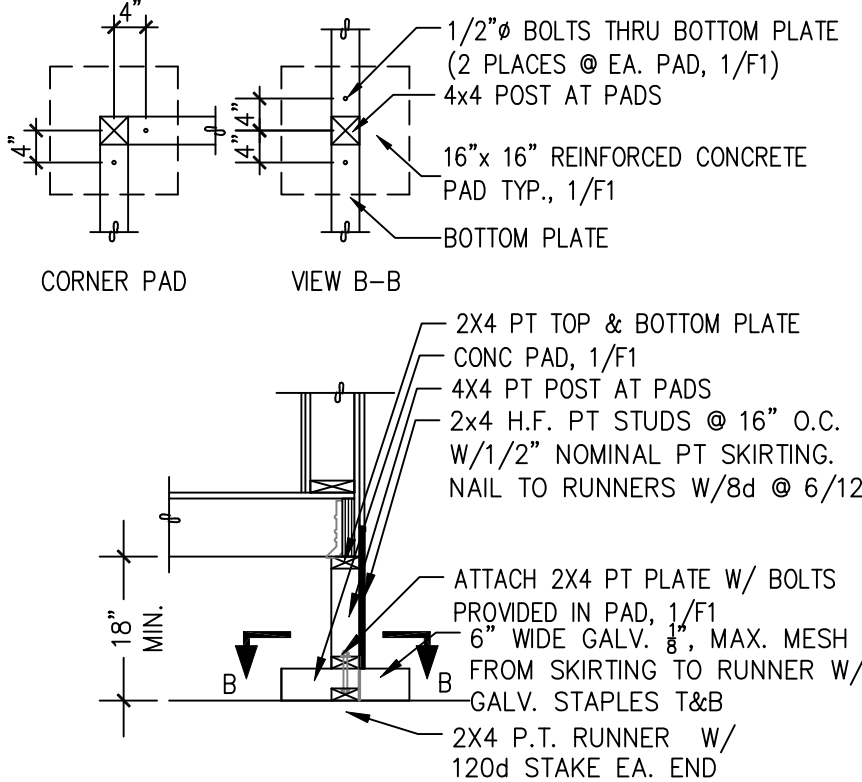
FORM A COMPLETE GROUNDING ELECTRODE SYSTEM PER 2017 NEC 250.53. PROVIDED AND INSTALLED ON SITE BY OTHERS

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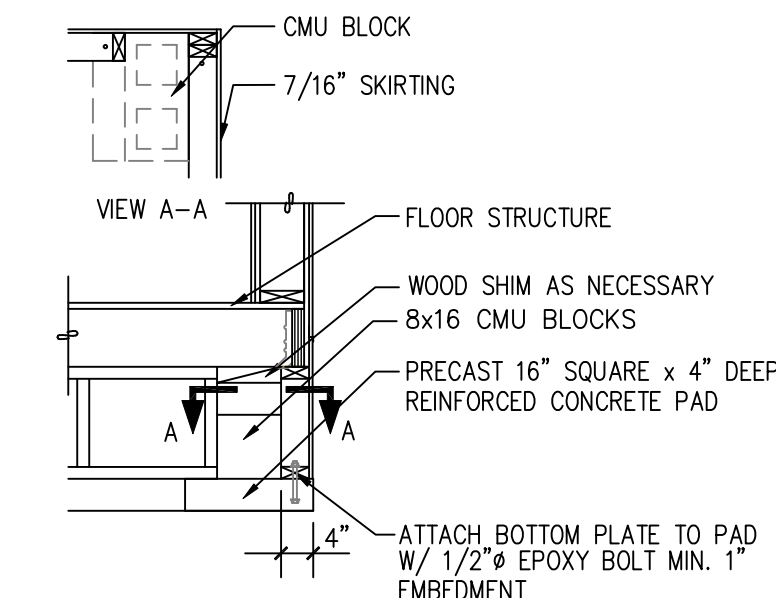
3-19-20	ELECTRICAL ENGINEERING	JF	COPYRIGHT 2020, BLAZER INDUSTRIES, INC. THIS MATERIAL IS THE EXCLUSIVE PROPERTY OF BLAZER INDUSTRIES, INC. AND SHALL NOT BE REPRODUCED, USED, OR DISCLOSED TO OTHERS EXCEPT AS AUTHORIZED BY THE WRITTEN PERMISSION OF BLAZER INDUSTRIES.		MODULAR	Classroom w/ HCRR for: North Kitsap School District Pacific Mobile	Approved for Const:	Job No: 19668
3-23-20	ENGINEERING REVIEW	HEM			28x64		File Copy:	
4-6-20	ADDED IDF CABINET	ARS			WA GOLD		Drawn By: AJB	
DATE	REVISION	BY					Issue Date: 3-24-20	



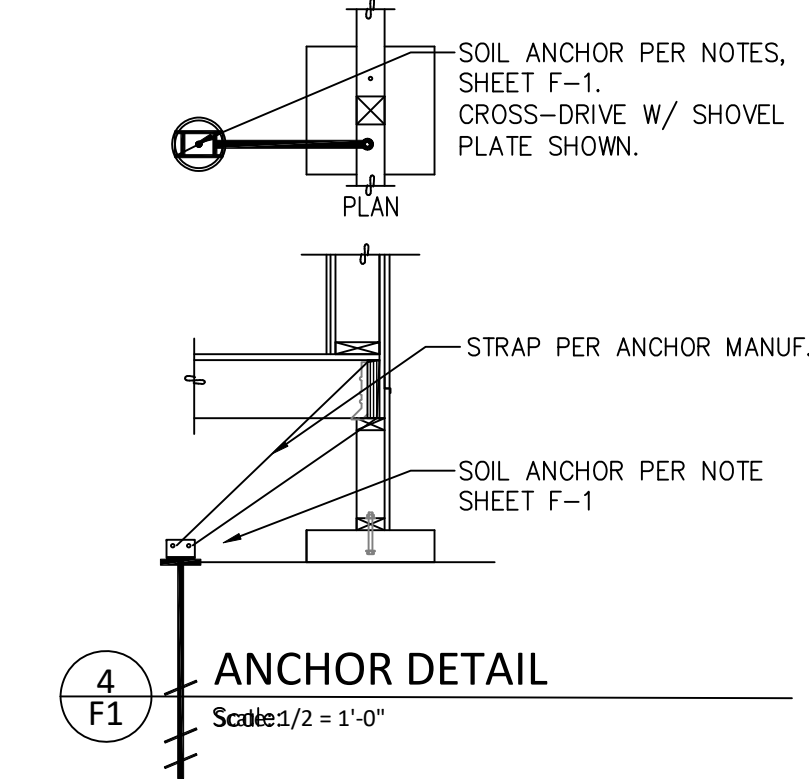
1 PRECAST PAD DETAIL
Scale: 1/2" = 1'-0"



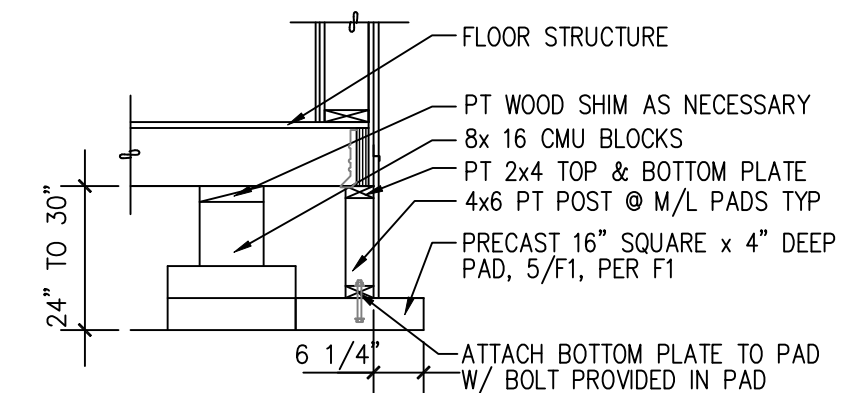
2 EXTERIOR WALL DETAIL
Scale: 1/2" = 1'-0"



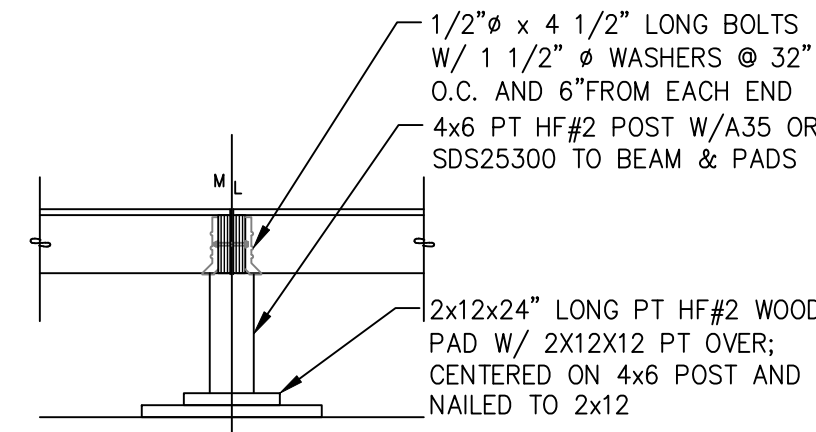
3 OPTIONAL CORNER DETAIL
Scale: 1/2" = 1'-0"



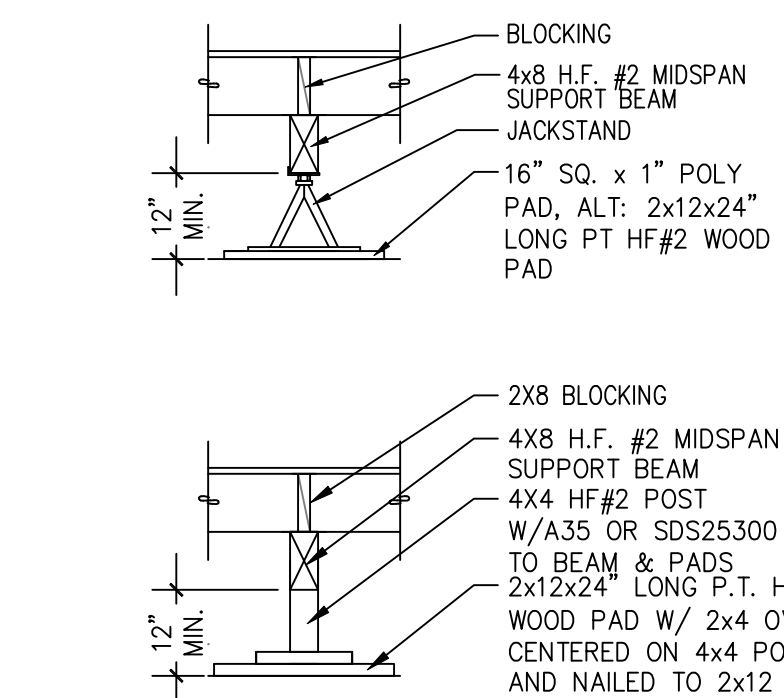
4 ANCHOR DETAIL
Scale: 1/2" = 1'-0"



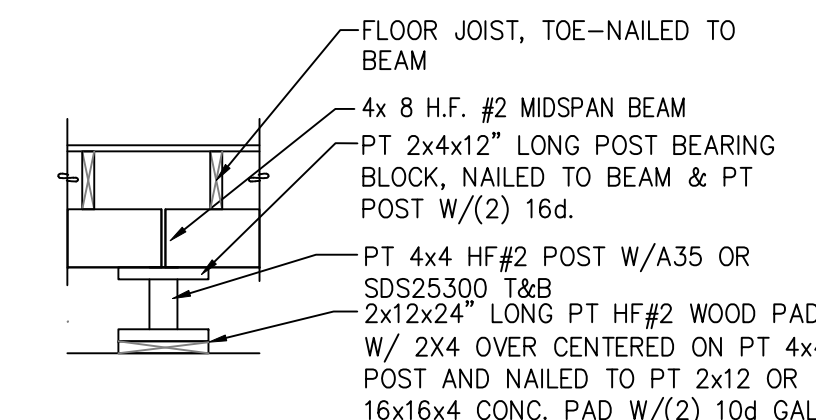
5 M/L EXT.COL.SUPPORT
Scale: 1/2" = 1'-0"



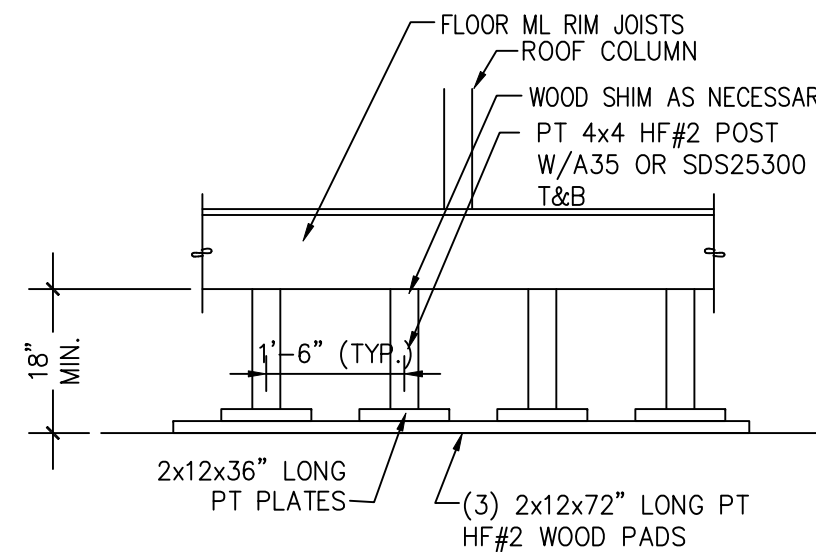
6 M/L SUPPORT, STANDARD
Scale: 1/2" = 1'-0"



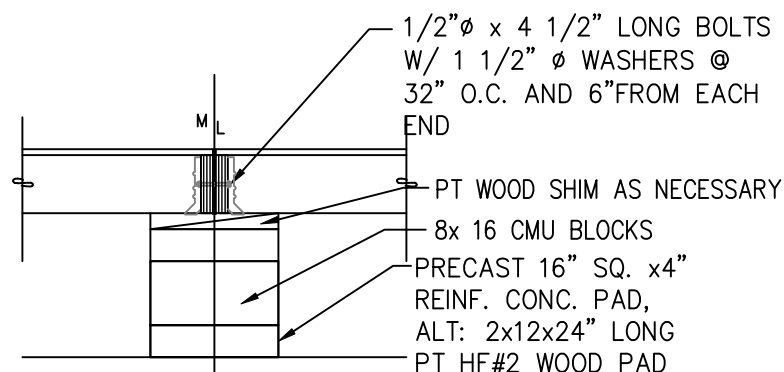
7 MID-SPAN SUPPORT, STANDARD
Scale: 1/2" = 1'-0"



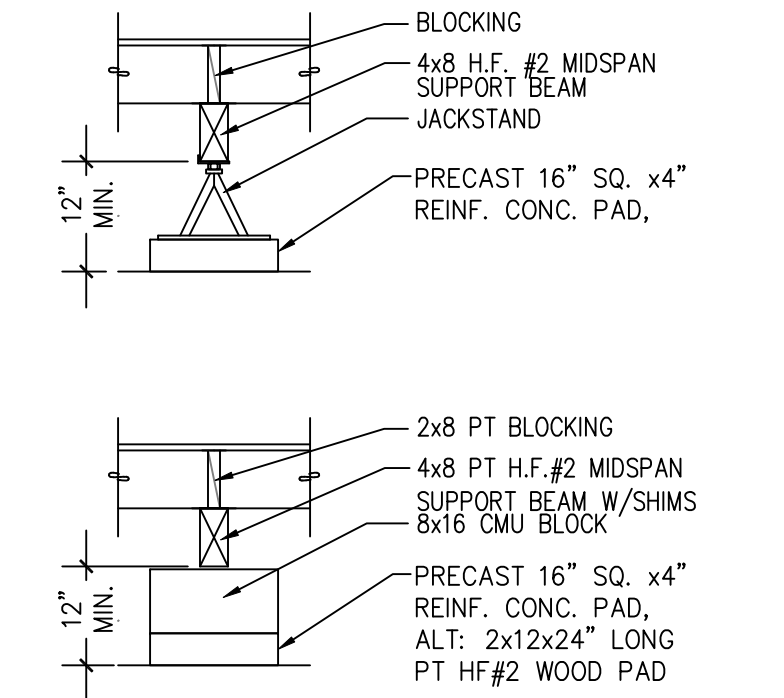
8 MID-SPAN BEAM SPLICE
Scale: 1/2" = 1'-0"



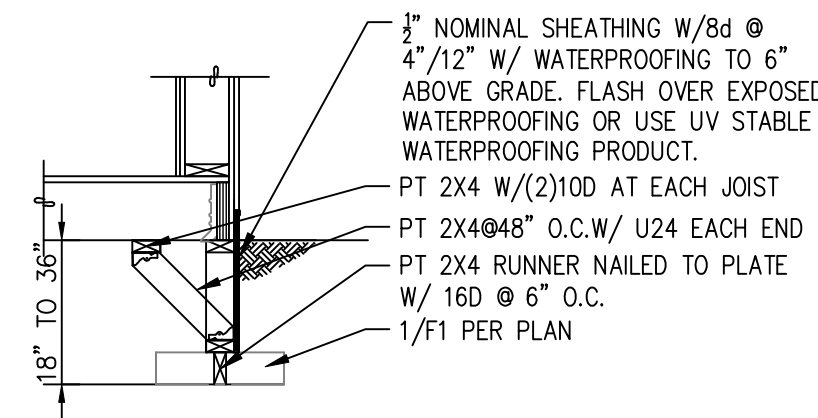
10 M/L POST SUPPORT, STANDARD
Scale: 1/2" = 1'-0"



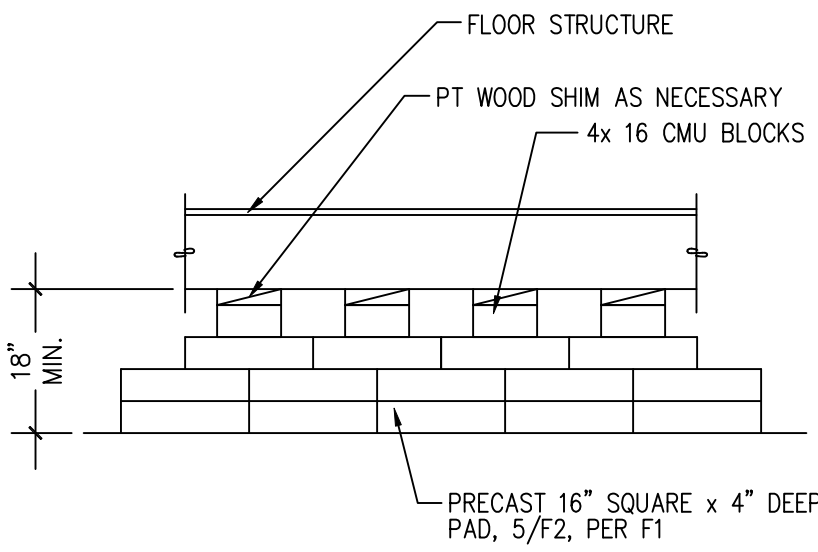
6A M/L SUPPORT, OPTIONAL
Scale: 1/2" = 1'-0"



7A MID-SPAN SUPPORT, OPTIONAL
Scale: 1/2" = 1'-0"

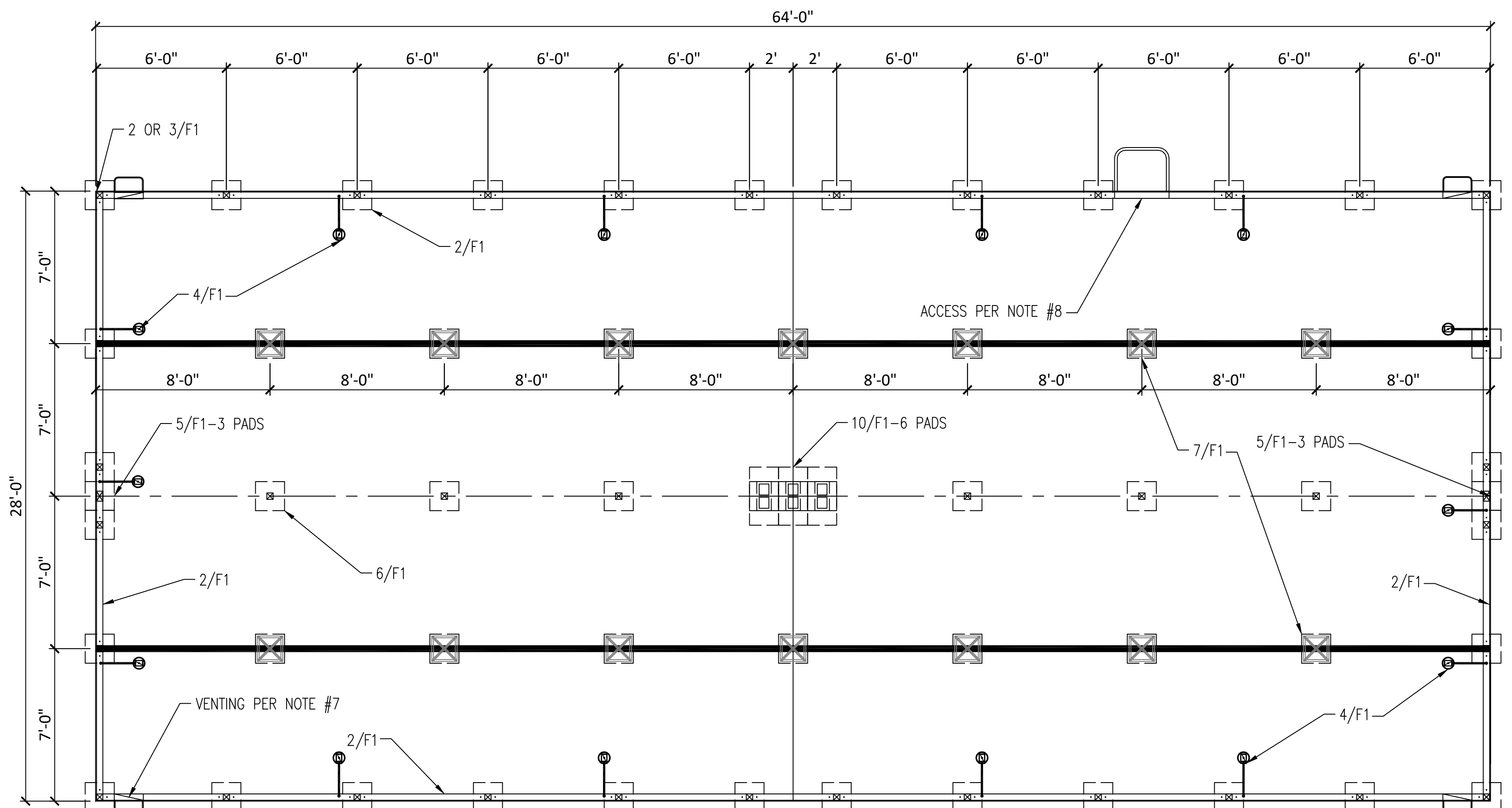


9 BACKFILLED WALL DETAIL
Scale: 1/2" = 1'-0"



10A M/L POST SUPPORT, OPTIONAL
Scale: 1/2" = 1'-0"

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1 FOUNDATION PLAN
Scale: 1/4" = 1'-0"

STRUCTURAL NOTES: CLASSROOM

- GENERAL:**
 - MODULAR BUILDING MAY VARY BY MANUFACTURER. VERIFY DIMENSIONS AND OTHER CHARACTERISTICS PRIOR TO BEGIN OF FOUNDATION INSTALLATION. MINOR VARIATIONS OF DIMENSION DO NOT CHANGE THE FOUNDATION DESIGN AND INSTALLATION REQUIREMENTS. MODULAR BUILDING DESIGN CRITERIA ARE ESTABLISHED FOR GENERAL WORST CASE IN LARGE REGIONS. THESE FOUNDATION PLANS ARE DESIGNED FOR SMALLER MORE SPECIFIC DESIGN AREAS AND MAY NOT MATCH THE BUILDING DESIGN CRITERIA. MATCH THE FOUNDATION TO THE SPECIFIC SITE. BUILDING DESIGN MAY MATCH OR EXCEED FOUNDATION DESIGN CRITERIA.
- DESIGN INFORMATION & LOADING:**
 - BUILDING CODE: IBC, 2015/2018, OSSC2019
 - RISK CATEGORY: II
 - ROOF LIVE LOAD: 25PSF, SNOW
 - FLOOR LIVE LOAD: 40 PSF OR 1,000# CONC.
 - WIND CRITERION: 110 MPH, EXP B, Kzt=1.0
 - SEISMIC CRITERION: Sds = 0.756, Is=1.0, CATEGORY D
 - SOIL BEARING: 1,500 PSF, SITE CLASS D
- CONCRETE:**
 - DESIGN COMP-STRENGTH: 2,500 PSI
 - REINFORCING BAR YIELD: 60 KSI
- MASONRY:**
 - 8x16x8 UNITS
 - SET UNITS W/CORES VERTICAL & NO MORE THAN 3 HIGH, PER PLAN
- WOOD:**
 - ALL WOOD MEMBERS OF THE FOUNDATION SYSTEM SHALL BE SPF-STD OR BETTER, UNLESS NOTED OTHERWISE.
 - ALL WOOD IN CONTACT OR WITHIN 8-INCHES WITH SOIL SHALL BE PRESERVATIVE TREATED.
 - CONNECTORS USED IN PRESERVATIVE TREATED WOOD MEMBERS SHALL BE STAINLESS STEEL OR HOT-DIPPED GALVANIZED TO THE GALVANIZING WEIGHT AS SPECIFIED IN IN ASTM A 153.
 - SKIRTING IS NOT INTENDED TO BE A 'SHEAR WALL', RATHER A SKIN FOR ENCLOSURE OF THE CRAWLSPACE.
 - PROVIDE 18" MIN. CLEARANCE FROM SOIL TO UNDERSIDE OF ANY UNTREATED WOOD MEMBER.
- SPECIALTY ITEMS: 'MINUTEMAN' OR EQUAL, www.minutemanproducts.com**
 - METAL PIERS TO BE CAPABLE OF SUPPORTING 6,000#
 - SOIL ANCHORS SHALL BE "MINUTEMAN" IN CONFORMANCE WITH THE TYPE SPECIFIED BY THE MANUFACTURER FOR THE SITE SPECIFIC SOILS AND SHALL CONFORM TO THE FOLLOWING:
 - DESIGN WORKING STRESS LOAD OF 3,150# W/ AN ULTIMATE STRENGTH LOAD OF 4,725#
 - INSTALL GROUND PORTION OF THE ANCHOR PRIOR TO SETTING THE BUILDING.
 - CONNECT ANCHOR TIES TO BUILDING ONLY AFTER BUILDING IS FULLY BLOCKED AND LEVELED.
 - ANCHORS TO BE ONE OF THE FOLLOWING:
 - SOIL CLASS 1 (ROCK): 36-XDH
 - SOIL CLASS 2 (ASPHALT W/GRAVEL BASE OR GRANULAR STRUCTURAL FILL, 24" MIN. DEPTH): (2) 36-XDH W/"MMASD2A" STABILIZER PLATE.
 - SOIL CLASS 3 (LOOSE SANDS & GRAVELS, STIFF SILTS & CLAYS): 4430-DH 3/4 AUGAR-ANCHOR SET VERTICAL W/"MMASD2A" STABILIZER PLATE INSTALL.
 - SOIL CLASS 4 (LOOSE SANDS, FIRM CLAYS AND SILTS, ALLUVIAL FILLS): 4636-DH 3/4 AUGER
- ANCHOR SET VERTICAL W/MMASD2 STABILIZER PLATE.
- INSTALL ALL SPECIALTY ITEMS PER THE MANUFACTURER'S RECOMMENDATIONS.
- VENTING:**
 - INSTALL A CLASS I VAPOR RETARDER OVER THE CRAWLSPACE AREA TO EXTERIOR OF BUILDING.
 - PROVIDE CRAWL SPACE VENTILATION PER IBC CODE AND LOCAL REQUIREMENTS AT 1 NET SF OF VENTILATION PER 1500 SF OF FLOOR AREA.
- ACCESS:**
 - PROVIDE ACCESS TO THE UNDER FLOOR AREA PER THE IBC CODE.
 - PROVIDE 18" MIN. CLEARANCE UNDER FROM SOIL TO UNDERSIDE OF ALL BUILDING STRUCTURE.
- SITE CONDITIONS:**
 - FOUNDATION SUBGRADE TO BE 4-INCHES OF ROAD-MIX GRAVEL, STRUCTURAL FILL OVER UNDISTURBED NATIVE SOILS OR STRUCTURAL FILL.
 - STRUCTURAL FILL TO BE COMPACTED TO 95% OF THE STANDARD PROCTOR DENSITY PER ASTM D-698.
 - SLOPE FINISHED GRADE AWAY FROM THE BUILDING FOUNDATION AT A MIN. GRADE OF 2%.
- SPECIAL STRUCTURAL INSPECTION (IBC CHAPTER 17):**
 - NO SPECIAL STRUCTURAL INSPECTION IS REQUIRED



Pacific Mobile
Mobile & Modular Buildings

BRIGGS ENGINEERING, INC.
REGISTERED PROFESSIONAL ENGINEER
ENGINEERS PLANNERS SUPERVISORS
PO BOX 108571 OAKLAND CITY, OR 97141-0857
PHONE: 503.251.1234 FAX: 503.251.1235
WWW.BRIGGS-ENGINEERING.COM

KCDA STYLE BUILDING
28'x64' MODULAR CLASSROOM
25 PSF-RL, 110C-WILL
SHEARWALL FOUNDATION
PLAN - ELEVATION - NOTES
SCALE: AS SHOWN
DWG NO.: 190101-01-4-2-17
DWG DATE: FEBRUARY 2019
REVISION DATE: 12/6/2019
F1
SHEET: 1 OF 1
PMSI-JOSEPH MANGAN

PRE-FABRICATED BUILDING DESIGN - FOUNDATION CALCULATIONS				IBC-2015, WBC, OSSC	
CLIENT	Pacific Mobile Structures, Inc		OWNER:	Pacific Mobile Structures, Inc	
DATE:	10-Dec-19	EST./PO#	E19246	LOCATION:	KCDA Standards
PROJECT#	201901	01.01.1		STATE:	ID-OR-WA PNW

Table of ContentsPREFABRICATED MODULAR BUILDING PAD FOUNDATION DESIGN

	DESCRIPTION	WIDTH:	LENGTH:	TYPE:
WEST				
	28x64 MODULAR FDN-Classroom w/(2) Floor Joist Spans /Module, W/ & W/O Firewall	28	64	25psf-RLL, 40psf-FLL, 110mph, Exp C, Cat-D, Ss=1.5, Fp=1500 psf
EAST				
	28x64 MODULAR FDN-Classroom w/(2) Floor Joist Spans /Module, W/ & W/O Firewall	28	64	40psf-RLL, 40psf-FLL, 115mph, Exp C, Cat-D, Ss=1.5, Fp=1500 psf



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MODULAR BUILDING PAD & PIER FOUNDATION DESIGN - FOUNDATION CALCULATIONS

IBC-2015, WBC, OSSC

CLIENT	Pacific Mobile Structures, Inc	DEALER:	Pacific Mobile Structures, Inc	Criteria	25psf-RLL, 40psf-FLL, 110mph, Exp C, Cat-D, Ss=1.5, Fp=1500 psf	
Date:	10-Dec-19	PO#	E19246	Location:	KCDA Standards	
Project #:	201901	#01.3.03 & 04-1	28x64 MODULAR FDN-Classroom w/(2) Floor Joist Spans /Module, W/ & W/O Firewall		State(s):	ID-OR-WA PNW

I. DESIGN CRITERIA: 28x64 MODULAR FDN-Classroom w/(2) Floor Joist Spans /Module, W/ & W/O Firewall

Dead Load:	Roof, RDL =		10	psf	
	1st Floor Ceiling CDL =		1		
E&M =			1		
	Floor, FDL =		10	psf	
Wall, WDL =			9	psf	
	Snow Load, RLL =		25	psf	
Roof Live Load:	Load Duration Factor, Cd =		1.15	%	
	Uniform Floor Load, FLL =	Classroom	40	psf	IBC Table 1607.1
Floor Load:	Concentrated Live Load, p =		1000	lbs.	IBC Table 1607.1
	Partion, PDL =		0	psf	
Building Risk Classification:	Category		II		ASCE 7 Table 1.5-1
	Wind Importance Factor, Iw =		1.00		ASCE 7 Table 1.5-1
Wind Directional Factor, Kd			0.85		ASCE 7 Table 26.6-1
	"a" Edge Pressure Distance =		3.00	ft	
Roof Slope =	2:12 =		9.46	Degrees	
	Edge Wind Pressure, Wep =		21.6	psf	ASCE 7 Figure 28.6-1
Interior Wind Pressure, Wip =			14.4	psf	ASCE 7 Figure 28.6-1
	Average Wind Pressure, Wp =		15.94	psf	ASCE 7 Figure 28.6-1
Exposure Category =	C	Exposure Factor, λ =	1.21		ASCE 7 Figure 28.6-1
	Wind Topographic Factor, Kz =		1.00		ASCE 7 Section 6.5
Design Wind Pressure, Pw = Wp*λ*Iw*Kz =			16.4	psf	IBC Section 1605.3.1
	Average Uplift Wind Pressure, Wup =		-19.6	psf	
Upper Module Weight =			0.00	psf	
	Base Module Weight =		27.79	psf	
Total Weight, Wtot =			27.79	psf	
	Snow Load % Used in Seismic Design =		0%		
Soil Site Class			D		
	Seismic Category =		D	PNW	IBC Table 1613.3(1)
Mapped Spectral Accelerations, short periods, Ss =			1.5000		IBC Figure 1615
	Site Coefficient, Fa =		1.00		IBC Table 1615.1.2(1)
Max. Spectral Response, SMS = Fa*Ss =			1.50		IBC Equation 16-16
	Design Spectral Response, SDS = 2/3*SMS =		1.00		IBC Equation 16-18
Response Modification Coefficient, R =			4.00		IBC Table 1617.6
	Lateral Load Factor, F = (1, Single Story; 1.1, 2-story; 1.2, 3-story)		1		ASCE 7-05, 12.14.8.1
Total Shear, pst = F*SDS*Wtot/R =			6.95	psf	ASCE 7-05 Equation 12.14.11
	Nominal Module Length, ML =		64	ft.	
Nominal Module Width, MW =			14.00	ft.	
	Width, W = # Units =	2	28.00	ft.	
Legnth, L = # Units =		1	64.00	ft.	
	1st Floor Wall Ht. =		9.00	ft.	
2nd Flr. Wall Height, Wht =			0.00	ft.	
	Roof Height, Rht = 2:12 Slope		2.33	ft.	
Floor Height above NG, Fht =	30	inches	2.50	ft	
	Building Ht Coeff, Htc = Rht+Wht+Fht-10		1.00		
No. of floor spans per module, nfs =			2		
	Clear Distance between supports, L2a =		84.00	inches	

MODULAR BUILDING PAD & PIER FOUNDATION DESIGN - FOUNDATION CALCULATIONS

IBC-2015, WBC, OSSC

CLIENT	Pacific Mobile Structures, Inc	DEALER:	Pacific Mobile Structures, Inc	Criteria	25psf-RLL, 40psf-FLL, 110mph, Exp C, Cat-D, Ss=1.5, Fp=1500 psf	
Date:	10-Dec-19	PO#	E19246	Location:	KCDA Standards	
Project #:	201901	#01.3.03 & 04-1	28x64 MODULAR FDN-Classroom w/(2) Floor Joist Spans /Module, W/ & W/O Firewall			State(s): ID-OR-WA PNW

II. FOUNDATION DESIGN**A. Foundation Components**

Option A	Individual Bearing Pads - Bearing Pads	Column Pads
	Width, wbp =	16 inches
	Length, lbp =	16 inches
	Surface Support Depth: Conc, Asph & Base	4 inches, Required
	Equivalent Bearing Area at Soil, BA =	400 Sq. Inches
IBC-T.18.4.2	Allowable Soil Bearing Pressure, [Class 4] Q =	1500 psf.
Option B	Perimeter Support Width	0 inches
	Allowable Load, Pbp = (BA)/144*Q =	4167 pounds
	Anchors: 'Minuteman' MMA-92 Auger Anchor OR Double MMA-35 w/MMA-SD2 Stabilizer Plate in Soil or SD2A in Asphalt or Compacted Gravel	
	Ultimate Anchor Capacity, Anchc =	4725 lbs.

B. Exterior Pads (Around Perimeter)**Floor and Roof Loads:**

	Exterior Pads Required, Epr =	1 pad	
	Allowable Load, Pfla =	4167 lbs.	From Computer Calculations, max. span
	Perimeter Support Bearing Pressure, (Skirting)	0 psf - OK!	
Classroom	Exterior Uniform Floor Load,	538 plf	7.76 ft.
Classroom	Use:	Perimeter Pads W/ (12) 16-inch x 16-inch pad @ 6-ft o.c. exterior supports.	

C. Interior Pads (Floor Loads Only - Mateline Supports)**Floor Loads:**

	Interior Pads Required, lpr =	1 pad	From Computer Calculations, max. span
	Allowable Load, Pfla =	4167 lbs.	
Classroom	Interior Uniform Floor Load,	350 plf	11.90 ft.
Classroom	Use:	(9) 16-inch x 16-inch Pads @ 8-ft o.c. interior supports.	

D. Column Pads (Roof Loads Only)**Roof Loads:**

Column Pads Required, Cpr =	1 pads
Allowable Load, Prla =	4000 lbs.
Mateline Roof Beams Uniform Roof Load,mbrl = (RLL+RDL)*MW =	518 lb/ft.
Effective Mateline Beam Span, Mps = Pfla/mbrl =	7.72 ft.
Use:	(1) 16-inch x 16-inch pads for every 7.72-ft effective Mateline Beam Span.

Effective Interior Roof Beam Span =

32 ft

5 PADS REQ'D

Effective Interior Roof Beam Span =

16 ft

3 PADS REQ'D

MODULAR BUILDING PAD & PIER FOUNDATION DESIGN - FOUNDATION CALCULATIONS						IBC-2015, WBC, OSSC	
CLIENT	Pacific Mobile Structures, Inc	DEALER: Pacific Mobile Structures, Inc			Criteria	25psf-RLL,40psf-FLL,110mph, Exp C, Cat-D, Ss=1.5, Fp=1500 psf	
Date:	10-Dec-19	PO# E19246		Location: KCDA Standards			
Project #:	201901	#01.3.03 & 04-1	28x64 MODULAR FDN-Classroom w/(2) Floor Joist Spans /Module, W/ & W/O Firewall		State(s):	ID-OR-WA	PNW

E. Lateral Design**1. Longitudinal Walls (Front & Back, Long Walls)**

Unit Wind Load, UWL = $(W_{ht} + R_{ht} + F_{ht}/2) * W_p * L =$ 13205 lbs Governs
 Unit Seismic Load, USL = $W * p_{st} =$ 12454 lbs
 Building Weight = 35840 lbs
 % Building Weight Used for Lateral Sliding

0%

 Transverse Foundation Friction Factor =

0.40

 Gravity Resistance, GR = Building WT * Friction Factor = 0 lbs.
 OTM = Lateral Load * $w_{ht}/2 + \text{Uplift}$ 94610 Ft-lbs
 RM = $0.6 * \text{Building } W_t * W/2$ 301056 Ft-lbs
 Factor of Safety = RM/OTM 3 No Uplift Anchors Required
 Use: (4) 'Minuteman' MMA-92 Auger Anchor OR Double MMA-35 w/MMA-SD2 Stabilizer
 Plate in Soil or SD2A in Asphalt or Compacted Gravel

2. Lateral Walls (End, Short Walls)

Unit Wind Load, UWL = $(W_{ht} + R_{ht}/2 + F_{ht}/2) * W_p =$ 5242 lbs
 Unit Seismic Lateral Load, USLL = $L * p_{st} =$ 12454 lbs Governs
 % Building Weight Used for Longitudinal Sliding

0%

 Longitudinal Foundation Friction Factor =

0.40

 Gravity Resistance, GR = Building WT * Friction Factor = 0 lbs.
 OTM = Lateral Load * $w_{ht}/2 + \text{Uplift}$ 91231 Ft-lbs
 RM = $0.6 * \text{Building } W_t * W/2$ 688128 Ft-lbs
 Factor of Safety = RM/OTM 8 No Uplift Anchors Required
 Use: (3) 'Minuteman' MMA-92 Auger Anchor OR Double MMA-35 w/MMA-SD2 Stabilizer
 Plate in Soil or SD2A in Asphalt or Compacted Gravel

MODULAR BUILDING PAD & PIER FOUNDATION DESIGN - FOUNDATION CALCULATIONS

IBC-2015, WBC, OSSC

CLIENT	Pacific Mobile Structures, Inc	DEALER:	Pacific Mobile Structures, Inc	Criteria	40psf-RLL, 40psf-FLL, 115mph, Exp C, Cat-D, Ss=1.5, Fp=1500 psf
Date:	10-Dec-19	PO#	E19246	Location:	KCDA Standards
Project #:	201901	#01.3.05 & 06-1	28x64 MODULAR FDN-Classroom w/(2) Floor Joist Spans /Module, W/ & W/O Firewall		
			State(s):	ID-OR-WA	PNW

I. DESIGN CRITERIA: 28x64 MODULAR FDN-Classroom w/(2) Floor Joist Spans /Module, W/ & W/O Firewall

Dead Load:	Roof, RDL =		10	psf	
	1st Floor Ceiling CDL =		1		
	E&M =		1		
	Floor, FDL =		10	psf	
	Wall, WDL =		9	psf	
Roof Live Load:	Snow Load, RLL =		40	psf	
	Load Duration Factor, Cd =		1.15	%	
Floor Load:	Uniform Floor Load, FLL =	Classroom	40	psf	IBC Table 1607.1
	Concentrated Live Load, p =		1000	lbs.	IBC Table 1607.1
	Partion, PDL =		0	psf	
Wind Load:	Basic Wind Speed, V =		115	mph	ASCE 7 Figure 26.5-1A
	Building Risk Classification:	Category	II		ASCE 7 Table 1.5-1
	Wind Directional Factor, Kd		0.85		ASCE 7 Table 26.6-1
	"a" Edge Pressure Distance =		3.00	ft	
2	Roof Slope =	2:12	9.46	Degrees	
	Edge Wind Pressure, Wep =		23.7	psf	ASCE 7 Figure 28.6-1
	Interior Wind Pressure, Wip =		15.75	psf	ASCE 7 Figure 28.6-1
	Average Wind Pressure, Wp =		17.45	psf	ASCE 7 Figure 28.6-1
	Exposure Category =	C	Exposure Factor, λ =	1.21	ASCE 7 Figure 28.6-1
	Wind Topographic Factor, Kz =		1.00		ASCE 7 Section 6.5
	Design Wind Pressure, Pw = Wp*λ*lw*Kz =		18.0	psf	IBC Section 1605.3.1
	Average Uplift Wind Pressure, Wup =		-21.5	psf	
Seismic:	Upper Module Weight =		0.00	psf	
	Base Module Weight =		27.79	psf	
	Total Weight, Wtot =		27.79	psf	
	Snow Load % Used in Seismic Design =		20%		
	Soil Site Class		D		
	Seismic Category =		D	PNW	IBC Table 1613.3(1)
	Mapped Spectral Accelerations, short periods, Ss =		1.5000		IBC Figure 1615
	Site Coefficient, Fa =		1.00		IBC Table 1615.1.2(1)
	Max. Spectral Response, SMS = Fa*Ss =		1.50		IBC Equation 16-16
	Design Spectral Response, SDS = 2/3*SMS =		1.00		IBC Equation 16-18
	Response Modification Coefficient, R =		4.00		IBC Table 1617.6
	Lateral Load Factor, F = (1, Single Story; 1.1, 2-story; 1.2, 3-story)		1		ASCE 7-05, 12.14.8.1
	Total Shear, pst = F*SDS*Wtot/R =		8.95	psf	ASCE 7-05 Equation 12.14.11
Dimensions:	Nominal Module Length, ML =		64	ft.	
	Nominal Module Width, MW =		14.00	ft.	
	Width, W =	# Units = 2	28.00	ft.	
	Legnth, L =	# Units = 1	64.00	ft.	
	1st Floor Wall Ht. =		9.00	ft.	
	2nd Flr. Wall Height, Wht =		0.00	ft.	
	Roof Height, Rht =	2:12 Slope	2.33	ft.	
	Floor Height above NG, Fht =	30	2.50	ft	
	Building Ht Coeff, Htc = Rht+Wht+Fht-10		1.00		
	No. of floor spans per module, nfs =		2		
	Clear Distance between supports, L2a =		84.00	inches	

MODULAR BUILDING PAD & PIER FOUNDATION DESIGN - FOUNDATION CALCULATIONS

IBC-2015, WBC, OSSC

CLIENT	Pacific Mobile Structures, Inc	DEALER:	Pacific Mobile Structures, Inc	Criteria	40psf-RLL, 40psf-FLL, 115mph, Exp C, Cat-D, Ss=1.5, Fp=1500 psf
Date:	10-Dec-19	PO#	E19246	Location:	KCDA Standards
Project #:	201901	#01.3.05 & 06-1	28x64 MODULAR FDN-Classroom w/(2) Floor Joist Spans /Module, W/ & W/O Firewall		
			State(s):	ID-OR-WA	PNW

II. FOUNDATION DESIGN**A. Foundation Components**

Option A	Individual Bearing Pads - Bearing Pads	Column Pads
	Width, wbp =	16 inches
	Length, lbp =	16 inches
	Surface Support Depth: Conc, Asph & Base	4 inches, Required
	Equivalent Bearing Area at Soil, BA =	400 Sq. Inches
IBC-T.18.4.2	Allowable Soil Bearing Pressure, [Class 4] Q =	1500 psf.
Option B	Perimeter Support Width	0 inches
	Allowable Load, Pbp = (BA)/144*Q =	4167 pounds
	Anchors: 'Minuteman' MMA-92 Auger Anchor OR Double MMA-35 w/MMA-SD2 Stabilizer Plate in Soil or SD2A in Asphalt or Compacted Gravel	
	Ultimate Anchor Capacity, Anchc =	4725 lbs.

B. Exterior Pads (Around Perimeter)**Floor and Roof Loads:**

	Exterior Pads Required, Epr =	1 pad	
	Allowable Load, Pfla =	4167 lbs.	From Computer Calculations, max. span
	Perimeter Support Bearing Pressure, (Skirting)	0 psf - OK!	
Classroom	Exterior Uniform Floor Load,	643 plf	6.49 ft.
Classroom	Use:	Perimeter Pads W/ (12) 16-inch x 16-inch pad @ 6-ft o.c. exterior supports.	

C. Interior Pads (Floor Loads Only - Mateline Supports)**Floor Loads:**

	Interior Pads Required, lpr =	1 pad	From Computer Calculations, max. span
	Allowable Load, Pfla =	4167 lbs.	
Classroom	Interior Uniform Floor Load,	350 plf	11.90 ft.
Classroom	Use:	(9) 16-inch x 16-inch Pads @ 8-ft o.c. interior supports.	

D. Column Pads (Roof Loads Only)**Roof Loads:**

Column Pads Required, Cpr =	1 pads
Allowable Load, Prla =	4000 lbs.
Mateline Roof Beams Uniform Roof Load,mbrl = (RLL+RDL)*MW =	728 lb/ft.
Effective Mateline Beam Span, Mps = Pfla/mbrl =	5.49 ft.
Use:	(1) 16-inch x 16-inch pads for every 5.49-ft effective Mateline Beam Span.

Effective Interior Roof Beam Span =

32 ft

6 PADS REQ'D

Effective Interior Roof Beam Span =

16 ft

3 PADS REQ'D

MODULAR BUILDING PAD & PIER FOUNDATION DESIGN - FOUNDATION CALCULATIONS						IBC-2015, WBC, OSSC	
CLIENT	Pacific Mobile Structures, Inc	DEALER: Pacific Mobile Structures, Inc			Criteria	40psf-RLL,40psf-FLL,115mph, Exp C, Cat-D, Ss=1.5, Fp=1500 psf	
Date:	10-Dec-19	PO# E19246		Location: KCDA Standards			
Project #:	201901	#01.3.05 & 06-1	28x64 MODULAR FDN-Classroom w/(2) Floor Joist Spans /Module, W/ & W/O Firewall		State(s):	ID-OR-WA	PNW

E. Lateral Design**1. Longitudinal Walls (Front & Back, Long Walls)**

Unit Wind Load, UWL = $(W_{ht} + R_{ht} + F_{ht}/2) * W_p * L =$ 14457 lbs
 Unit Seismic Load, USL = $W * p_{st} =$ 16040 lbs Governs
 Building Weight = 35840 lbs
 % Building Weight Used for Lateral Sliding

0%

 Transverse Foundation Friction Factor =

0.40

 Gravity Resistance, GR = Building WT * Friction Factor = 0 lbs.
 OTM = Lateral Load * $w_{ht}/2 + \text{Uplift}$ 110642 Ft-lbs
 RM = $0.6 * \text{Building } W_t * W/2$ 301056 Ft-lbs
 Factor of Safety = RM/OTM 3 No Uplift Anchors Required
Use: (5) 'Minuteman' MMA-92 Auger Anchor OR Double MMA-35 w/MMA-SD2 Stabilizer Plate in Soil or SD2A in Asphalt or Compacted Gravel

2. Lateral Walls (End, Short Walls)

Unit Wind Load, UWL = $(W_{ht} + R_{ht}/2 + F_{ht}/2) * W_p =$ 5738 lbs
 Unit Seismic Lateral Load, USLL = $L * p_{st} =$ 16040 lbs Governs
 % Building Weight Used for Longitudinal Sliding

0%

 Longitudinal Foundation Friction Factor =

0.40

 Gravity Resistance, GR = Building WT * Friction Factor = 0 lbs.
 OTM = Lateral Load * $w_{ht}/2 + \text{Uplift}$ 110642 Ft-lbs
 RM = $0.6 * \text{Building } W_t * W/2$ 688128 Ft-lbs
 Factor of Safety = RM/OTM 6 No Uplift Anchors Required
Use: (4) 'Minuteman' MMA-92 Auger Anchor OR Double MMA-35 w/MMA-SD2 Stabilizer Plate in Soil or SD2A in Asphalt or Compacted Gravel

WELCOME RAMP, INC.

STRUCTURAL ANALYSIS

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WELCOME RAMP, INC.

STRUCTURAL ANALYSIS

Ramp System Design Criteria and Analysis

- 1) Reference Design Criteria:
 - a) International Building Code, 2012 & 2015 Editions
 - b) ANSI A 117.1, 2009 Edition
- 2) Site Specific Criteria:
 - a) Building Occupancy Classifications: II
 - b) Vertical Loading: 100 psf for Landings, 300 lbs. concentrated loads for steps
 - c) Horizontal Loading:
 - i) Wind Loads: 135 mph(ult), Exposure B, $K_z=0.85$, $K_{zt}=1.0$; Design Wind Pressure = 30 psf (At less than 15 feet above grade, IBC 2012, 1609.6.2)
 - ii) Seismic Loads: $S_{ds} = 1.00$, $S_1=0.50$, $I=1.0$, $R=3.25$, $\Omega_o=2$, $C_d=3.25$, $C_s=0.307$
 - d) Soil Bearing: 1,500 psf, Unless verified by Geotechnical Report or Building Official
- 3) Material Specifications:
 - a) Aluminum:
 - i) Handrail ASTM 6063-T5, 16 ksi, minimum yield strength
 - ii) Structural ASTM 6061-T5, 35 ksi, minimum yield strength
 - b) Density 170 lbs. per cubic foot
- 4) Connectors:
 - a) Bolts Grade 5 zinc-coated (Design), ASTM A-325 may be substituted.
 - b) Screws #10x1.25" zinc plated Self-Tapping Screw (STS)
 - c) Welding Per AWS D1.2 and size as shown on the drawings
 - d) Sleeves Length of snug-fitting sleeves designed resist moment and shear of sleeved connection.
- 5) Design Basis:
 - a) Each side of the assembly is a framed made rigid by either welding or assembling parts together in sleeves to resist movement. Base connections are a pinned condition.
 - b) Each frame is connected together with landing or ramp frames and planking to distribute dead and live loads to the frames. Railing is added to the frame assembly.
 - c) Landing Platforms are attached to buildings with Lag-bolts or SDS Screws.
 - d) Basic Dead Load is 5 psf for frame, ramp & landing surfaces. 2 psf is added for railing.

- e) A 300 lb. lateral load is used in the design to simulate seismic, wind and pedestrian lateral loading for each frame (2 frames per unit, 600# per assembly). This results in an effective Design Cs for a 30-foot ramp and 5x10 platform of 0.5 and a design wind load of 30 psf without consideration for stress duration. Seismic and wind loads do not govern lateral loading for standard configurations. For those configurations having landings attached a building on one side longer than 40', soil anchors shall be installed at the rate of (1) anchor for each length of landing 40' longer than 40'. For those configurations having landings attached to a building on two sides longer than 60', soil anchors shall be installed at the rate of (1) anchor for each length of landing 60' longer than 60'. See Typical Soil Anchor Detail.

WELCOME RAMP, INC.

STRUCTURAL ANALYSIS

Ramp System Design

Member Data

Member Label	I Joint	J Joint	Rotate (degrees)	Shape / Section Set	Material Set	Phys Memb	End Releases I-End J-End AVM AVM	End Offsets I-End J-End (in) (in)	Inactive Code Length (ft)
M1	N1	N10		SEC1	AL	Y	PIN		4.768
M2	N10	N11		SEC1	AL	Y	PIN		4.768
M3	N11	N9		SEC1	AL	Y			4.768
M4	N9	N6		SEC1	AL	Y	PIN		5.012
M5	N6	N8		SEC2	AL	Y			5
M6	N7	N8		SEC3	AL	Y			1.599
M7	N5	N6		SEC3	AL	Y			1.599
M8	N4	N9		SEC3	AL	Y			1.25
M9	N3	N11		SEC3	AL	Y			.833
M10	N2	N10		SEC3	AL	Y			.417

Sections

Section Label	Database Shape	Material Label	Area (in) ²	SA (0,180)	SA (90,270)	I (90,270) (in ⁴)	I (0,180) (in ⁴)	T/C Only
SEC1	Welcome Ramp	AL	1.438	1.2	1.2	.421	2.02	
SEC2	Welcome Deck	AL	1.438	1.2	1.2	.421	1.378	
SEC3	TU2X2X2	AL	.897	1.2	1.2	.513	.513	

Basic Load Case Data

BLC No.	Basic Load Case Description	Category Code	Category Description	Gravity X Y	Load Type Totals Joint Point Direct Dist.
1	w1 - Dead Load	DL	Dead Load	-1	5
2	w2 -Pedestrian Load	LLS	Live Load Special (public as..	1	5

Member Direct Distributed Loads, Category : DL, BLC 1 : w1 - Dead Load

Member Label	Direction	Start Magnitude (k/ft, F)	End Magnitude (k/ft, F)	Start Location (ft or %)	End Location (ft or %)
M1	Y	-.014	-.014	0	0
M2	Y	-.014	-.014	0	0
M3	Y	-.014	-.014	0	0
M4	Y	-.014	-.014	0	0
M5	Y	-.018	-.018	0	0

Member Direct Distributed Loads, Category : LLS, BLC 2 : w2 -Pedestrian Load

Member Label	Direction	Start Magnitude (k/ft, F)	End Magnitude (k/ft, F)	Start Location (ft or %)	End Location (ft or %)
M1	Y	-.2	-.2	0	0
M2	Y	-.2	-.2	0	0
M3	Y	-.2	-.2	0	0
M4	Y	-.2	-.2	0	0
M5	Y	-.25	-.25	0	0

Load Combinations

Num	Description	Env	WS	PD	SRSS	CD	BLC	Factor	BLC	Factor	BLC	Factor	BLC	Factor
1	DL + Ped. Load	y				1	1	1	2	1				
2	Ped. Load Only	y				1	2	1						

Load Combinations (continued)

Num	Description	Env	WS	PD	SRSS	CD	BLC	Factor	BLC	Factor	BLC	Factor	BLC	Factor
3						1								
4						1								
5						1								

Envelope Member Stresses

Member Label	Section		Axial		Shear		Bending top		Bending bot	
			(ksi)	Lc	(ksi)	Lc	(ksi)	Lc	(ksi)	Lc
M1	1	max	.023	1	.319	1	0	1	0	1
		min	.022	2	.299	2	0	1	0	1
	2	max	.003	1	.036	1	4.933	1	-2.906	2
		min	.003	2	.034	2	4.625	2	-3.1	1
	3	max	-.017	2	-.23	2	2.009	1	-1.197	2
		min	-.018	1	-.247	1	1.906	2	-1.262	1
M2	4	max	-.036	2	-.494	2	-8.157	2	5.513	1
		min	-.039	1	-.53	1	-8.774	1	5.125	2
	1	max	.059	2	.531	1	-8.355	2	5.589	1
		min	.053	1	.497	2	-8.895	1	5.25	2
	2	max	.04	2	.248	1	1.928	1	-1.114	2
		min	.032	1	.232	2	1.773	2	-1.211	1
M3	3	max	.02	2	-.032	2	4.893	1	-2.864	2
		min	.011	1	-.035	1	4.558	2	-3.074	1
	4	max	.001	2	-.296	2	0	1	0	1
		min	-.009	1	-.318	1	0	1	0	1
	1	max	.2	1	.359	1	-2.64	2	1.752	1
		min	.199	2	.337	2	-2.789	1	1.659	2
M4	2	max	.18	2	.077	1	3.268	1	-1.91	2
		min	.18	1	.072	2	3.039	2	-2.053	1
	3	max	.16	2	-.192	2	1.467	1	-.864	2
		min	.159	1	-.206	1	1.375	2	-.922	1
	4	max	.141	2	-.456	2	-7.633	2	5.147	1
		min	.138	1	-.489	1	-8.192	1	4.796	2
M5	1	max	.029	1	.55	1	-8.455	2	5.68	1
		min	.026	2	.514	2	-9.04	1	5.313	2
	2	max	.012	1	.252	1	2.667	1	-1.564	2
		min	.01	2	.236	2	2.489	2	-1.676	1
	3	max	-.006	1	-.043	2	5.681	1	-3.334	2
		min	-.006	2	-.046	1	5.307	2	-3.569	1
M6	4	max	-.022	2	-.321	2	0	1	0	1
		min	-.023	1	-.343	1	0	1	0	1
	1	max	.152	1	.56	1	-5.456	2	6.538	1
		min	.141	2	.523	2	-5.832	1	6.116	2
	2	max	.152	1	.188	1	6.427	1	-6.715	2
		min	.141	2	.175	2	5.99	2	-7.205	1
M7	3	max	.152	1	-.173	2	6.464	1	-6.765	2
		min	.141	2	-.185	1	6.035	2	-7.246	1
	4	max	.152	1	-.52	2	-5.322	2	6.414	1
		min	.141	2	-.558	1	-5.721	1	5.966	2
	1	max	.745	1	.523	1	0	1	0	1
		min	.695	2	.487	2	0	1	0	1
M8	2	max	.745	1	.523	1	2.717	1	-2.527	2

Envelope Member Stresses, (continued)

Member Label	Section	Axial (ksi)		Shear (ksi)		Bending top (ksi)		Bending bot (ksi)	
		Lc		Lc		Lc		Lc	
M7	3	min	.695	2	.487	2	2.527	2	-2.717
		max	.745	1	.523	1	5.435	1	-5.055
		min	.695	2	.487	2	5.055	2	-5.435
	4	max	.745	1	.523	1	8.152	1	-7.582
		min	.695	2	.487	2	7.582	2	-8.152
	1	max	1.208	1	-.499	2	0	1	0
M8		min	1.129	2	-.533	1	0	1	0
	2	max	1.208	1	-.499	2	-2.591	2	2.77
		min	1.129	2	-.533	1	-2.77	1	2.591
	3	max	1.208	1	-.499	2	-5.182	2	5.54
		min	1.129	2	-.533	1	-5.54	1	5.182
	4	max	1.208	1	-.499	2	-7.774	2	8.31
		min	1.129	2	-.533	1	-8.31	1	7.774
	1	max	1.367	1	-.108	2	0	1	0
		min	1.275	2	-.112	1	0	1	0
	2	max	1.367	1	-.108	2	-.44	2	.454
		min	1.275	2	-.112	1	-.454	1	.44
	3	max	1.367	1	-.108	2	-.879	2	.907
M9		min	1.275	2	-.112	1	-.907	1	.879
	4	max	1.367	1	-.108	2	-1.319	2	1.361
		min	1.275	2	-.112	1	-1.361	1	1.319
	1	max	.93	1	-.521	2	0	1	0
		min	.87	2	-.55	1	0	1	0
	2	max	.93	1	-.521	2	-1.411	2	1.49
		min	.87	2	-.55	1	-1.49	1	1.411
	3	max	.93	1	-.521	2	-2.822	2	2.98
		min	.87	2	-.55	1	-2.98	1	2.822
	4	max	.93	1	-.521	2	-4.233	2	4.471
		min	.87	2	-.55	1	-4.471	1	4.233
	1	max	1.424	1	-.048	2	0	1	0
M10		min	1.332	2	-.078	1	0	1	0
	2	max	1.424	1	-.048	2	-.065	1	.106
		min	1.332	2	-.078	1	-.106	2	.065
	3	max	1.424	1	-.048	2	-.129	1	.212
		min	1.332	2	-.078	1	-.212	2	.129
	4	max	1.424	1	-.048	2	-.194	1	.318
		min	1.332	2	-.078	1	-.318	2	.194

Envelope Member Section Forces

Member Label	Section	Axial (k)		Shear (k)		Moment (k)	
		Lc		Lc		Lc	
M1	1	max	.034	1	.382	1	0
		min	.031	2	.358	2	0
	2	max	.004	1	.043	1	-.317
		min	.004	2	.041	2	-.338
	3	max	-.024	2	-.276	2	-.131
		min	-.026	1	-.296	1	-.138
	4	max	-.052	2	-.592	2	.601
		min	-.056	1	-.634	1	.559
	1	max	.085	2	.636	1	.61
		min	.076	1	.595	2	.573
M2	2	max	.057	2	.297	1	-.122

Envelope Member Section Forces, (continued)

Member Label	Section	Axial (k)	Lc	Shear (k)	Lc	Moment (k)	Lc
M3	min	.046	1	.278	2	-.132	1
	3 max	.029	2	-.038	2	-.312	2
	min	.016	1	-.042	1	-.335	1
	4 max	.002	2	-.355	2	0	1
	min	-.013	1	-.38	1	0	1
	1 max	.288	1	.431	1	.191	1
	min	.286	2	.403	2	.181	2
	2 max	.258	2	.092	1	-.208	2
	min	.258	1	.087	2	-.224	1
	3 max	.231	2	-.23	2	-.094	2
	min	.229	1	-.247	1	-.101	1
	4 max	.203	2	-.547	2	.561	1
M4	min	.199	1	-.586	1	.523	2
	1 max	.042	1	.659	1	.62	1
	min	.038	2	.616	2	.58	2
	2 max	.017	1	.302	1	-.171	2
	min	.015	2	.282	2	-.183	1
	3 max	-.008	1	-.051	2	-.364	2
	min	-.009	2	-.055	1	-.389	1
	4 max	-.032	2	-.384	2	0	1
	min	-.033	1	-.411	1	0	1
	1 max	.218	1	.671	1	.355	1
	min	.203	2	.627	2	.332	2
	2 max	.218	1	.225	1	-.365	2
M5	min	.203	2	.21	2	-.391	1
	3 max	.218	1	-.207	2	-.368	2
	min	.203	2	-.222	1	-.394	1
	4 max	.218	1	-.623	2	.348	1
	min	.203	2	-.669	1	.324	2
	1 max	.669	1	.218	1	0	1
	min	.623	2	.203	2	0	1
	2 max	.669	1	.218	1	-.108	2
	min	.623	2	.203	2	-.116	1
	3 max	.669	1	.218	1	-.216	2
	min	.623	2	.203	2	-.232	1
	4 max	.669	1	.218	1	-.324	2
M6	min	.623	2	.203	2	-.348	1
	1 max	1.084	1	-.208	2	0	1
	min	1.012	2	-.222	1	0	1
	2 max	1.084	1	-.208	2	.118	1
	min	1.012	2	-.222	1	.111	2
	3 max	1.084	1	-.208	2	.237	1
	min	1.012	2	-.222	1	.222	2
	4 max	1.084	1	-.208	2	.355	1
	min	1.012	2	-.222	1	.332	2
	1 max	1.226	1	-.045	2	0	1
	min	1.144	2	-.047	1	0	1
	2 max	1.226	1	-.045	2	.019	1
M7	min	1.144	2	-.047	1	.019	2
	3 max	1.226	1	-.045	2	.039	1
	min	1.144	2	-.047	1	.038	2
	4 max	1.226	1	-.045	2	.058	1
	min	1.144	2	-.047	1	.056	2
	1 max	1.226	1	-.045	2	0	1
	min	1.144	2	-.047	1	0	1
	2 max	1.226	1	-.045	2	.019	1
	min	1.144	2	-.047	1	.019	2
	3 max	1.226	1	-.045	2	.039	1
	min	1.144	2	-.047	1	.038	2
	4 max	1.226	1	-.045	2	.058	1
	min	1.144	2	-.047	1	.056	2

Envelope Member Section Forces, (continued)

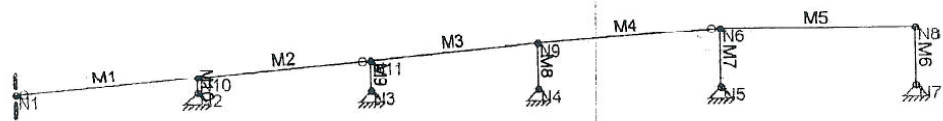
Member Label	Section		Axial (k)	Lc	Shear (k)	Lc	Moment (k)	Lc
M9	1	max	.834	1	-.217	2	0	1
		min	.78	2	-.229	1	0	1
	2	max	.834	1	-.217	2	.064	1
		min	.78	2	-.229	1	.06	2
	3	max	.834	1	-.217	2	.127	1
		min	.78	2	-.229	1	.121	2
M10	4	max	.834	1	-.217	2	.191	1
		min	.78	2	-.229	1	.181	2
	1	max	1.277	1	-.02	1	0	1
		min	1.195	2	-.033	2	0	1
	2	max	1.277	1	-.02	1	.005	2
		min	1.195	2	-.033	2	.003	1
	3	max	1.277	1	-.02	1	.009	2
		min	1.195	2	-.033	2	.006	1
	4	max	1.277	1	-.02	1	.014	2
		min	1.195	2	-.033	2	.008	1

Envelope Member Deflections

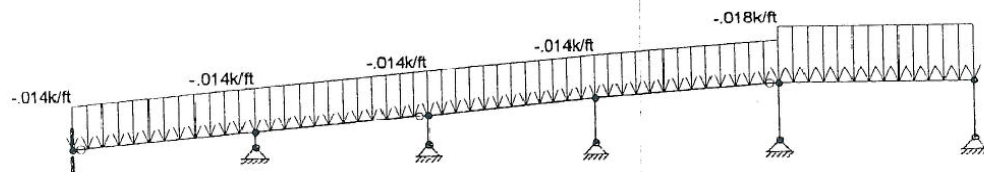
Member Label	Section		x-Translate (in)	Lc	y-Translate (in)	Lc	(n) L/y Ratio	Lc
M1	1	max	0	1	0	2	NC	
		min	0	2	0	1	NC	
	2	max	0	1	-.046	2	1243.875	2
		min	0	2	-.049	1	1169.664	1
	3	max	0	1	-.033	2	1756.299	2
		min	0	2	-.035	1	1659.338	1
M2	4	max	0	1	0	2	NC	
		min	0	2	0	1	NC	
	1	max	0	1	0	2	NC	
		min	0	2	0	1	NC	
	2	max	0	1	-.032	2	1848.986	2
		min	0	2	-.034	1	1708.638	1
	3	max	0	1	-.045	2	1280.237	2
		min	0	2	-.049	1	1189.011	1
	4	max	0	1	0	2	NC	
		min	0	2	0	1	NC	
M3	1	max	0	1	0	2	NC	
		min	0	2	0	1	NC	
	2	max	0	1	-.029	2	2063.401	2
		min	-.001	2	-.031	1	1919.616	1
	3	max	-.001	1	-.021	2	2931.998	2
		min	-.002	2	-.022	1	2735.504	1
	4	max	-.002	1	-.002	2	NC	
		min	-.002	2	-.002	1	NC	
	1	max	-.002	1	-.002	2	NC	
		min	-.002	2	-.002	1	NC	
M4	2	max	-.002	1	-.047	2	1336.222	2
		min	-.002	2	-.05	1	1247.236	1
	3	max	-.002	1	-.062	2	996.057	2
		min	-.002	2	-.067	1	930.197	1
	4	max	-.002	1	-.002	2	NC	
		min	-.002	2	-.002	1	NC	

Envelope Member Deflections, (continued)

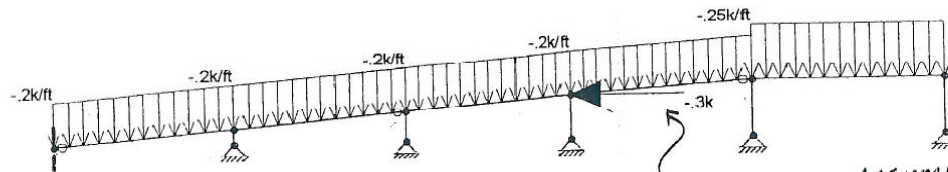
Member Label	Section		x-Translate (in)	Lc	y-Translate (in)	Lc	(n)	L/y Ratio	Lc
M5	1	max	-.001	1	-.002	2	NC		
		min	-.002	2	-.002	1	NC		
	2	max	-.002	1	-.109	2	559.623	2	
		min	-.002	2	-.117	1	521.856	1	
	3	max	-.002	1	-.109	2	557.976	2	
		min	-.002	2	-.117	1	520.674	1	
M6	4	max	-.002	1	-.001	2	NC		
		min	-.003	2	-.001	1	NC		
	1	max	0	1	0	1	NC		
		min	0	1	0	1	NC		
	2	max	0	2	-.013	2	1392.207	2	
		min	0	1	-.014	1	1294.941	1	
M7	3	max	0	2	-.016	2	1113.766	2	
		min	0	1	-.017	1	1035.953	1	
	4	max	-.001	2	.003	2	NC		
		min	-.001	1	.002	1	NC		
	1	max	0	1	0	1	NC		
		min	0	1	0	1	NC		
M8	2	max	0	2	.016	1	1270.353	1	
		min	0	1	.015	2	1357.948	2	
	3	max	-.001	2	.02	1	1016.282	1	
		min	-.002	1	.019	2	1086.359	2	
	4	max	-.002	2	.002	2	NC		
		min	-.002	1	.001	1	NC		
M9	1	max	0	1	0	1	NC		
		min	0	1	0	1	NC		
	2	max	0	2	.002	1	4529.485	1	
		min	0	1	.002	2	4784.344	2	
	3	max	0	2	.003	2	3827.475	2	
		min	0	1	.003	1	3623.588	1	
M10	4	max	0	2	0	2	NC		
		min	0	1	0	1	NC		
	1	max	0	1	0	1	NC		
		min	0	1	0	1	NC		
	2	max	0	2	0	2	NC		
		min	0	1	0	1	NC		
	3	max	0	2	0	2	NC		
		min	0	1	0	1	NC		
	4	max	0	2	0	2	NC		
		min	0	1	0	1	NC		
		max	0	2	0	2	NC		
		min	0	1	0	1	NC		



Solution: Envelope

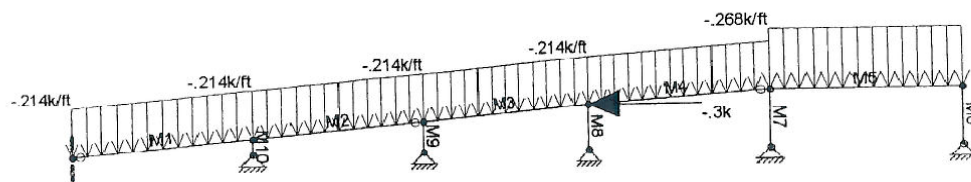


Loads: BLC 1, w1 - Dead Load
Solution: Envelope



HORIZONTAL ASSUMED
LIVELOAD SIMULATING
PEOPLE BUNCHED UP
ON RAMP WALKING
UP HILL.

Loads: BLC 2, w2 -Pedestrian Load
Solution: Envelope



Loads: LC 1, DL + Ped. Load
Solution: Envelope

Section: Welcome Ramp

Section Properties:

Number of Shapes	= 2	
Total Width	= 2.00	in
Total Height	= 4.00	in
Center, X _o	= 0.304	in
Center, Y _o	= -0.457	in
X-bar (Right)	= 1.571	in
X-bar (Left)	= 0.429	in
Y-bar (Top)	= 2.457	in
Y-bar (Bot)	= 1.543	in

Equivalent Properties:

Area, A _x	= 1.438	in ²
Inertia, I _{xx}	= 2.02	in ⁴
Inertia, I _{yy}	= 0.4212	in ⁴
Inertia, I _{xy}	= -0.4565	in ⁴
Torsional, J	= 0.0299	in ⁴

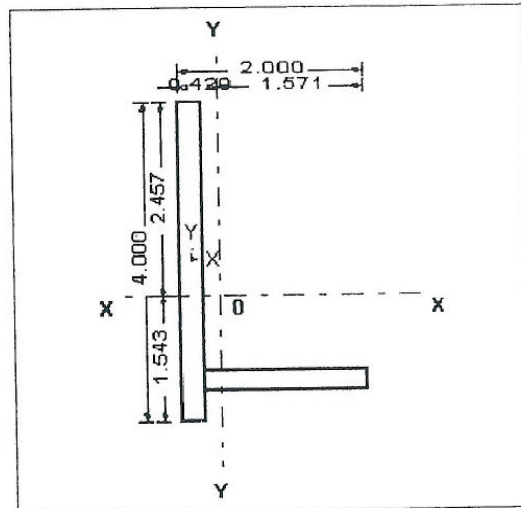
Modulus, S _x (Top)	= 0.8225	in ³
Modulus, S _x (Bot)	= 1.309	in ³
Modulus, S _y (Left)	= 0.981	in ³
Modulus, S _y (Right)	= 0.2682	in ³

Plastic Modulus, Z _x	= 1.4921	in ³
Plastic Modulus, Z _y	= 0.4852	in ³

Radius, r _x	= 1.186	in
Radius, r _y	= 0.541	in

Summary of Section Properties

Sh. No.	Section	Width in	Height in	X _o in	Y _o in	A _x in ²	I _{xx} in ⁴	I _{yy} in ⁴
1	Welcome Ramp	2.00	4.00	0.304	-0.457	1.438	2.02	0.4212



Section Diagram

Section: Welcome Deck

Section Properties:

Number of Shapes	= 2	
Total Width	= 2.00	in
Total Height	= 4.00	in
Center, Xo	= 0.304	in
Center, Yo	= 0.114	in
X-bar (Right)	= 1.571	in
X-bar (Left)	= 0.429	in
Y-bar (Top)	= 1.886	in
Y-bar (Bot)	= 2.114	in

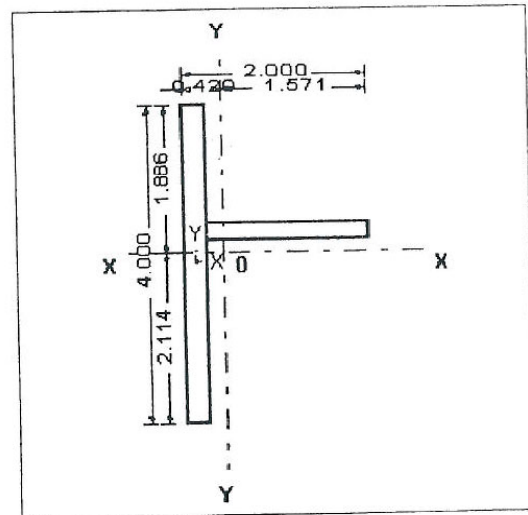
Equivalent Properties:

Area, Ax	= 1.438	in ²
Inertia, Ixx	= 1.378	in ⁴
Inertia, Iyy	= 0.4212	in ⁴
Inertia, Ixy	= 0.1141	in ⁴
Torsional, J	= 0.0299	in ⁴

Modulus, Sx(Top)	= 0.7309	in ³
Modulus, Sx(Bot)	= 0.652	in ³
Modulus, Sy(Left)	= 0.981	in ³
Modulus, Sy(Right)	= 0.2682	in ³

Plastic Modulus, Zx	= 1.0532	in ³
Plastic Modulus, Zy	= 0.4852	in ³

Radius, rx	= 0.9792	in
Radius, ry	= 0.5413	in



Section Diagram

Summary of Section Properties

Sh. No.	Section	Width in	Height in	Xo in	Yo in	Ax in ²	Ixx in ⁴	Iyy in ⁴
1	Welcome Deck	2.00	4.00	0.304	0.114	1.438	1.378	0.4212

Member Stress Results

Access the **Member Section Stresses** spreadsheet by selecting the **Results** menu and then selecting **Members ▸ Stresses**.

These are the member stresses calculated along each active member. The number of sections for which stresses are reported is controlled by the **Number Of Sections** specified on the Global window. The actual number of segments is this **Number Of Sections** minus 1. The incremental length of each segment is the same. For example, if you specify 5 sections, the member is divided into 4 equal pieces, and the stresses are reported for each piece.

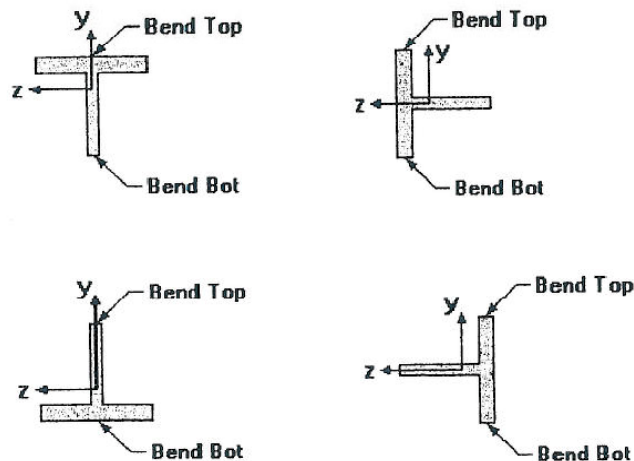
There will be four stress values listed for each section location along the member taking into account any member offsets. The units for the stresses are shown at the top of each column. As for the sign convention, the signs of these results correspond to the signs of the forces. These line up as positive or negative according to the member local axis directions.

The axial stress is the ratio P/A , where P is the section axial force. A positive stress is compressive, since the sign of the stress follows the sign of the force.

The shear stress is calculated as $V/S.A.$, where $S.A.$ is the effective shear area. For members not defined with a section set a value of 1.2 is used for the shear area coefficient $S.A.$

The bending stresses are calculated using the familiar equation $M * c / I$, where " M " is the bending moment, " c " is the distance from the neutral axis to the extreme fiber and " I " is the moment of inertia. The stress for the section's extreme edge is listed with respect to the positive and negative directions of the local y and z axes. A positive stress is compressive and a negative stress is tensile.

Some shapes are not symmetrical about both local axes. For example Tee and Channel shapes. Thus the stress at the positive and negative edges may not be the same. The locations for the calculated stresses are illustrated in this diagram:

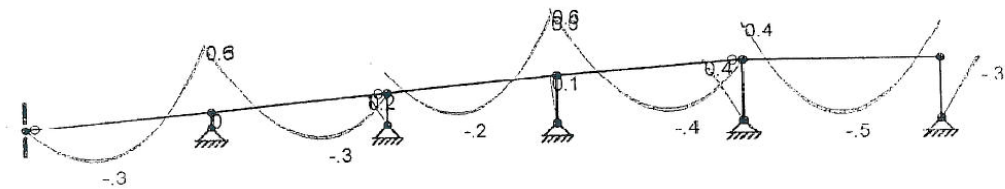


So, the y-top location is the extreme fiber of the shape in the positive local y direction, y-bot is the extreme fiber in the negative local y direction, etc. The y-top,bot stresses are calculated using M_z .

For enveloped results the maximum and minimum value at each location is listed. The load combination producing the maximum or minimum is also listed, in the " I_c " column. To include a particular Load Combination in the envelope analysis, open the **Load Combinations** spreadsheet and check the box in the "Env" column.

Note

- A special case is bending stress calculations for single angles. The bending stresses for single angles are reported for bending about the principal axes.
- To view the results for a particular member, use the Find option. To view the maximums and minimums, use the Sort option.



Solution: Envelope
Member Bending Moments (k-ft)
Reaction units are k and k-ft

TABLE 20-II-A—MINIMUM MECHANICAL PROPERTIES FOR ALUMINUM ALLOYS—(Continued)
Values Are Given in Units of ksi (1,000 lb/in²)

ALLOY AND TEMPER	PRODUCT ¹	THICKNESS RANGE ¹ (Inch) × 25.4 for mm	TENSION ✓		COMPRES- SION ↙	SHEAR		BEARING		COMPRESSIVE MODULUS OF ELASTICITY ³
			F_{tu}^2 ksi	F_{ty}^2 ksi	F_{cy} ksi	F_{su} ksi	F_{sy} ksi	F_{bu} ksi	F_{by} ksi	E ksi
			× 6.89 for MPa							
5086-H111	Extrusions	up to 0.500	36	21	18	21	12	70	36	10,400
-H111	Extrusions	0.501 and over	36	21	18	21	12	70	34	10,400
-H112	Plate	0.250-0.499	36	18	17	22	10	72	31	10,400
-H112	Plate	0.500-1.000	35	16	16	21	9	70	28	10,400
-H112	Plate	1.001-2.000	35	14	15	21	8	70	28	10,400
-H112	Plate	2.001-3.000	34	14	15	21	8	68	28	10,400
-H32	Sheet and plate	All	40	28	26	24	16	78	48	10,400
-H34	Drawn tube.	All	44	34	32	26	20	84	58	10,400
5154-H38	Sheet	0.006-0.128	45	35	33	24	20	81	56	10,300
5454-H111	Extrusions	up to 0.500	33	19	16	20	11	64	32	10,400
-H111	Extrusions	0.501 and over	33	19	16	19	11	64	30	10,400
-H112	Extrusions	up to 5.000	31	12	13	19	7	62	24	10,400
-H32	Sheet and plate	0.020-2.000	36	26	24	21	15	70	44	10,400
-H34	Sheet and plate	0.020-1.000	39	29	27	23	17	74	49	10,400
5456-H111	Extrusions	up to 0.500	42	26	22	25	15	82	44	10,400
-H111	Extrusions	0.501 and over	42	26	22	24	15	82	42	10,400
-H112	Extrusions	up to 5.000	41	19	20	24	11	82	38	10,400
-H321	Sheet and plate	0.188-1.250	46	33	27	27	19	87	56	10,400
-H321	Plate	1.251-1.500	44	31	25	25	18	84	53	10,400
-H321	Plate	1.501-3.000	41	29	25	25	17	82	49	10,400
-H323	Sheet	0.051-0.249	48	36	34	28	21	94	61	10,400
-H343	Sheet	0.051-0.249	53	41	39	31	24	101	70	10,400
6005-T5	Extrusions	up to 0.500	38	35	35	24	20	80	56	10,100
6061-T6, -T651	Sheet and plate	0.010-4.000	42	35	35	27	20	88	58	10,100
-T6, -T651 ¹	Extrusions	up to 3.000	38	35	35	24	20	80	56	10,100
-T6, -T651	Rolled rod and bar	up to 8.000	42	35	35	27	20	88	56	10,100
-T6	Drawn tube	0.025-0.500	42	35	35	27	20	88	56	10,100
-T6	Pipe	up to 0.999	42	35	35	27	20	88	56	10,100
-T6	Pipe	over 0.999	38	35	35	24	20	80	56	10,100

MAIN RAILS

HAND RAILS

6063-T5	Extrusions	up to 0.500	22	16	16	13	9	46	26	10,100
-T5	Extrusions	over 0.500	21	15	15	12	8.5	44	24	10,100
-T6	Extrusions	All	30	25	25	19	14	63	40	10,100
	Pipe									
6351-T5	Extrusions	up to 1.00	38	35	35	24	20	80	56	10,100

¹Values also apply to -T6511 temper.² F_{tu} and F_{ty} are minimum specified values (except for Alclad 3004-H14, -H16 and F_{ty} for Alclad 3003-H18). Other strength properties are corresponding minimum expected values.³For deflection calculations an average modulus of elasticity is used; numerically this is 100 ksi (689 MPa) lower than the values in this column.

TABLE 20-II-B—MINIMUM MECHANICAL PROPERTIES FOR WELDED ALUMINUM ALLOYS¹
(Gas Tungsten Arc or Gas Metal Arc Welding with No Postweld Heat Treatment)

(Gas Tungsten Arc or Gas Metal Arc Welding with No Postweld Heat Treatment)								
ALLOY AND TEMPER	PRODUCT AND THICKNESS RANGE (Inch) × 25.4 for mm	TENSION		COMPRES- SION	SHEAR		BEARING	
		F_{tut}^1 ksi	F_{tyt}^2 ksi	F_{cwt}^2 ksi	F_{suw} ksi	F_{syw} ksi	F_{buw} ksi	F_{byw} ksi
		× 6.89 for MPa						
1100-H12, -H14	All	11	4.5	4.5	8	2.5	23	8
3003-H12, -H14, -H16, -H18	All	14	7	7	10	4	30	12
Alclad 3003-H12, -H14, -H16, -H18	All	13	6	6	10	3.5	30	11
3004-H32, -H34, -H36	All	22	11	11	14	6.5	46	20
Alclad 3004-H32, -H34, -H14, -H16	All	21	11	11	13	6.5	44	19
3005-H25	Sheet 0.013-0.050	17	9	9	12	5	36	15
5005-H12, -H14, -H32, -H34	All	14	7	7	9	4	28	10

F_{yw} = bearing yield strength within 1.0 inch (25.4 mm) of a weld, ksi (MPa).
 F_c = allowable compressive stress, ksi (MPa).
 F_{cy} = compressive yield strength, ksi (MPa).
 F_{cyw} = compressive yield strength across a butt weld (0.2 percent offset in 10-inch (254 mm) gage length), ksi (MPa).
 F_{ec} = $\pi^2 E / (l/r)^2$, where l/r is slenderness ratio for member considered as a column tending to fail in the plane of the applied bending moments, ksi (MPa).
 F_n = allowable stress for cross section 1.0 inch (25.4 mm) or more from weld, ksi (MPa).
 F_{pw} = allowable stress on cross section, part of whose area lies within 1.0 (25.4 mm) inch of a weld, ksi (MPa).
 F_s = allowable shear stress for members subjected only to torsion or shear, ksi (MPa).
 F_{su} = shear ultimate strength, ksi (MPa).
 F_{uw} = shear ultimate strength within 1.0 inch (25.4 mm) of a weld, ksi (MPa).
 F_{yw} = shear yield strength, ksi (MPa).
 F_{tu} = tensile ultimate strength, ksi (MPa).
 F_{tw} = tensile ultimate strength across a butt weld, ksi (MPa).
 F_{ty} = tensile yield strength, ksi (MPa).
 F_{yw} = tensile yield strength across a butt weld (0.2 percent offset in 10-inch (254 mm) gage length), ksi (MPa).
 F_y = either F_y or F_{cy} , whichever is smaller, ksi (MPa).
 f = calculated stress, ksi (MPa).
 f_a = average compressive stress on cross section of member produced by axial compressive load, ksi (MPa).
 f_b = maximum bending stress (compressive) caused by transverse loads or end moments, ksi (MPa).
 f_s = shear stress caused by torsion or transverse shear, ksi (MPa).
 G = modulus of elasticity in shear, ksi (MPa).
 g = spacing of rivet or bolt holes perpendicular to direction of load, inches (mm).
 h = clear height of shear web, inches (mm).
 I = moment of inertia, inches⁴ (mm⁴).
 I_a = moment of inertia of horizontal stiffener, inches⁴ (mm⁴).
 I_s = moment of inertia of transverse stiffener to resist shear buckling, inches⁴ (mm⁴).
 I_x = moment of inertia of a beam about axis perpendicular to web, inches⁴ (mm⁴).
 I_y = moment of inertia of a beam about axis parallel to web, inches⁴ (mm⁴).
 I_{yc} = moment of inertia of compression element about axis parallel to vertical web, inches⁴ (mm⁴).
 J = torsion constant, inches⁴ (mm⁴).
 k_1 = coefficient for determining slenderness limit S_2 for sections for which the allowable compressive stress is based on crippling strength.
 k_2 = coefficient for determining allowable compressive stress in sections with slenderness ratio above S_2 for which the allowable compressive stress is based on crippling strength.
 k_c = coefficient for compression members.
 k_t = coefficient for tension members.
 L = length of compression member between points of lateral support, or twice the length of a cantilever column (except where analysis shows that a shorter length can be used), inches (mm).

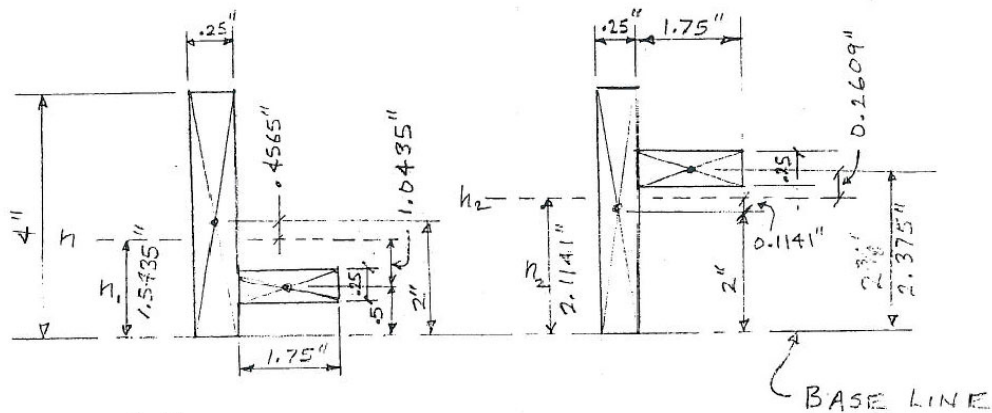
2-272

(2)

L_b = length of beam between points at which the compression flange is supported, or length of cantilever beam from free end to point at which flange is supported against lateral movement, inches (mm).
 L_h = total length of portion of column lying within 1.0 inch (25.4 mm) of welds at ends of columns that are supported at both ends, inches (mm).
 L_w = increased length to be substituted in column formula to determine welded column, inches (mm).
 l/r = slenderness ratio for columns.
 M = bending moment, inch-kips (kN-m).
 M_c = bending moment at center of span resulting from applied bending (kN-m).
 M_m = maximum bending moment in span resulting from applied bending (kN-m).
 M_1, M_2 = bending moments at two ends of a beam, inch-kips (kN-m).
 N = length of bearing at reaction or concentrated load, inches (mm).
 n_a = factor of safety on appearance of buckling.
 n_u = factor of safety on ultimate strength.
 n_y = factor of safety on yield strength.
 P = local load concentration on bearing stiffener, kips (kN).
 P_c = allowable reaction or concentrated load per web, kips (kN).
 P_t = allowable tensile load per fastener, sheet to purlin or girt, kips (kN).
 R = outside radius of round tube or maximum outside radius for an oval tube.
 R_b = radius of curvature of tubular members, inches (mm).
 R_t = transition radius, the radius of an attachment of the weld detail.
 r = least radius of gyration of a column, inches (mm).
 r_L = radius of gyration of lip or bulb about face of flange from which lip projects.
 r_y = radius of gyration of a beam (about axis parallel to web), inches (mm). (If unsymmetrical about the horizontal axis, r_y should be calculated as the same as the compression flange.)
 S_c = section modulus of a beam, compression side, inches³ (mm³).
 SR = stress ratio, the ratio of minimum stress to maximum stress.
 S_x = section modulus of a beam, tension side, inches³ (mm³).
 S_1, S_2 = slenderness limits.
 s = spacing of transverse stiffeners (clear distance between stiffeners for stiffeners consisting of a pair of members, one on each side of the web, center-to-center distance consisting of a member on one side of the web only), inches (mm) or bolt holes parallel to direction of load, inches (mm).
 t = thickness of flange, plate, web or tube, inches (mm). (For tapered flange thickness.)
 V = shear force on web at stiffener location, kips (kN).
 α = a factor equal to unity for a stiffener consisting of equal members on both sides and equal to 3.5 for a stiffener consisting of a member on one side only.
 θ = angle between plane of web and plane of bearing surface ($\theta \leq 90^\circ$, degrees).
2001.4 Identification. Aluminum for structural elements shall at all times be separately handled in the fabricator's plant so that the separate alloys and tempers are

(1.) CALC. I_{xx}

FOR TWO AL. SECTIONS.



$$h = \frac{\sum M}{\sum A}$$

$$h_1 = \frac{(2'')(.25)(4.0) + (.5)(.25)(1.75)}{(.25)(4.0) + (.25)(1.75)} = \frac{2.2188}{1.4375} = 1.5435''$$

$$h_2 = \frac{(2'')(.25)(4.0) + (2.375)(.25)(1.75)}{(.25)(4.0) + (.25)(1.75)} = \frac{3.0391}{1.4375} = 2.1141''$$

$$I_i = I + Ad^2 + I + Ad_n^2 = \frac{bd^3}{3} + bd(d_n^2) + \dots$$

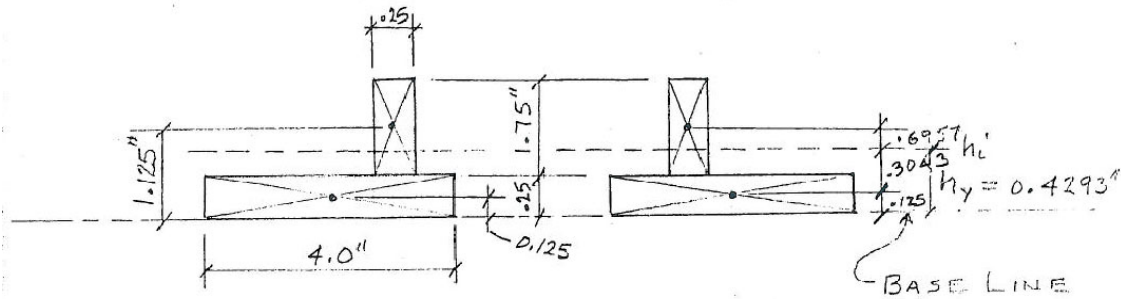
$$I_1 = \frac{.25(4^3)}{12} + .25(4)(.4565)^2 + \frac{1.75(.25^3)}{12} + 1.75(.25)(1.0435)^2$$

$$I_1 = 1.333 + 0.2064 + 0.0023 + 0.4764 = \underline{2.0201 \text{ in}^4}$$

$$I_2 = \frac{.25(4^3)}{12} + .25(4)(0.1141)^2 + \frac{1.75(.25^3)}{12} + 1.75(.25)(0.2609)^2$$

$$I_2 = 1.333 + 0.0130 + 0.0023 + 0.0298 = \underline{1.3784 \text{ in}^4}$$

(2.) CALC. I_{yy} FOR TWO AL. SECTIONS.



$$n = \frac{\sum M}{\sum A}$$

$$I_1 = I_{yy}$$

$$h_y = \frac{(0.125)(0.25)(4.0) + (1.125)(0.25)(1.75)}{0.25(4.0) + 0.25(1.75)} = 0.4293"$$

$$I_1 = I + Ad^2 + I + Ad^2 = \frac{bd^3}{3} + bd(d_h^2) + \dots$$

$$I_1 = \frac{4.0(0.25)^3}{12} + 4.0(0.25)(0.3043)^2 + \frac{0.25(1.75)^3}{12} + 0.25(1.75)(0.6957)^2$$

$$I_1 = 0.0052 + 0.0926 + 0.1117 + 0.2117 = \underline{\underline{0.4212 \text{ in}^4}}$$

(3.) CALC. RAMP:
(USING RISA-2D)

$$A_{\frac{1}{42}} = .25(4') + 1.75(.75) = 1.4375 \text{ in}^2$$

$$I_1 = 2.0201 \text{ in}^4$$

$$I_2 = 1.3784 \text{ in}^4$$

$$I_1 = \text{RAMP}$$

$$I_2 = \text{PLATFORM}$$

$$6061\text{-T6 AL}, F_y = 35 \text{ KSI}$$

$$\text{DEAD LOAD} = 7 \text{ PSF}$$

$$\text{LIVE LOAD} = 100 \text{ PSF}$$

$$\text{PEDESTRIAN WALK} = (\text{UB7 TABLE 16-A})$$

$$\text{RAMP BEAM DL} = 7\left(\frac{4'}{2}\right) = 14 \text{ PLF}$$

$$\text{RAMP BEAM LL} = 100\left(\frac{4'}{2}\right) = 200 \text{ PLF}$$

$$\text{PLATFORM DL} = 7\left(\frac{5'}{2}\right) = 17.5 \text{ PLF}$$

$$\text{PLATFORM LL} = 100\left(\frac{5'}{2}\right) = 250 \text{ PLF}$$

WELCOME RAMP, INC.

STRUCTURAL ANALYSIS

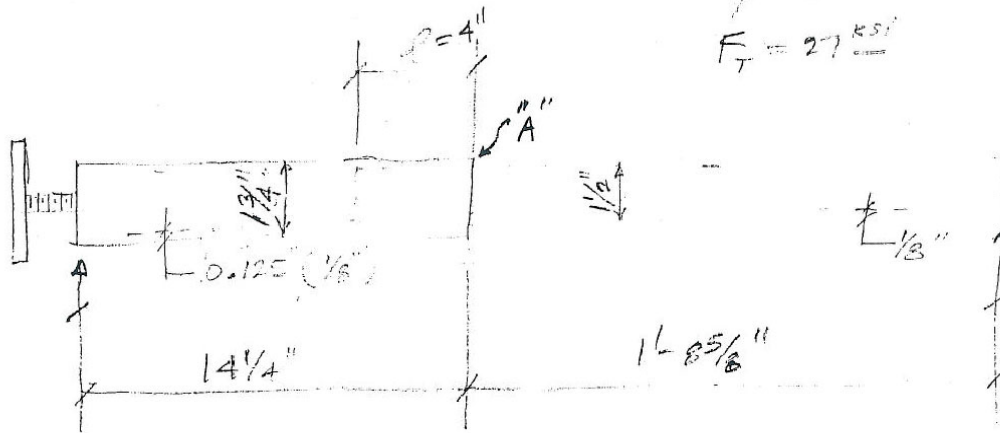
Adjustable Leg Design

425-754-4108
(client)

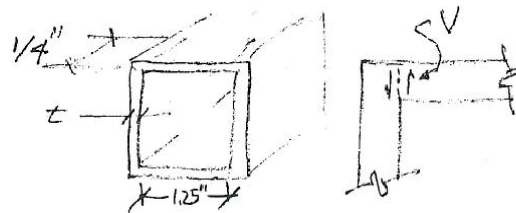
ASSUME:
6063-T5 AL (ASTM B 221)

$$F_y = 21 \text{ ksi}$$

$$F_T = 27 \text{ ksi}$$



(1.) Check Point "A" For MAX. V OF WALL = Z



ASSUME 1/4" BEARING
IN SHEAR = V
(IGNORE BENDING OF 1/4" SECT.)
Z = 0.125"

ASSUME 1ST 1/4" OF SHEAR = V

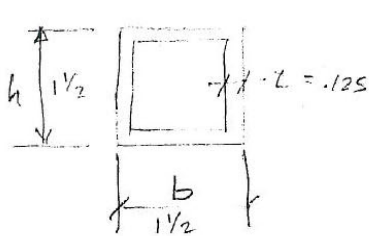
$$F_T = 27 \text{ ksi} \therefore V = 3/4 F_T = 20.25 \text{ ksi (ASSUMED)}$$

$$0.125" (0.25") (2 \text{ sides}) (20.25 \text{ ksi}) = 1.2656 \text{ K} = 1,265 \text{ lb MAX.}$$

(2.) Check Point "A" For MAX. BENDING OF 1 1/2" D.

$$F_b = 2/3 F_y = 2/3 (21) = 14 \text{ ksi}$$

(2.) CONT.



$$S = \frac{bh^3 - b'h'^3}{6h} = \frac{1.5(1.5)^3 - 1.25(1.25)^3}{6(1.5)}$$

$$S = 0.2912 \text{ in}^3$$

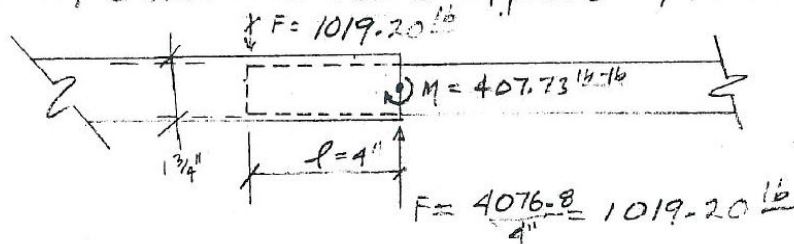
$$S = \frac{M_{\max}}{F_b}$$

$$M_{\max} = (0.2912 \text{ in}^3) \left(14 \frac{15}{16} \text{ in} \right) (1000) = 4076.80 \frac{\text{in} \cdot \text{lb}}{\text{in}^3}$$

∴ THE MAX. BENDING OF THE $1 \frac{1}{2}'' \times 1 \frac{1}{2}'' = 4076.80 \frac{\text{in} \cdot \text{lb}}{\text{in}^3}$

BUT THE ABILITY OF THE $1 \frac{3}{4}'' \times 1 \frac{3}{4}''$ AT POINT "A" TO ACCEPT SHEAR IS 1,265 $\frac{\text{lb}}{\text{in}^2}$.

(3.) NEXT, CALC. MAX. FORCE APPLIED BY $1 \frac{1}{2}'' \times 1 \frac{1}{2}''$ & COMPRI.



$$\therefore 1019.20 \frac{\text{lb}}{\text{in}^2} < 1,265 \frac{\text{lb}}{\text{in}^2} \quad \text{OK!}$$

THEREFOR, THE POST WILL FAIL IN BENDING PRIOR TO FAILING IN SHEAR AT POINT "A". $l = 4$ IS THE MINIMUM ALLOWABLE LEG OVERLAP FOR ANY LEG OF THE PREVIOUS DESIGNS

WELCOME RAMP, INC.

STRUCTURAL ANALYSIS

Alternate 7-foot Landing Design

→ INCLUDED IS THE NEW DESIGN FOR A 7' SECTION PLATFORM.

1) FOR A SINGLE POST AND DOUBLE ANGLE BEAM.

2) FOR A DOUBLE POST AND DOUBLE 20" BEAM CONFIGURATION.

- THIS CHECKS ONLY WHAT HAS BEEN CHANGED FOR THE 7'-0" PLATFORM ASSUMES TREADS ARE 1091/2" ON STAIRS TO SPAN 7'-0".

SUMMARY

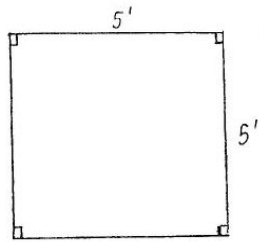
USE CURRENT POST IN CENTER.

POST WILL BE PLACED ON A 16"X16" FOOTING.

NEW DOUBLE ANGLE FOR BEAM SECTION IS A 4X2X3/16

ANGLE PLACED BACK TO BACK.

DESIGN OF 7' SECTION USING
SINGLE POST IN CENTER OF NEW
DOUBLE ANGLE BEAM.



Existing Design

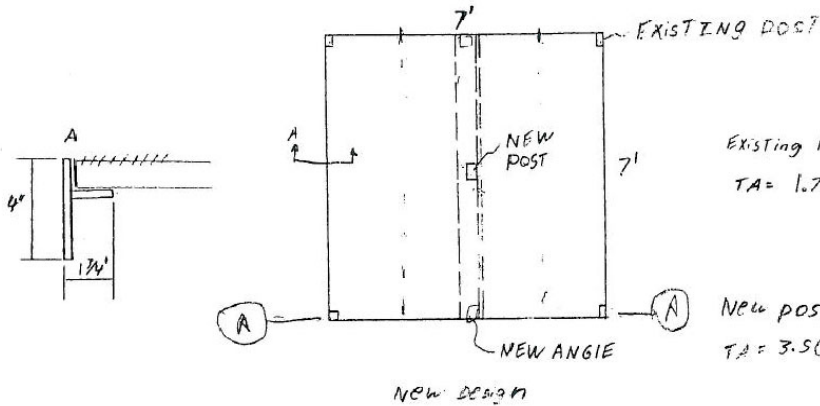
post Load Existing

$$TA = 2.5 \times 2.5 = 6.25 \text{ FT}^2$$

100 psf LL

7 psf DL

$$\text{service load per post} = \underline{669 \text{ lb}}$$



NEW DESIGN

Existing POST New load

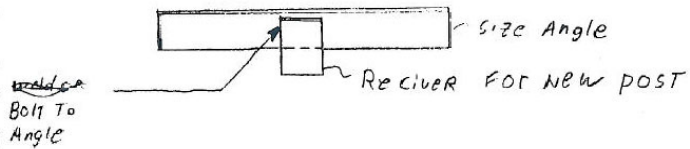
$$TA = 1.75 \times 3.5 = 6.125 \text{ FT}^2$$

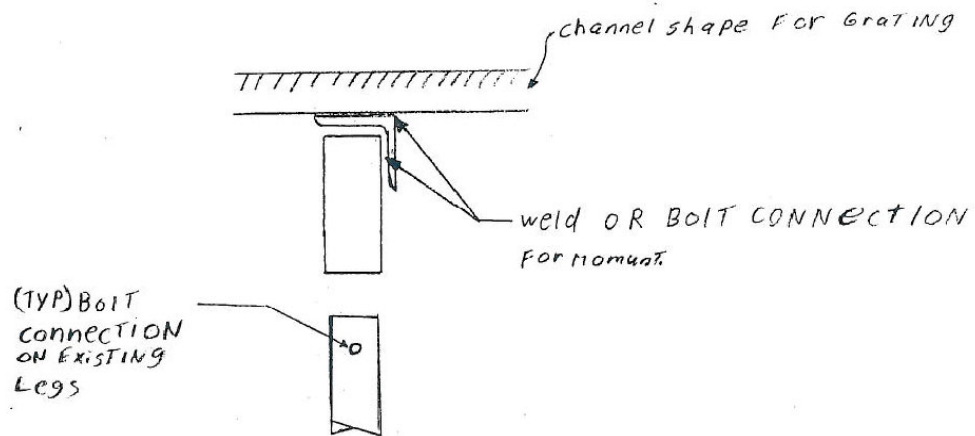
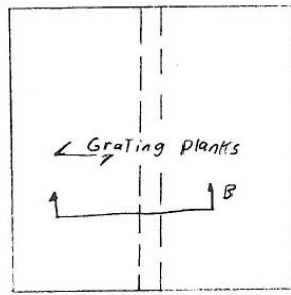
New post Load

$$TA = 3.5(7') = 24.5 \text{ FT}^2$$

$$\text{Service Load} = \underline{2622 \text{ lb}} \quad 400\% \text{ increase}$$

NOT Including Angle member wt.





Typical POST CALCULATIONS.

TABLE 20-11-A pg 2-296

PIPING = 6061-T6 EXTRUSIONS

Tension $F_{tx} = 38 \text{ ksi}$; $F_{ty} = 35 \text{ ksi}$

compression $F_{cy} = 35 \text{ ksi}$

shear $F_{su} = 24 \text{ ksi}$; $F_{sy} = 20 \text{ ksi}$

Bearing $F_{bu} = 80 \text{ ksi}$; $F_{by} = 56 \text{ ksi}$

$E = 10,100 \text{ ksi}$

square structural tubing pg 111 section 4

leg material = $1\frac{1}{2}'' \text{ sq} \times .12'' \text{ AL tubing}$

WT per FT = 2.252 lb/ft

ITEM 1. BUCKLING LOAD

For Buckling assuming 48" with NO eccentricity

$$F_{cr} = \frac{\pi^2 E}{(K L/r)^2} \quad r = \sqrt{I/A} = \sqrt{\frac{2.118}{.6624}} = .5655 \quad K=1$$

$$= \frac{\pi^2 (10,100 \text{ ksi})}{(1 \cdot 48'' / .5655)^2} = \underline{13.84 \text{ kips}} < \overset{\text{service load}}{262216}$$

ITEM 2. AXIAL LOAD

AXIAL BEARING $P/A_g = \text{service Load} = \frac{2622}{.6624} = \underline{3958 \text{ psi}}$

ITEM 3. BEARING.

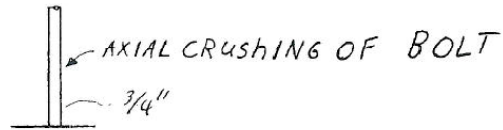
allow comp = 35 ksi

Bolt Bearing - Aluminum will fail before Bolt bearing

Tube thickness = .12 in Bolt size = $\frac{3}{8}'' = .375$ $F_{bu} = 80 \text{ ksi}$

$$F_b = (.375(.12))^2 \times 80 \text{ ksi} = \underline{7.2 \text{ kips}} < 2.6 \text{ k}$$

ITEM 4. AXIAL LOAD on Rod AT BASE



$$Area = \pi r^2 = \pi (.375)^2 = .4418 \text{ in}^2$$

$$Load = \frac{2622 \text{ lb}}{.4418 \text{ in}^2} = 5934 \text{ psi} < F_{cy} = 35 \text{ ksi} \quad \text{OK}$$

ITEM 5. Base PLATE Bering

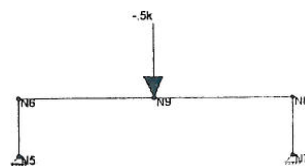
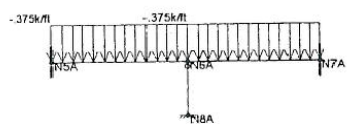
Base plate = 2"x2"

$$\frac{2622 \text{ lb}}{4 \text{ in}^2} = 655 \text{ psi} \quad \text{NOT OK}$$

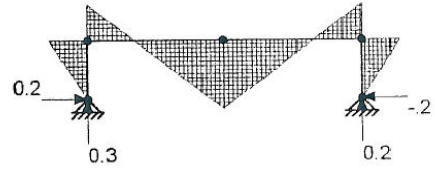
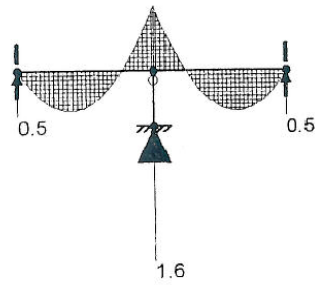
allowable load = 4000 psf at FOOT or 27.7 psi

$$\text{Try a 16" Block} = 1.78 \text{ FT}^2$$

$$4000 \text{ psf} (1.78 \text{ FT}^2) = 7111 \text{ lb} > 2622 \text{ lb} \quad \text{OK!} \leftarrow$$



Loads: ULC 1, w1 - Dead Load
Results for LC 1, DL + Ped. Load



Results for LC 1, DL + Ped. Load
Member Bending Moments (k-ft)
Reaction units are k and k-ft

Member Data

Member Label	I Joint	J Joint	Rotate (degrees)	Shape / Section Set	Material Set	Phys Memb	End Releases I-End J-End AVM AVM	End Offsets I-End J-End (in) (in)	Inactive Code	Length (ft)
M1	N6	N9		SEC2	AL	Y				3.5
M2	N7	N8		SEC3	AL	Y				1.599
M3	N5	N6		SEC3	AL	Y				1.599
M4	N5A	N6A		SEC4	AL	Y				3.5
M5	N6A	N7A		SEC4	AL	Y				3.5
M6	N8A	N6A		SEC3	AL	Y		PIN		1.5
M7	N9	N8		SEC2	AL	Y				3.5

Sections

Section Label	Database Shape	Material Label	Area (in) ²	SA (0,180)	SA (90,270)	I (90,270) (in ⁴)	I (0,180) (in ⁴)	T/C Only
SEC1	Welcome Ramp	AL	1.438	1.2	1.2	.421	2.02	
SEC2	Welcome Deck	AL	1.438	1.2	1.2	.421	1.378	
SEC3	TU2X2X2	AL	.897	1.2	1.2	.513	.513	
SEC4	WT4X10.5	AL	3.08	1.2	1.2	4.89	3.9	

Member Deflections, By Combination

LC	Member Label	Section	x-Translation (in)	y-Translation (in)	(n) U/y Ratio
1	M1	1	0	0	NC
		2	0	-.086	3035.648
		3	0	-.174	1377.517
		4	0	-.214	NC
1	M2	1	0	0	NC
		2	0	-.013	1458.898
		3	0	-.016	1167.118
		4	0	0	NC
1	M3	1	0	0	NC
		2	0	.013	1458.898
		3	0	.016	1167.118
		4	0	0	NC
1	M4	1	0	0	NC
		2	0	-.015	3103.087
		3	0	-.012	4257.729
		4	0	-.003	NC
1	M5	1	0	-.003	NC
		2	0	-.012	4257.729
		3	0	-.015	3103.087
		4	0	0	NC
1	M6	1	0	0	NC
		2	-.001	0	NC
		3	-.002	0	NC
		4	-.003	0	NC
1	M7	1	0	-.214	NC
		2	0	-.174	1377.517
		3	0	-.086	3035.648
		4	0	0	NC

Member Stresses, By Combination

LC	Member Label	Section	Axial (ksi)	Shear (ksi)	Bending top (ksi)	Bending bot (ksi)
1	M1	1	.135	.21	-5.078	5.693
		2	.135	.21	-.271	.304
		3	.135	.21	4.536	-5.085
		4	.135	.21	9.343	-10.474
1	M2	1	.279	.464	0	0
		2	.279	.464	2.412	-2.412
		3	.279	.464	4.824	-4.824
		4	.279	.464	7.236	-7.236
1	M3	1	.279	-.464	0	0
		2	.279	-.464	-2.412	2.412
		3	.279	-.464	-4.824	4.824
		4	.279	-.464	-7.236	7.236
1	M4	1	0	.579	0	0
		2	0	.072	.838	-3.338
		3	0	-.435	.371	-1.479
		4	0	-.942	-1.401	5.577
1	M5	1	0	.942	-1.401	5.577
		2	0	.435	.371	-1.479
		3	0	-.072	.838	-3.338
		4	0	-.579	0	0
1	M6	1	1.812	0	0	0
		2	1.812	0	0	0
		3	1.812	0	0	0
		4	1.812	0	0	0
1	M7	1	.135	-.21	9.343	-10.474
		2	.135	-.21	4.536	5.085
		3	.135	-.21	-.271	.304
		4	.135	-.21	-5.078	5.693

Section: RShape1

Section Properties:

Number of Shapes	= 2	
Total Width	= 4.014	in
Total Height	= 4.01	in
Center, X _o	= 14.995	in
Center, Y _o	= -1.605	in

X-bar (Right)	= 2.007in
X-bar (Left)	= 2.007in
Y-bar (Top)	= 2.617in
Y-bar (Bot)	= 1.393in

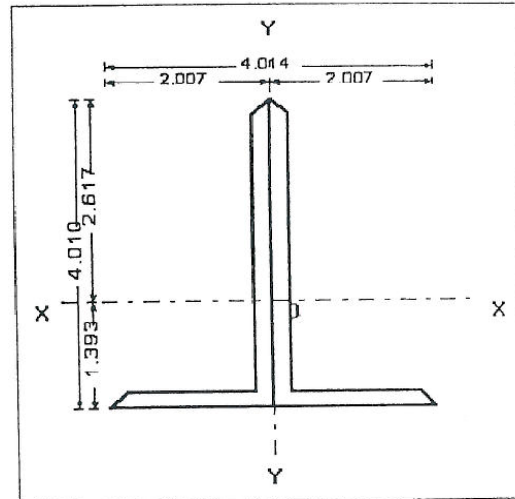
Equivalent Properties:

Area, A _x	= 2.24	in ²
Inertia, I _{xx}	= 3.607	in ⁴
Inertia, I _{yy}	= 0.9487	in ⁴
Inertia, I _{xy}	= 0.000	in ⁴
Torsional, J	= 0.0304	in ⁴

Modulus, S _x (Top)	= 1.378	in ³
Modulus, S _x (Bot)	= 2.589	in ³
Modulus, S _y (Left)	= 0.473	in ³
Modulus, S _y (Right)	= 0.473	in ³

Plastic Modulus, Z _x	= 2.492	in ³
Plastic Modulus, Z _y	= 16.794	in ³

Radius, r _x	= 1.269	in
Radius, r _y	= 0.651	in



Section Diagram

Basic Properties of Shapes in Section:

Sh. No.	Shape	Factor	Width in	Height in	X _o in	Y _o in	A _x in ²	I _{xx} in ⁴	I _{yy} in ⁴
1	Unequal L	1	2.00	4.00	14.60	-1.60	1.12	1.804	0.30
2	Unequal L	1	2.00	4.00	15.39	-1.61	1.12	1.804	0.30

Additional Properties of Shapes in Section:

Sh. No.	Shape	J in ⁴	S _x in ³	S _y in ³	Z _x in ³	Z _y in ³	r _x in	r _y in
1	Unequal L	0.0152	0.6905	0.1859	1.246	0.533	1.269	0.517
2	Unequal L	0.0152	0.6905	0.1859	1.246	0.533	1.269	0.517

Summary of Properties

Sh. No.	Section	Width in	Height in	X _o in	Y _o in	A _x in ²	I _{xx} in ⁴	I _{yy} in ⁴
1	RShape1	4.014	4.01	14.995	-1.605	2.24	3.607	0.949

Calculation Procedure

- 1) Closed Shapes:
The geometric properties for closed shapes are computed by using the Polygon method. All closed shapes are represented by closed polygons. Curvilinear and circular shapes or edges are represented by several straight line segments. The properties the overall shape are computed by geometric summation of the properties of a trapezoid defined by projection of two consecutive points of the cross-section on to the x and y axis.
- 2) Open Shapes:
The geometric properties for open (thin walled) shapes are computed by using the Polyline method. All open shapes are represented by polylines. Curvilinear and circular shapes or edges are represented by several straight line segments. The properties the overall shape are computed by geometric summation of the properties of a line defined by projection of two consecutive points of the cross-section on to the x and y axis.
For details refer to the User's Manual

FOOTING SIZING CALCULATIONS

1) LOADING

Dead Load=	7 psf
Live Load =	100 psf
Total Load, RAMP_TL =	107 psf

2) FOOTING ON SOIL

Soil Allowable Bearing Pressure =	1500 psf
7' Platform Center Column, Area =	12.25 psf
Max Load =	1311 #
Min. Footing Area =	0.87 sf
Footing Pad w/ minimum Size =	11.22 inch

USE: 12-INCH, MIN. SQUARE PAD UNDER COLUMN ON SOIL

3) FOOTING ON PAVEMENT (Based on 8-inch Depth Pavement+Base)

Allowable Bearing Pressure =	8831 psf
7' Platform Center Column, Area =	12.25 psf
Max Load =	1311 #
Min. Footing Area =	0.15 sf
Footing Pad w/ minimum Size =	4.62 inch

USE: 5-INCH, MIN. SQUARE PAD UNDER COLUMN ON PAVEMENT

D. DEFLECTION CHECK FOR ALUMINUM TUBES

$$\text{ALLOWABLE } \delta = \frac{L}{240} = .175"$$

$$\delta = \frac{5 W L^4}{384 E I} = \frac{5 (374.5/12) (3.5' \times 12)^4}{384 (10,100 \times 1000) (2.074 \text{ in}^4)}$$

$\text{Load} = 107(3.5) = 374.5 \text{ PLF}$

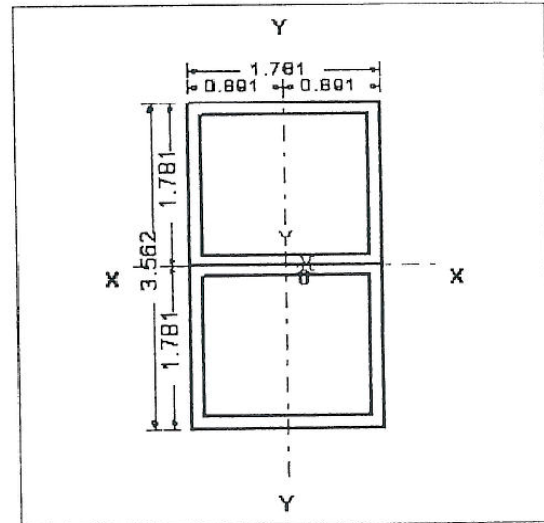
$$= .064" < .175 \text{ OK} \leftarrow$$

USE 2 - 1.781" TUBES STACKED.

Section:Section1

Section Properties:

Number of Shapes	= 2	
Total Width	= 1.781	in
Total Height	= 3.562	in
Center, Xo	= 0.00	in
Center, Yo	= 0.00	in
X-bar (Right)	= 0.891	in
X-bar (Left)	= 0.891	in
Y-bar (Top)	= 1.781	in
Y-bar (Bot)	= 1.781	in
Equivalent Properties:		
Area, Ax	= 1.656	in ²
Inertia, Ixx	= 2.074	in ⁴
Inertia, Iyy	= 0.7612	in ⁴
Inertia, Ixy	= 0.000	in ⁴
Torsional, J	= 1.2688	in ⁴
Modulus, Sx(Top)	= 1.164	in ³
Modulus, Sx(Bot)	= 1.164	in ³
Modulus, Sy(Left)	= 0.855	in ³
Modulus, Sy(Right)	= 0.855	in ³
Plastic Modulus, Zx	= 1.568	in ³
Plastic Modulus, Zy	= 1.029	in ³
Radius, rx	= 1.119	in
Radius, ry	= 0.678	in



Section Diagram

Basic Properties of Shapes in Section: (Local Axis, for n=1)

Sh. No.	Shape	Modular Ratio(n)	Width in	Height in	Xo in	Yo in	Ax in ²	Ixx in ⁴	Iyy in ⁴
1	Tube	1.00	1.781	1.781	0.00	-0.891	0.828	0.3806	0.3806
2	Tube	1.00	1.781	1.781	0.00	0.891	0.828	0.3806	0.3806

Additional Properties of Shapes in Section: (Local Axis, for n=1)

Sh. No.	Shape	J in ⁴	Sx-Top in ³	Sy-Right in ³	Zx in ³	Zy in ³	rx in	ry in
1	Tube	0.6344	0.4274	0.4274	0.5144	0.5144	0.678	0.678
2	Tube	0.6344	0.4274	0.4274	0.5144	0.5144	0.678	0.678

Summary of Section Properties

Sh. No.	Section	Width in	Height in	Xo in	Yo in	Ax in ²	Ixx in ⁴	Iyy in ⁴
1	Section1	1.781	3.562	0.00	0.00	1.656	2.074	0.7612

Calculation Procedure

- 1) Closed Shapes:
The geometric properties for closed shapes are computed by using the Polygon method. All closed shapes are represented by closed polygons. Curvilinear and circular shapes or edges are represented by several straight line segments. The properties of the overall shape are computed by geometric summation of the properties of a trapezoid defined by projection of two consecutive points of the cross-section on to the x and y axis.
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For details refer to the User's Manual

WELCOME RAMP, INC.

STRUCTURAL ANALYSIS

Manufacturer Information - Planks

TRACTION TREAD LOAD TABLES

PLANKING

Plank Description
Plank: Traction Tread
Width: 12"
Gauge: 13 GA

2" Channel Height

Se: 0.27 in³
Mmax: 5335 lb-in

1 1/2" Channel Height

Se: 0.174 in³
Mmax: 3438 lb-in

2" Channel Height

	2'-0	3'-0	4'-0	5'-0	6'-0	7'-0	8'-0	9'-0	10'-0
U	889	395	222	142	99	73	56	44	36
D	0.057	0.129	0.229	0.357	0.514	0.7	0.915	1.158	1.429
C	889	593	445	356	298	254	222	198	178
D	0.046	0.103	0.183	0.286	0.412	0.56	0.732	0.926	1.143

1 1/2" Channel Height

	2'-0	3'-0	4'-0	5'-0	6'-0	7'-0	8'-0	9'-0	10'-0
U	573	255	143	92	64	47	36	28	23
D	0.07	0.157	0.279	0.436	0.627	0.854	1.115	1.411	1.742
C	573	382	287	229	191	164	143	127	115
D	0.056	0.125	0.223	0.348	0.502	0.683	0.892	1.129	1.394

Notes:

U = Uniform Load, psf
C = Concentrated Load, psf
D = Deflection, in.

③ 4'-8" u = 109 or!

- 1.) Allowable loads are based on the latest edition of AISI, 1986 Edition w/ 12/11/89 Addendum.
- 2.) This table is a theoretical calculation of the allowable loads and deflections for the specified spans. There are no test results to verify the actual load carrying capabilities. This table should be used as a reference only.
- 3.) Loads and deflections are based on side channel deflection only, and does not account for strut loading of the grating surface.

TRACTION TREAD LOAD TABLES

STAIRS

Plank Description
 Plank: Traction Tread
 Width: 12"
 Gauge: 11 GA

2" Channel Height
 Se: 0.541 in³
 Mmax: 10690 lb-in

1 1/2" Channel Height
 Se: 0.331 in³
 Mmax: 6541 lb-in

2" Channel Height		2'-0	3'-0	4'-0	5'-0	6'-0	7'-0	8'-0	9'-0	10'-0
U	1782	792	445	285	198	145	111	88	71	
D	0.028	0.064	0.113	0.177	0.254	0.346	0.452	0.572	0.706	
C	1782	1188	891	713	594	509	445	396	356	
D	0.023	0.051	0.09	0.141	0.203	0.277	0.362	0.458	0.565	

1 1/2" Channel Height		2'-0	3'-0	4'-0	5'-0	6'-0	7'-0	8'-0	9'-0	10'-0
U	1090	484	273	174	121	89	68	54	44	
D	0.035	0.079	0.14	0.219	0.315	0.429	0.561	0.71	0.876	
C	1090	727	545	436	363	311	273	242	218	
D	0.028	0.063	0.112	0.175	0.252	0.343	0.449	0.568	0.701	

Notes:

U = Uniform Load, psf
 C = Concentrated Load, psf
 D = Deflection, in.

- 1.) Allowable loads are based on the latest edition of AISI, 1986 Edition w/ 12/11/89 Addendum.
- 2.) This table is a theoretical calculation of the allowable loads and deflections for the specified spans. There are no test results to verify the actual load carrying capabilities. This table should be used as a reference only.
- 3.) Loads and deflections are based on side channel deflection only, and does not account for strut loading of the grating surface.